ALESIS MATICA 500/900 (A4/A8) Service Manual P/N: 8-31-0030-A

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1.00 Theory of Operation

The A4/A8 amplifiers are basic stereo amplifiers. They have 0dBm input sensitivities for rated output at 4Ω , with the ability to drive any load impedance from 2Ω to an open circuit. They have balanced inputs via Neutrik combination connectors providing XLR and 1/4" TRS connections and also a barrier strip. The output of the amplifier is obtained by way of four five way binding posts. Reference designations in the text refer specifically to the A4 amplifier except where otherwise noted. Though reference designations between the two units are different, the designs are virtually identical. The only significant differences occur in the output section (since the A8 is required to handle much more power than the A4).

Here are some of the major features and building blocks of the Matica:

- **À** An input balanced to unbalanced converter.
- **À** A second stage pre-amp and an amplifier gain stage utilizing a monolithic front end with discrete complimentary transconductance stage and a complimentary output stage in a common collector configuration.
- **à** Output device protection is accomplished with a conventional volt-amp current limiter circuit. The output devices use a new perforated emitter technology unique to **MOTOROLA.** The output devices are driven by similar technology devices, but they have been optimized for extremely linear current gain with a unity gain bandwidth (F_t) of 50 MHz.
- **à** The speakers are protected by output relays. They are activated during the first 3 to 5 seconds the amplifier is turned on. Also, if a DC condition exists at the output of the amplifier or the amplifier is driven to full output below 5Hz the relays will be activated.
- **à** Thermal management and protection are accomplished with a large heavy aluminum extruded heat sink the is fan cooled. If the sink gets warmer than 55 deg. C, the fan is automatically stepped up in speed and if the heat sink gets warmer than 80 deg. C the fan is run at high speed and the output relays are activated to disconnect the load until the unit has cooled to 65 deg. C. There is also a unique feature of the amplifier fan circuit in that when the amplifier is providing an output signal of a little more that a watt the fan speed is modulated or increased by the signal. This will help get longer run times with the amplifier under extreme load conditions.

1.10 Input Section

The input stage is made up of a dual *Signetics* 5532A op amp. This is a low noise selected version of the 5532. One half of the dual is used for each channel. The circuit is a basic balanced to unbalanced converter. It can be driven unbalanced but 6dB differences in gain may result for various hookups. If the (+) input is driven with the (-) input grounded the gain will be unity. If the (+) input is driven with the (-) input left open there will be a gain reduction of 6dB. This is not recommended as a noisier condition may result. If the (-) input is driven, gain will be unity and will not change with the grounding or ungrounding the (+) input The maximum input level before clipping in about +21dBm. Since there is no level control in front of the converter this is the maximum input level for the amplifier. Connections to the Alink connector are between R1, R2 and R3, R4. These are provided so an outboard impedance may be connected to modify the gain and overload characteristics as well as its frequency response. Following the amplifier is a passive low pass (R7, C1) filter that begins to limit the high frequency gain of the amplifier.

1.20 Pre-Amp Section

The pre-amp section also uses the *Signetics* 5532A op amp. The circuits of the pre-amp are of opposing signal polarity to provide push pull characteristics and are connected via the stereo/bridge switch. Each of the two pre-amp channels has 15.7 dB of gain but channel A is inverting and channel B is not.

Since the main amplifier is inverting, channel A will not invert the signal and channel B will. Doing this facilitates two things. When the stereo/bridge switch is in the bridge mode channel B will already be out of phase with A so no signal inversion will have to be done to achieve bridge operation. Also by operating B out of phase all the time, (even in stereo operation) getting the phase of the signal flipped back at the speaker terminals, the amplifiers low frequency power bandwidth will be increased. This allows the power supply to be utilized more efficiently.

This section also shapes the bandwidth of the amplifier further via another low pass pole being added to each stage. First and second stage high pass filtering occurs via the 100uf coupling capacitors preceding the volume pots and after the pre-amp stages. The pre-amp stages drive the main amplifier directly.

ALINK connections at the junction between R8, C2 and R13, C5 are for sending the output signal of the input stage at a low impedance for use with auxiliary equipment. The connection between R9, R10 and R14, R17 are to be used to for defeating the level controls by supplying an input signal from a very low source impedance to swamp out the signal from the pots.

1.30 Main Amplifier Section

The main amplifier is composed of four sections:

- The monolithic front end.
- A complimentary voltage gain stage or transconductance stage
- àààà The output driver
- The output stage

The amplifier is configured in the inverting mode. This allows for the inputs of the op amp to remain at a 0 voltage potential and ease operation on a +/-15 volt supply. The large voltage swing is accomplished with a discrete, complimentary darlington connected transconductance stage Q1, Q2, Q3, and Q4. The current in the transconductance stage is set by the voltage divider network made up of R19, R20, R21, and R22. The first transistor in the darlington is a TO-92 packaged device with the current set by R27, and R28. The collector of this transistor is not tied to the second collector in the darlington connection but rather to the +/-15 volt supply to help increase the bandwidth of the stage and reduce the dissipation in the TO-92 devices. The closed loop gain of the amplifier has been set for 10X or 20dB. The DC output offset is a function of the input offset voltage error of the op amp times the gain of the system. With the offset error of the op amp at about +/- 1mv the amplifier will have less than +/- 10mv of output offset. The feedback network is composed of R25, R18, and C11. C11 reduces the bandwidth of the amplifier. The large low frequency gain of the op amp helps to reduce the supply ripple that is introduced into the system by the lack of supply rejection in the voltage gain stage. Under driven conditions at mild loads of 4 or 8Ω at mid and high frequencies, the output of the op amp will appear not to have any signal or very little signal on it. When the amplifier is clipped, or driven to its rail, the output of the op amp will be driven to its rail, or about +/- 14 volts. It is trying to correct the loop error or non linearity of clipping in the amplifier. The only other time the output of the op amp will become a large signal is at a 2Ω condition at lower frequencies. This is due to the loss of loop gain when the transconductance stage is required to deliver large amounts of current to the output stage drivers. CR1 and CR2 are connected as clamps to the discrete

darlingtons (causing the transconductance stage not to saturate, which reduces the possibility of saturation in the gain stage).

The drivers and output devices are mounted on the large extruded aluminum heat sink. The drivers have extremely linear gain with changes in current. They also have an Ft of 50mHz keeping the gain linear with frequency. The output devices are 16 amp, 250 volt, 200 watt devices. These are very strong devices. The output stage is configured in a common collector, or emitter follower configuration. The drivers are connected again in a discrete complimentary darlington configuration. This allows for a class A bias and protection scheme that offers very close bias tracking and simple current limiting. Also there are 1.2Ω resistors in the bases of all the output devices. This helps linearize the gain with frequency and reduce high current parasitics. When the output stage is biased properly, the DC voltage drop across the emitter resistors should by 2-3mv cold and may rise to as much as 6-10mv when hot. Finally the output of the amplifier is de coupled from the load with a traditional termination network. This network isolates the amplifier and feedback loop from loads at high frequencies, especially capacitive ones. This is how unconditional loop stability is achieved. Under bench test conditions it is recommended that the amplifier not be driven to full power at 20kHz and above for periods longer than a few minutes as this will cause R53 to over heat. Under music conditions there is never enough energy to have this be a problem.

