# "TRADER" SERVICE SHEET

ESIGNED with access for servicing in view, the K.-B. GR15 chassis can be slipped out of its cabinet in the space of a minute, and the layout then gives ready access to all parts. The receiver is a 4-valve (plus rectifier) 3-band superhet operating from A.C. or D.C. mains of 200-250 V, 50-100 c/s. The waveband ranges are: 16.3-51 m, 187-535 m and 740-2100 m 740-2,100 m.

740-2,100 m. The small differences between the GR15 and its associated models, DR15, ER15 and FR15 are explained under "Associated Models" overleaf. This Service Sheet was prepared from a GR15. Release dates and original prices: GR15, August 1951, £19 5s 2d; FR15, August 1950, £16 9s; ER15, August 1949, £16 is 3d; DR15, October 1948. £16 is 3d. Purchase tax extra.

## CIRCUIT DESCRIPTION

Aerial input via L1 (S.W.) and bottom capacitance coupler C4 (M.W. and L.W.) to single-tuned circuits L2, C35 (S.W.), L3, C35 (M.W.) or L4, C35 (L.W.) which precede triode hexodevalve (V1, Brimar 12K8GT) operating as frequency changer with internal coupling. C1, C2 isolate the aerial and earth sockets. R1, R2 prevent the build-up of static charges on the aerial, and R3 shunts the aerial input to prevent modulation hum.

Oscillator grid coils L5 (S.W.), L6 (M.W.) and L7 (L.W.) are tuned by C36. Parallel trimming by C37 (S.W.), C38 (M.W.) and C39 (L.W.); series tracking by C12 (M.W.), C12, C13 (L.W.). Second valve (V2, Brimar 12K7GT) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C6, L9, L10, C7 and C18, L11, L12, C19. Intermediate frequency 470 ke/s.

Diode signal detector is part of double diode triode valve (V3, Brimar 12Q7GT). Audio frequency component in rectified output is developed across load resistor R14 and passed via volume control R15 and C24 to grid of triode section which operates as A.F. amplifier.

(Continued Col. 1 overleaf)

and associated Models DR15, ER15 and FR15

### **COMPONENTS AND VALUES**