1.40 Output Device Protection

Output device protection is accomplished with a relatively simple circuit. The protection circuit is broken up into Q17 that protects the NPN output devices and Q18 that protects the PNP output devices. These devices are complimentary as are the output devices but they also have similar V_{be} N to P. This allows selection of a point of protection that will be about equal for each half of the output stage. R55 and R56 sense the voltage at the emitter of two of the output devices and sum them. The emitter of Q17 is connected to the output of the amplifier. When a voltage across the emitter resistors of the output devices reaches about 0.7 volts, Q17 will conduct if there is no voltage across R54. This condition exists for a short circuit or something very close. As the amplifier impresses a voltage across a load it also has that same voltage across R54. As the voltage across R54 gets larger more current must flow through the emitter resistors of the output devices to cause enough voltage to be developed at the base of the protection device to turn it on. This is what is known as the load line. As the voltage across the output devices gets lower they can deliver more current in keeping with a constant power. When the protection device is conducting the current from the transconductance stage is essentially being diverted around the output stage to the load. Everything described for the positive half cycle is the same for the negative half. C18 and C19 slow down the protection device and keep it from any possible oscillation condition. CR3 and CR4 are used to protect possible reverse Vbe conduction of the protection devices and CR4 and CR5 prevent conduction of the protection devices while in the opposite half cycle.

1.50 Bias Circuit

The bias circuit is more that just a single device V_{be} multiplier seen in many audio amplifiers. The circuit consists of an active shunt regulator. The reason for this is two fold. The shunt regulator has a much lower impedance than the single device regulator. This helps control the bias voltage better when there is a change in the quiescent operating current of the transconductance stage. Since the operating, or quiescent current of the transconductance stage is supply dependent, the need for a bias circuit that doesn't change voltage with current is imperative. Also by reducing the current through the bias sense transistor a larger change in V_{be} with temperature can be realized. This tracks the needs of the output stage better. The 5k pot in the bias circuit adjusts the potential of the regulator. A 1.5k resistor (R55) sets the current

through the bias sense transistor (Q18) making the current in the sense transistor relatively constant. Q17 is the pass transistor of the regulator. Note that any time the output transistors are replaced, the pass and bias transistors must also be replaced. Failure to do so will probably result in the output transistors failing again.

1.60 Speaker Protection

There are two sections to the speaker protection circuit. A section made up of a quad comparator with a low pass filter before it and a discrete bipolar transistor circuit that controls the two speaker relays. The transistor circuit and +15 volt three terminal regulator make up the power up delay circuit and "instant off" power down circuit. When the unit is turned on the 15 volt regulator supplies power to the discrete circuit. Q24 controls the speaker relays and is held off during power up by Q23. During power up C24 is not charged and must be charged before Q23 will turn off. This delays the turn on of the output relays to protect against any transients that may occur at power up. Once on, there are four ways the relays can be opened again.

- The first is if the heat sink gets to 80 deg. C. then TH1 will open and release the relays.
- Second is by shut down of the amplifier. Upon the removal of AC to the amplifier, the three terminal regulator will fall out of regulation that forces Q21 on because C23 acts like a battery and momentarily turns on Q21. This pulse will cause Q22 to dump the charge on C24, turning on Q23.
- The third way is if the line voltage get low (about 90 volts in the 120v unit). At this time the regulator will fall out of regulation and the first pulse from the 50 or 60 Hz that gets through the regulator will cause C24 to be dumped again and the 3-5 second charge time will occur again.
- The fourth way is to have the circuit be triggered by the comparator circuit.

The comparator is DC coupled to the output of the amplifier before the speaker relays. They are set up with each one of their inputs tied to a +/- 1.2v reference derived from CR7, CR8, CR9, and CR10. The low pass filter is comprised of R64, R65, R66, R67, C21, and C22. When the output of the amplifier is driven to full output at or below 5Hz, or 1.2v of DC offset appears at the output of the amplifier, it will trigger one of the comparators which in turn opens the output relays. When this happens the same 3 to 5 second period must occur before the relays will engage again. If the fault condition persists then the relays will remain open.

The 18 volt AC winding which runs this circuit is rectified by a half wave rectifier. This is allows one side of the winding to be grounded. The 18 volt winding is also provided at the Alink connector to facilitate generation a +/- 15 volt supply to run auxiliary accessories requiring phantom power.

1.70 Fan Speed Control

The fan circuit has three modes of operation in which it varies the speed of the fan depending on demand or condition. At power up of the amplifier Q25 and Q26 will be saturated until the relay circuit enables the speaker relays. This condition lasts for 3 to 5 seconds. During this time Q27 is also saturated. This forces the fan to run at an elevated speed momentarily. After this time only R85 will be delivering current to the fan. The fan will be running at a very slow speed. The reason for the accelerated speed of the fan at turn on is that the current delivered by R85 may not be sufficient to start the fan, especially at low power line levels. Signals from both channels are detected by Q25 and Q26 as the amplifier is driven harder. They act as rectifiers of the signal, and when they conduct the 40Ω resistor connected to Q27 delivers more current to the fan motor, causing the fan speed to increase with the drive of the amplifier. The fan motor itself acts as a flywheel or filter to smooth the modulation and the speed of the fan is proportional to the average of the drive to the amplifier. If the heat sink gets hotter than 55 deg.C. then an additional 20Ω resistor is switched in to deliver more current to the fan. The fan.

speed will still be modulated by the drive to the amplifier. If the heat sink gets hot enough to trip the 80deg. C. breaker, then the relay circuit will disconnect the load and also turn on Q25 and Q26. This will increase the fan to its highest speed and cool the amplifier. Upon cooling below 65deg. C. the amplifier will resume normal operation.

1.80 Thermal Management System

The large extruded aluminum heat sink in the center of the chassis is the heart of the amplifiers heat dissipation scheme. It is a forced air cooling system. In the A8 the heat sink has a thermal resistance of .075 deg. C. per watt when the fan is at full speed. This is equal to about 800 watts of heat. The air from the fan is forced into the center of the side of the heat sink with fins and the air flows around the sink and out over the amplifier circuitry. It has an air intake at the front of the amplifier and exhaust at the left rear. As explained in the fan speed control section, the speed of the fan is determined by the demands on the amplifier. If for some reason the fan should stop but not fail there is enough dissipation in the main heat sink as well as the four TO-220 stand up heat sinks on the PCB to allow operation indefinitely while at a quiescent condition.

2.00 Updates and Corrections.

2.10 Stripped Heat Sinks

Occasionally when tightening down the heat sink clamps one of the screws will strip the threads out of the heat sink itself. Because heat sink is a rather expensive and bulky item, a way was found to reuse stripped heat sinks. Use a long (at least 1 1/4") machine screw from the clamp side, and a threaded hex standoff inserted into the heat sink fin side. Do not use just a hex nut, as it will probably not be able to hold the clamp pressure any more then the heat sink did. See diagram on next page.



2.20 New Case Bracket Insulator(s)

found that lt was it was possible for the insulation on the wires from the main power transformer(s) could over time be cut by the case bracket(s) (one in A4, two in A8). This could in turn make it possible for the end-user to be shocked through the case itself. The solution was to replace the insulators with a version that covered those areas of the metal that could potentially cut the insulation.

To replace the old insulators, first remove the rectifier and move the cables away from the case brackets. Be sure to examine the wires for any



damage that have already occurred. Then remove the bracket(s) from the chassis. Figure 2 shows the locations of the bracket mounting screws while Figures 3 and 4 show the new and old styles of insulator (New style Alesis Part # 5-04-1018). Replace the old insulators and reassemble the brackets and rectifier. Route the wires around the transformer bracket(s) as shown in Figure 5. In addition, the regulator U5 (A8) U4 (A4) and transistor Q53 (A8) Q39 (A4) on the Fan PCB (See Figure 2) should be checked to ensure that they do not short to the case. If necessary, bend these components away from the case bottom and resolder both of them to ensure a solid connection.





2.30 Transformer Insulators

These foam insulators were added for two purposes:

- Electrical Isolation
- Added resistance to mechanical shock.

The insulators stick to the case top as shown in Figure 6 (A8) so that they are directly over the transformer(s) when the casetop is reassembled. The part numbers for the foam insulators are 9-23-1067 for the A8, and 9-23-1068 for the A4.



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3.00 Troubleshooting

The following chart is intended to help point a technician in the right direction. Unfortunately there isn't space to provide an absolutely comprehensive list, however this should help with some of the more common solutions.

Symptoms	Probable Cause	Solution	
No Power (No LED, No Fan)	Tripped breaker.	Reset breaker.	
	Faulty breaker.	Replace breaker.	
	Faulty transformer.	Replace transformers and retest.	
	Faulty A.C.	Be sure that 30 amp service is available without significant voltage drop.	
No output, no LED, Fan running full on.	Fan board/Main harness disconnected.	Reconnect and retest.	
	Faulty +15V regulator.	Troubleshoot and repair as necessary.	
Clip LED on, no output.	Blown output section.	Replace all active components following the diver I.C. (U2-channel A U3 channel B) in blown channel. Also replace any out of tolerance resistors in the output section.	
	Poor solder on the large power supply capacitors. (Causes ground reference to drift).	Troubleshoot and repair as necessary.	
	J1 or J14 loose.	Reseat cable and apply hot glue to prevent re loosening.	
One channel out.	Poor solder connections at the Neutrik connector or the high pass capacitors (see section 1.20).	Troubleshoot and repair as necessary.	









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BOM

4.00 A4 Service Parts List

Group	Part.Number	Description	Qty	PCB	Ref.Designator	Comment
ASY	7-40-0120	TRANSFORMER 120V A4	1			
ASY	9-79-0109	ASSY PCB MAIN A4	1			
ASY	9-79-0130	ASSY DISPLAY/VOL A4	1			
ASY	9-79-0132	MODULE OUTPUT A4	1			
ASY	9-79-0134	ASSY FAN/RELAY/PS A4	1			
ASY	9-96-1259	ASSY BINDING POSTS COMPLETE 44/48	1		FINAL ASSEMBLY	
CAB	4-18-1676	CABLE 6" BLK (TWO WIRES TWISTED)	2		I WAE NOOEMBET	
CAB	4-18-1678	CABLE 7" RED/BLK (TWO WIRES TWISTED)	1	FΔN	B+ B-	
CAR	4 10 1752		1	MAIN	UTO UM MAIN	
CAR	4 10 1754		1	IVICALIN	12 to 114 (GRAV)	
CAB	4-13-17.54		1			
	4-19-1755		1		123 TO 120,313,30,33	
CAB	4-19-1759		1		JIZ TO JIS (TELLOW, GRN, BLOE)	
CAB	4-19-1760					
CAB	4-19-1761	CABLE 3-PIN BIAS CH A	1		J15 TO J21 (BRN,RED,ORANGE)	
CAB	4-74-0013	ASSY WIRE HARNESS 14" (25-PIN D-CON & 26-PIN DIL HDR CON) 26 AWG	1			
CAB	7-41-0006	CABLE POWER W/SPADE LUG (UL/CSA) A4/A8	1			
CFC	1-99-0010	CAP 10uF ELEC 35V 20%	1	FAN	C39	
CFC	1-99-0100	CAP 100PF 100V 5% NPO MC	2	MAIN	C 19, 49	
CFC	1-99-0101	CAP 100uF 25V 20% MUSE	4	MAIN	C 2, 3, 16, 30	
CFC	1-99-0101	CAP 100uF 25V 20% MUSE	2	FAN	C42, 43	
CFC	1-99-0102	CAP 0.1uF 100V 5% FILM	12	MAIN	C 9, 11, 14, 18, 20, 21, 23, 25, 28, 32, 33, 34	
CFC	1-99-0102	CAP 0.1uF 100V 5% FILM	4	FAN	C38, 47, 48, 50	
CFC	1-99-0103	CAP .01uF 250V 20% XCAP	1	MAIN	C 6	
CFC	1-99-0103	CAP .01uF 250V 20% XCAP	1	FAN	C44	
CFC	1-99-0104	CAP 10000uF ELEC 80V 20%	2	FAN	C45, 46	
CFC	1-99-0220	CAP 22PE 100V 5% NPO MC	4	MAIN	C 10, 12, 24, 26	
CEC	1-99-0221	CAP 220µE ELEC 25V 20%	2	MAIN	C4 7	
CEC	1-99-0221	CAP 220µE ELEC 25V 20%	2	OUTPUT M	C35_36	
CEC	1-99-0221	CAP 220UE ELEC 25V 20%	2	FAN	C37 40	
CEC	1.00.1200	CAP 1200PE 100V 5% EII M	4	MAIN	C 9 12 22 27	
CEC	1 00 2200		4	EAN	C 0, 13, 22, 27	
CEC	1.00.2200	CAP 3300PE 100V 5% EILM	6	MAIN	C 1 5 15 17 29 31	
CFD	2 00 0021		0	MAIN	CD 4 5 11 12	
OFD	2-99-0021		4	IVIAIIN		
OFD	2-99-1757	DIODE ZENER IN/S/A (9.1V)	2	IVIAIIN		
CFD	2-99-4003	DIODE POWER IN4003	2	FAN		
CFD	2-99-4148	DIODE SIGNAL 1N4148	8	MAIN	CR 6-9, 13-16	
CFD	2-99-4148	DIODE SIGNAL 1N4148	/	FAN	UR 17, 19, 20, 22-25	
CFD	2-99-5400	DIODE POWER 1N5400	1	FAN	CR21	
CFM	2-02-5352	DIODE 1N5352BRL 15V 5W 5%	2	MAIN	CR 1, 2	
CFR	0-99-0002	RES 0.2 OHM 3W 5% MO	6	MAIN	R30, 32, 57, 83,86, 89	
CFR	0-99-0002	RES 0.2 OHM 3W 5% MO	6	OUTPUT M	R93, 96, 99, 104, 107, 109	
CFR	0-99-0010	RES 10 OHM 1/4W 5% CF	4	MAIN	R 23, 59, 90, 91	
CFR	0-99-0010	RES 10 OHM 1/4W 5% CF	1	FAN	R128	
CFR	0-99-0011	RES 10 OHM 3W 5% MO	2	FAN	R137, 138	
CFR	0-99-0012	RES 1.2 OHM 1/2W 5% MO	6	MAIN	R 29, 31, 56, 82, 85, 88	
CFR	0-99-0012	RES 1.2 OHM 1/2W 5% MO	6	OUTPUT	R94, 97, 100, 105, 108, 110	
CFR	0-99-0020	RES 20 OHM 5W 5% WW	1	FAN	R114	
CFR	0-99-0027	RES 2.7 OHM 3W 5% MO	2	OUTPUT	R92, 111	
CFR	0-99-0040	RES 40 OHM 5W 5% WIRE WOUND	1	FAN	R112	
CFR	0-99-0100	RES 100 OHM 1W 5% MO	2	MAIN	R 9, 11	
CFR	0-99-0103	RES 10K 1/4W 1% MF	8	MAIN	R 3, 6, 14, 17, 45, 53, 71, 79	
CFR	0-99-0104	RES 10K 1/4W 5% CE	2	MAIN	R 12, 13	
CER	0-99-0104	BES 10K 1/4W 5% CE	10	FAN	B116 123 125-127 130 131 133-135	1
CER	0-99-0120	BES 120 OHM 5W 5% WW	1	FAN	R113	
CER	0-99-0202	RES 2K OHM 1/4W 5% CE	2	MAIN	B 22 28	
CER	0-00-0202	RES 22K 1/AW 5% CF	1	MAIN	R 136	
CEP	0.00.0223	DES 22K 1/4W 5% CE	2	EAN		
	0.00.0223	DES 220 OUM 1/4W 5% MO	3	MAIN	D22 50 94 97	l
	0.00.0330		4		DOE 09 102 100	l
	0.00.0511		4			
	0-99-0511		0	MAIN	[Γ /, 10, 30, 49, 02, /5	
Group	Part.Number	Description	Qty	PCB	Ref.Designator	Comment
CFR	0-99-0511	RES 51.1 OHM 1/4W 1% MF	2	OUTPUT M	R101, R102	

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CER	0-99-0563	RES 5 6K 1/2W 5% CE	2	ΜΔΙΝ	R 54 80	
CER	0.99-0503	DES 50K 1/4W 1% ME	4	MAIN	R 41 46 67 72	
	0.00.0690		4	MAIN	R 41, 40, 07, 72	
CER	0-33-0000		6	MAIN	D 25 49 50 61 74 70	
CEP	0.99.1000		1	EAN	P120	
CER	0-33-1000		1	MAIN	D 10	
CER	0-00-1001		1	EAN	R120	
	0.00 1402		2	FAIN	R 129	
CER	0-99-1402		2	MAIN	R 42, 00	
	0-99-1500	RES 1.5K OHM 1/4W 5% CF	2	IVIAIN	R 51, //	
	0-99-1300			FAIN	R124	
	0-99-2210		4	MAIN		
OFR	0-99-3033		2	IVIAIIN	R 20, 27	
OFR	0-99-3300	RES 3.3K 1/4W 5% CF	2	MAIN	R 55, 81	
CFR OFR	0-99-3300	RES 3.3K 1/4W 5% CF	1	FAN	R117	
	0-99-3303	RES 330K 1/4W 5% CF	3	FAN		
CFR	0-99-4990	RES 4.99K 1/4W 1% CF	8	MAIN	R 1, 2, 4, 5, 15, 16, 20, 21	
CFR	0-99-4991	RES 499 OHM 1/4W 1% MF	8	MAIN	R 8, 19, 43, 44, 69, 70, 139, 140	
CFR	0-99-4992	RES 49.9K OHM 1/4W 1% MF	2	MAIN	R 38, 64	
CFR	0-99-5001	RES 5K LINEAR TRIM POT	2	MAIN	[VR 1, 2	
CFR	0-99-7682	RES 7.68K OHM 1/4W 1% MF	3	MAIN	R 39, 40, 66	
CFR	0-99-9092	RES 9.09K OHM 1/4W 1% MF	1	MAIN	R 65	
CON	4-10-0007	CON BINDING POST A4, A8	1		Final Assembly	REPLACED BY 9-96-1259 ASSY.
CON	4-10-0007	CON BINDING POST A4, A8	1			
CON	4-98-0003	STRIP BARRIER (5-POS) DT-55-B-14N-05	1	MAIN	J5	
CON	4-98-0004	TAB FASTON 1/4" (AMP 62650-1)	22	FAN	P1-22	
HDR	4-15-2002	HEADER 2-PIN SIL 0.1 SPC LOCKING (AMP 640456-2)	1	FAN	J22	
HDR	4-15-2003	HEADER 3-PIN SIL 2MM CTR (SHROUDED)	4	MAIN	J 1, 12, 14, 15	
HDR	4-15-2003	HEADER 3-PIN SIL 2MM CTR (SHROUDED)	2	OUTPUT M	J19, 21	
HDR	4-15-1002	HEADER 2-PIN SIL 2mm SPC (shrouded)	4	MAIN	J 3, 9, 10, 13	
HDR	4-15-1002	HEADER 2-PIN SIL 2mm SPC (shrouded)	1	OUTPUT M	J20	
HDR	4-15-1006	HEADER 6-PIN SIL 2MM CTR (SHROUDED)	1	MAIN	J16	
HDR	4-15-1006	HEADER 6-PIN SIL 2MM CTR (SHROUDED)	1	CONTROL	J 17	
HDR	4-15-1008	HEADER 8-PIN SIL 2MM CTR (SHROUDED)	2	MAIN	J 2, 8	
HDR	4-15-1008	HEADER 8-PIN SIL 2MM CTR (SHROUDED)	1	CONTROL	J 18	
HDR	4-15-1014	HEADER 14 PIN SIL 2mm SHROUDED	1	FAN	J23	
HDR	4-99-0026	HEADER 26-PIN DIL .100 SPC	1	MAIN	J6	
HDW	5-00-0076	SCREW 6-32 x 3/8 TAP TIGHT THREAD ROLLING PAN HEAD TROX BLK	11		COVER AND MTG 8	
HDW	5-00-0077	SCREW 10-32 x 5/16 TAP TIGHT THREAD ROLLING PAN HEAD TROX BLK	5		TRANSFORMER MTG AND AC GND	
HDW	5-00-0078	SCREW 6-32 x 1/2 TAP TIGHT THREAD ROLLING PAN HEAD TROX ZINC	1		BINDING POST	
HDW	5-00-0079	SCREW 10-32 x 7/8 TAP TIGHT THREAD ROLLING PAN HEAD TROX ZINC	1		BRIDGE RECTIFIER	
HDW	5-00-0085	SCREW 8-32 x 1/2 #6 PH TAPTITE TORX BLACK OXIDE W/WAX	4		HEATSINK ASSY/TRANSISTOR CLAMP	
HDW	5-00-0086	SCREW M3 x 6MM PPZ MACHINE	4		COMBO CONNECTOR	
HDW	5-00-0088	SCRW,6-32x3/8 PPH THRD LNGR CAD	1		REAR PANEL	
HDW	5-00-2006	SCREW, JACK, 3/16 X 1/4	2		REAR PANEL	
HDW	5-01-0020	WASHER #10 FLAT SPLIT RING	1		AC GROUND SCREW	
HDW	5-01-0022	RING RETAINING F/P A4/A8	5		FRONT PANEL FASTENER	
HDW	5-02-0005	STANDOFF,.400,24AWG,PVC TUBING	4		E AND C LEADS OF Q31,Q36	
HDW	5-04-0016	FASTENER STUD RECEIVER (PUSH-ON)	10			
HDW	5-04-0017	SPACER LED (LTM-480)	3	CONTROL	DS 1-3	
HDW	5-04-0018	WASHER #10 FLAT BRASS	1		BRIDGE RECTIFIER	
HDW	5-04-0019	WASHER .140 ID x .375 OD x .047 VFP	2		PCB MTG SPACERS	
HDW	5-04-0022	SPACER #10 x .125	1			
HDW	5-04-0023	INSULATOR TO220 SIL-PAD A4/A8	4	MAIN	ADD TO THERMALLOY HEATSINK	
HDW	5-05-0001	CLIP STRAIN RELIEF HEYCO 1207	1		Power cord	
HDW	5-07-0005	SPACER PCB 5/16 x 1/4 NYLON (RICHCO SSRS-8-4-01)	3	MAIN	MIG 1-3	
HDW	5-07-0005	SPACER PCB 5/16 x 1/4 NYLON (RICHCO SSRS-8-4-01)	3	OUTPUT	MIG 5-7	
IC	2-22-1339	IC LMT339N QUAD COMP (MOT)	1	FAN	U5	
JAC	4-05-0007	JACK XLR + 1/4" FEMALE	2	MAIN	J 4, 11	
LED	3-99-0001	LED RED HIGH EFF (LED TECH LT5241R)	2	CONTROL	DS 1,3	
LED	3-99-0002	LED GREEN (LED TECH LT5221)	1	CONTROL	DS 2	
LIT	7-51-1107	MANUAL REFERENCE A4/A8	1		LITERATURE PACK	
Group	Part.Number	Description	Qty	PCB	Ref.Designator	Comment
LIT	7-53-0001	STICKER BUMPER	1		-	
ME	7-03-0006	BRIDGE CM3502 35AMP/200V	1		BR1	
ME	7-06-0004	RELAY SPST 901CS-DC12	2	FAN	K1,2	Relay MUST be 'C'-config

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ME	7-06-0008	CIRCUIT BREAKER 28-YO1A-12	1			
	7-00-0000		1	MAIN		
	7-00-0010		1			
	7 10 0020	EAN DO STADIEY	1			
IVIE	7-10-0029				FAN I	
ME	7-20-0015		2	OUTPUTM		
MIS	5-04-0000	INSULATOR, RECTIFIER 1.250X1.250.200 HOLE	1		BRIDGE RECTIFIER	
MIS	5-04-1018	INSULATOR XFMR BRACKET	2		TRANSFORMER MOUNTING	
MIS	7-70-0001	FISH PAPER 6x5	1			
MIS	7-70-0006	FISH PAPER 10.0 A4	1		CHASSIS	
MIS	7-70-0008	FISH PAPER 1.5 x 9 A4	1		COVER	
MIS	7-70-0010	INSULATOR, FELT DISC375 DIA. X .032	3		COVER	
MIS	7-90-0007	TWIST TIE, PLASTC WIRE 7"	1			
MIS	9-23-1058	INSULATOR FOAM A4, A8	1			
MTL	9-03-1145	CHASSIS A4	1			
MTL	9-03-1147	COVER TOP A4	1		Top Assembly	
MTL	9-03-1149	BRACKET TRANSFORMER A4/A8	1		Final Assembly	
MTL	9-03-1151	CLAMP TRANSISTOR A4/A8	2		Module Assembly	
MTL	9-03-1152	HEATSINK EXTRUSION 150 inch stick (REV C.)	8			
MTI	9-03-1154	HEATSINK A4	1		Module assembly	
MTL	9-03-1156		4	ΜΔΙΝ	HS 1-A	
MTL	9-03-1150		4	IV/AUN	113 1-4	
MTL	0.02.1164		4			
DIO	9-03-1104		44			
PLS	5-10-1008	THE WRAP 3.250 BLACK PLASTIC RICHU (WIT-18SF-BK)	14			
PLS	9-15-0040	KNOB 35MM PA	2		Final Assembly	
PLS	9-15-0095	INSULATOR K6 A4	2		Module Assembly	
PLS	9-15-1189	PANEL FRONT A4, A8	1		Final assembly	
PLS	9-15-1190	LABEL A4 F/P LOGO	1		Chassis assembly	
PLS	9-15-1194	BLOCK BINDING POST A4,A8	1			
POT	0-09-1037	POT 5K SINGLE W/RIGHT ANGLE LEADS	2	CONTROL	VR 3,4	
RES	0-00-0000	RES 0 OHM 1/8W 5%	1			
RUB	9-23-1056	FASTENER FAN (A4 A8)	4	FAN		
RUB	9-23-1057	FEET RUBBER .30 x .81 BLK (3M SJ5023)	4		Packing Assembly	
SWT	6-01-0002	SWITCH SLIDE DPDT	1	MAIN	S1	
SWT	6-02-1500	SWITCH SPST 16A POWER 1500H11E	1		S2	
TRN	2-03-0006	TRANS MPSA06RLRA	4	MAIN	Q 1, 2, 7, 20	
TRN	2-03-0006	TRANS MPSA06RLRA	2	OUTPUT M	Q31, 36	
TRN	2-03-0006	TRANS MPSA06RI RA	4	FAN	Q40, 41, 42, 45	
TRN	2-03-0056	TRANS MPSA56RI RA	2	MAIN	Q 5, 18	
TRN	2-03-0650	TRANS MPS650RI BA	2	MAIN	0 10 23	
TRN	2-03-0650	TRANS MPS650RI RA	1	FAN	043	
TDN	2.02.0750		4	MAIN	0.6 11 10 24	
	2-03-0750		4	EAN	040, 11, 19, 24	
TDN	2-03-0750	TRANS MIES/JURERA	6		030 30 32 35 37 39	
TDN	2-03-1193	TRANS MJL21193	6			
TRN	2-03-1194	TRANS MJL21194	0	MAIN	000.04	
TDN	2-03-1302	TRANS MJL1302A	2		[Q33, 34	
TRN	2-03-3281	TRANS MJL3281A	2	MAIN	U 15, 16	
TRN	2-04-1837	TRANS 2SA1837	2	MAIN	Q 9, 22	
TRN	2-07-4793	TRANS 2SC4793	2	MAIN	Q 13, 26	
WIR	4-19-1404	WIRE 3.75" BLK W/AMP CRIMP CONS	3	MAIN	A, D, J	
WIR	4-19-1405	WIRE 3.25" WHT W/AMP CRIMP CONS	1	MAIN	BGND-GNDB	
WIR	4-19-1407	WIRE 13" GRN W/AMP CRIMP CONS	1			
WIR	4-19-1408	WIRE 13" GREY W/AMP CRIMP CONS	1			
WIR	4-19-1413	WIRE 18.5" GREY W/AMP CRIMP CONS	1	OUTPUT	SPKR B	
WIR	4-19-1414	WIRE 13" GRN W/AMP CRIMP CONS (REV. B)	1	OUTPUT	SPKR A	
WIR	4-19-1415	WIRE 17" RED W/AMP CRIMP CONS	1	MAIN	B+	
WIR	4-19-1416	WIRE 14" BLK W/AMP CRIMP CONS	2			1
WIR	4-19-1419	WIRE 17" BLK W/ AMP CRIMP CONNS	1	MAIN	B-	
WIR	4-19-1420	WIRE 4" BLUE W/ AMP CRIMP CONNS	7	MAIN	BCEEHKAGND-GNDA	
WIR	4-19-1421	WIRE 13" WHITE WAMP CRIMP ON	1	MAIN	IGNDCT	1
Groun	Port Number	Description	0.54	PCP	Bof Designator	Commont
Group	2.00.0021		4	FOD		Comment
	2-99-0031		1	FAN		
	2-99-5532	IG NEDDJZAN DUAL OPAMP (FF)	3	MAIN	U 1-3	
	2-99-7815	REG MC17815C1 +15V TO220 (MOT)	1	FAN	04	
	9-23-1068	FOAM PAD TRANSFORMER A4	1			1

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<u>4.10 A8</u>	4.10 A8 Service Parts List							
Group	Part.Number	Description	Qtv	PCB	Ref.Designator	Comments		
ASV	7-40-1120	TRANSFORMER 1201/ A8	2					
ASV	9-79-0115		1					
AGY	0.70.0117		1					
ASV	0.70.0119		1	-				
	9-79-0110		1					
AGT	0.06.1250		1					
	1 19 1676		2		I INAL ASSI			
CAR	4-10-1070		1					
CAR	4-10-1077		1					
CAR	4-10-1077		1	MAIN	11 114 (BED)			
CAB	4-19-1757		1	IV/AIIN	12 to 118 (grav)			
CAR	4-13-17.57		1		122 TO 10 (glay)			
CAR	4-13-1750		1		112 110 (VEL CON DUTE)			
CAB	4=13=17.33							
CAB	4-13-1700							
CAB	4-13-1701		1		JIGGET (BRN, RED, ORANGE)			
CAR	7 41 0006		1					
CEC	1 00 0010		1	EAN	C45			
	1.00.0100	CAP 100P ELEC 33V 20%		FAIN	C45			
CFC	1.00.0101		2	IVIAIIN				
CEC	1 00 0101	CAD 1000 25V 20 /0 MUSE	4	EAN	C40, C50	·		
CFC	1.00.0102	CAP 1000F 25V 20% MUSE			C49, C50			
	1.00.0102	CAP 0.10F 100V 5% FILM	14		09, 011, 014, 016-20, 025, 026, 026, 050, 055, 057, 056, 040			
	1.00.0102	CAP 0.10F 100V 5% FILM	- 2	FAIN	C44, C52			
	1-99-0103	CAP .010F 200V 20% XCAP		IVIAIIN	010			
	1-99-0103	CAP .010F 250V 20% XCAP		FAN	004.04			
	1-99-0104		4	MAIN	021-24			
CFC	1-99-0220	[CAP 22PF 100V 5% NPO MC	4	MAIN	[C10, C12, C29, C31			
	1-99-0221		2					
	1-99-0221		2		041, 042			
	1-99-0221	CAP 2200F ELEC 25V 20%	2	FAN				
CFC	1-99-1200	CAP 1200PF 100V 5% FILM	4	MAIN	08, 013, 027, 032			
CFC	1-99-2200	ICAP 22000F ELEC 25V 20%	1	FAN				
CFC	1-99-3300	ICAP 3300PF 100V 5% FILM	6	MAIN	C1, C4, C15, C34, C36, C51			
	2-99-0021		4	MAIN	CR3, CR5, CR10, CR12			
CFD	2-99-1/5/	DIODE ZENER IN/57A (9.1V)	2	MAIN				
	2-99-4003		2	FAN				
CFD	2-99-4148	DIODE SIGNAL 1N4148	8	MAIN	CR6-9, CR13-16			
CED	2-99-4148	DIODE SIGNAL 1N4148	1	FAN	CR17, CR19, CR20, CR22-25			
CFD	2-99-5400	DIODE POWER INStan	1	FAN				
	2-02-5352	DIODE 1N5352BRL 15V 5W 5%	2	MAIN	CR1, CR2			
CFR	0-99-0010	IRES 10 OHM 1/4W 5% CF	4	MAIN	R35, R42, R75, R103			
CFR	0-99-0010	IRES 10 OHM 1/4W 5% CF	1	FAN	R142			
CFR	0-99-0011	IRES 10 OHM 3W 5% MO	2	MAIN	R64, R66			
CFR	0-99-0012	IRES 1.2 OHM 1/2W 5% MO	10	MAIN	R27, R29, R56, R58, R61, R68, R71, R74, R99, R101			
	0-99-0012	RES 1.2 OHM 1/2W 5% MU	10		R105, R107, R109, R112, R115, R120, R123, R125, R127, R129			
	0-99-0020	RES 20 OHM 5W 5% WW	1	FAN	R132			
	0-99-0027	RES 2.7 OHM 3W 5% MU	2	MAIN	R05, R07			
CFR	0-99-0040	IRES 40 OHM 5W 5% WIRE WOUND	1	FAN	R130			
CFR	0-99-0100	IRES 100 OHM 1W 5% MO	2	MAIN	R9, R11			
CFR	0-99-0102	IRES 1K OHM 10W 5% W.W. FORMED	2	MAIN	R25, R50			
CFR	0-99-0103	IRES 10K 1/4W 1% MF	8	MAIN	R3, R6, R16, R19, R40, R53, R84, R95			
CFR	0-99-0104	RES 10K 1/4W 5% CF	2	MAIN	R12, R13			
CFR	0-99-0104	RES 10K 1/4W 5% CF	10	FAN	[R134, R139-141, R144, R148-152			
CFR	0-99-0120	IRES 120 OHM 5W 5% WW	1	FAN	[K13]			
CFR	0-99-0202	RES 2K OHM 1/4W 5% CF	2	MAIN	[K22, K26			
CFR	0-99-0223	RES 22K 1/4W 5% CF	4	FAN	[R146, R147, R153, R154			
CFR	0-99-0330	RES 330 OHM 1/4W 5% MO	4	MAIN	R60, R63, R70, R73			
CFR	0-99-0330	RES 330 OHM 1/4W 5% MO	4	OUTPUT M	K110, K113, K118, K121			
CFR	0-99-0511	RES 51.1 OHM 1/4W 1% MF	6	MAIN	R7, R20, R33, R45, R78, R88			
CFR	0-99-0511	IRES 51.1 OHM 1/4W 1% MF	2	OUTPUT M	[R116, R117			
CFR	0-99-0593	RES 59K 1/4W 1% MF	4	MAIN	K39, K41, K83, R85			
Group	Part.Number	Description	Qty	PCB	Ref.Designator	Comments		

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CFR	0-99-0752	RES 7.5K OHM 1/2W 5% CF	2	MAIN	R54, R96	
CFR	0-99-1000	RES 1K OHM 1/4W 1% MF	8	MAIN	R32, R44, R47, R52, R77, R87, R90, R94	
CFR	0-99-1000	RES 1K OHM 1/4W 1% MF	1	FAN	R145	· · · · · · · · · · · · · · · · · · ·
CER	0-99-1001	RES 1K OHM 1/2W 5% CE	1	MAIN	R10	
CER	0-99-1001	RES 1K OHM 1/2W 5% CF	1	FAN	R143	
CER	0.00.1500	PES 1 5K OHM 1/4W 5% CE	2	MAIN	P51 P02	
CER	0.00.1500			EAN	D129	
CFR	0-99-1500	RES 1.5K OHM 1/4W 5% CF	1	FAN	R138	
CFR	0-99-2210	RES 2.21K OHM 1/4W 1% MO	4	MAIN	R31, R43, R76, R86	
CFR	0-99-3033	RES 0.33 OHM 1/4W 5% METAL OXIDE (FLAMEPROOF)	2	MAIN	R23, R24	
CFR	0-99-3300	RES 3.3K 1/4W 5% CF	2	MAIN	R55, R97	
CFR	0-99-3300	RES 3.3K 1/4W 5% CF	1	FAN	R135	
CFR	0-99-3303	RES 330K 1/4W 5% CF	3	FAN	R133, R136, R137	
CFR	0-99-4990	RES 4.99K 1/4W 1% CF	8	MAIN	R1, R2, R4, R5, R14, R15, R17, R18	
CFR	0-99-4991	RES 499 OHM 1/4W 1% MF	8	MAIN	R8, R21, R48, R49, R91, R92, R155, R156	
CFR	0-99-4992	RES 49.9K OHM 1/4W 1% MF	2	MAIN	R36, R80	
CFR	0-99-5001	RES 5K LINEAR TRIM POT	2	MAIN	VR1, VR2	
CFR	0-99-7682	RES 7.68K OHM 1/4W 1% MF	3	MAIN	R37, R38, R82	
CFR	0-99-9092	RES 9.09K OHM 1/4W 1% MF	1	MAIN	R81	
CON	4-10-0007	CON BINDING POST A4, A8	1			
CON	4-10-0007	CON BINDING POST A4, A8	1			
CON	4-98-0003	STRIP BARRIER (5-POS) DT-55-B-14N-05	1	MAIN	J5	
CON	4-98-0004	TAB EASTON 1/4" (AMP 62650-1)	25	FAN	P1-25	
HDR	4-15-2002	HEADER 2-PIN SIL 0.1 SPC LOCKING (AMP 640456-2)	1	FAN		
HDR	4-15-2002	HEADER 3-PIN SIL 2MM CTR (SHROLIDED)	4	MAIN	11 112 114 116	
HDR	4-15-2003	HEADER 3-PIN SIL 2MM CTR (SHROUDED)	2		110 121	·
	4-10-2003	HEADER 3-FIN SIL 2MM CTR (SHROUDED)	2		J 19, J21	
	4-15-1002	HEADER 2-PIN SIL 2000 STIOUDEU	4		13, 39, 310, 313	
HDR	4-15-1002	HEADER 2-PIN SIL 2mm SPC (shrouded)	1	DICPLAY	J 20	
HDR	4-15-1006	HEADER 6-PIN SIL 2MM CTR (SHROUDED)	1	DISPLAY	J1/	
HDR	4-15-1006	HEADER 6-PIN SIL 2MM CTR (SHROUDED)	1	MAIN	J15	
HDR	4-15-1008	HEADER 8-PIN SIL 2MM CTR (SHROUDED)	1	DISPLAY	J 18	
HDR	4-15-1008	HEADER 8-PIN SIL 2MM CTR (SHROUDED)	2	MAIN	J2, J8	
HDR	4-15-1014	HEADER 14 PIN SIL 2mm SHROUDED	1	FAN	J23	
HDR	4-99-0026	HEADER 26-PIN DIL .100 SPC	1	MAIN	J6	
HDW	5-00-0076	SCREW 6-32 x 3/8 TAP TIGHT THREAD ROLLING PAN HEAD TROX BLK	13		MTG 8 AND COVER	
HDW	5-00-0077	SCREW 10-32 x 5/16 TAP TIGHT THREAD ROLLING PAN HEAD TROX BLK	10		TRANSFORMER MOUNTING/AC GND	
HDW	5-00-0078	SCREW 6-32 x 1/2 TAP TIGHT THREAD ROLLING PAN HEAD TROX ZINC	1		BINDING POST BLOCK	
HDW	5-00-0079	SCREW 10-32 x 7/8 TAP TIGHT THREAD ROLLING PAN HEAD TROX ZINC	1		BRIDGE RECT.	
HDW	5-00-0085	SCREW 8-32 x 1/2 #6 PH TAPTITE TORX BLACK OXIDE W/WAX	6		TRANSISTOR CLAMP	
HDW	5-00-0086	SCREW M3 x 6MM PPZ MACHINE	4		XLR CONNECTOR	
HDW	5-00-0088	SCRW,6-32x3/8 PPH THRD LNGR CAD	1		Rear panel	
HDW	5-00-2006	SCREW, JACK, 3/16 X 1/4	2		Rear panel	
HDW	5-01-0020	WASHER #10 FLAT SPLIT RING	1		AC ground screw	
HDW	5-01-0022	RING RETAINING F/P A4/A8	5		FRONT PANEL FASTENER	
HDW	5-02-0005	STANDOFF, 400, 24AWG, PVC TUBING	4	OUTPUT	E AND C LEADS Q35, Q44	
HDW	5-04-0016	FASTENER STUD RECEIVER (PUSH-ON)	5			
HDW	5-04-0017	SPACER LED (LTM-480)	3	DISP.	DS 1.2.3	
HDW	5-04-0018	WASHER #10 FLAT BRASS	2		BRIDGE RECTIFIER	
HDW	5-04-0019	WASHER . 140 ID x . 375 OD x .047 VEP	2		PCB MOUNTING SPACER	
HDW	5-04-0023	INSULATOR TO220 SIL-PAD A4/A8	4		APPLY TO Q7, Q11, Q28, Q32	
HDW	5-05-0001	CLIP STRAIN RELIEF HEYCO 1207	1			
HDW	5-07-0005	SPACER PCB 5/16 x 1/4 NYL ON (BICHCO SSRS-8-4-01)	10	MAIN	MTG1-7, MTG9-11	
IC	2-22-1339		1	FAN		
10	4.05.0007		2	MAIN	IA 111	
JAC	3 00 0001		2		DE 1.2	
	3 00 0002				DS 1, 5	
	7 51 1107			DIGFLAT	552	
	7-01-1107					
ME	7-03-0006		1	EAN	K1 K2	
ME	7-00-0004		4	FAN	N I, NZ	
ME	7-06-0010	BREAKER THERMAL CUTOUT 80 DEG.O.O.R.		MAIN		
ME	7-06-0011	BREAKER THERMAL CUTOUT 55 DEG. C.O.R.		OUTPUT M	THZ	
ME	7-06-0012	CIRCUIT BREAKER 28-XQ1A-20				
ME	/-10-0029	FAN,DC ST12N6X	1	FAN		
Group	Part.Number	Description	Qty	PCB	Ref.Designator	Comments
ME	7-20-0015	INDUCTOR,AIR CORE 1uH	2	MAIN	L1, L2	
MIS	5-04-0000	INSULATOR, RECTIFIER 1.250X1.250 .200 HOLE	1		Bridge rectifier	

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MIS	5-04-1018	INSULATOR XFMR BRACKET	4			
MIS	7-70-0007	FISH PAPER 5.7 x 14.0 A8	1		CHASSIS	
MIS	7-70-0009	FISH PAPER 1.5 x 13 A8	1		TOP COVER	
MIS	7-70-0010	INSULATOR, FELT DISC375 DIA. X .032	3		Cover	
MTL	9-03-1146	CHASSIS A8	1			
MTL	9-03-1148	COVER TOP A8	1			
MTL	9-03-1149	BRACKET TRANSFORMER A4/A8	2			
MTL	9-03-1151	CLAMP TRANSISTOR A4/A8	3		HEATSINK ASSEMBLY	
MTL	9-03-1152	HEATSINK EXTRUSION,150 inch stick (REV C.)	12			
MTL	9-03-1155	HEATSINK A8	1			
MTL	9-03-1156	HEATSINK THM7022B-MT	4	MAIN	HS1-4	
MTL	9-03-1157	CLIP HEAT SINK CLP-201	4			
MTL	9-03-1157	CLIP HEAT SINK CLP-201	4			
MTL	9-03-1164	HEATSINK RECTIFIER 3 x 1.250 x .125	1			
PLS	9-15-0040	KNOB 35MM PA	2			
PLS	9-15-0096	INSULATOR K6 A8	2			
PLS	9-15-1189	PANEL FRONT A4, A8	1			
PLS	9-15-1194	BLOCK BINDING POST A4,A8	1			
POT	0-09-1037	POT 5K SINGLE W/RIGHT ANGLE LEADS	2	DISPLAY	VR 3,4	
RES	0-99-0033	RES .33 OHM 3W 5%	10	MAIN	R28, R30, R57, R59, R62, R69, R72, R98, R100, R102	
RES	0-99-0033	RES .33 OHM 3W 5%	10	OUTPUT M	R104, R106, R108, R111, R114, R119, R122, R124, R126, R128	
RUB	9-23-1056	FASTENER FAN (A4 A8)	4	FAN		
RUB	9-23-1057	FEET RUBBER .30 x .81 BLK (3M SJ5023)	4		INFORMATION PACK	
SWT	6-01-0002	SWITCH SLIDE DPDT	1	MAIN	S1	
SWT	6-02-1500	SWITCH SPST 16A POWER 1500H11E	1		S2	
TRN	2-03-0006	TRANS MPSA06RLRA	4	MAIN	Q1, Q2, Q4, Q25	
TRN	2-03-0006	TRANS MPSA06RLRA	2	OUTPUT M	Q35, Q44	
TRN	2-03-0006	TRANS MPSA06RLRA	4	FAN	Q47, Q48, Q50, Q52	
TRN	2-03-0056	TRANS MPSA56RLRA	2	MAIN	Q3, Q24	
TRN	2-03-0650	TRANS MPS650RLRA	2	MAIN	Q8, Q29	
TRN	2-03-0650	TRANS MPS650RLRA	1	FAN	Q51	
TRN	2-03-0750	TRANS MPS750RLRA	4	MAIN	Q5, Q9, Q26, Q30	
TRN	2-03-0750	TRANS MPS750RLRA	1	FAN	Q49	
TRN	2-03-1193	TRANS MJL21193	10	OUTPUT M	Q33, Q34, Q36-38, Q41-43, Q45, Q46	
TRN	2-03-1194	TRANS MJL21194	10	MAIN	Q12-16, 19-23	
TRN	2-03-1302	TRANS MJL1302A	2	OUTPUT	Q39, Q40	
TRN	2-03-3281	TRANS MJL3281A	2	MAIN	Q17, Q18	
TRN	2-04-1837	TRANS 2SA1837	2	MAIN	Q7, Q28	
TRN	2-07-4793	TRANS 2SC4793	2	MAIN	Q11, Q32	
	2-99-0031	IC TIP31A NPN (FF)	1	FAN	Q306	
	2-99-5532	IC NE5532AN DUAL OPAMP (FF)	3	MAIN	U1-3	
	2-99-7815	REG MCT7815CT +15V TO220 (MOT)	1	FAN	U 5	
	9-23-1067	FOAM PAD TRANSFORMER A4	1			

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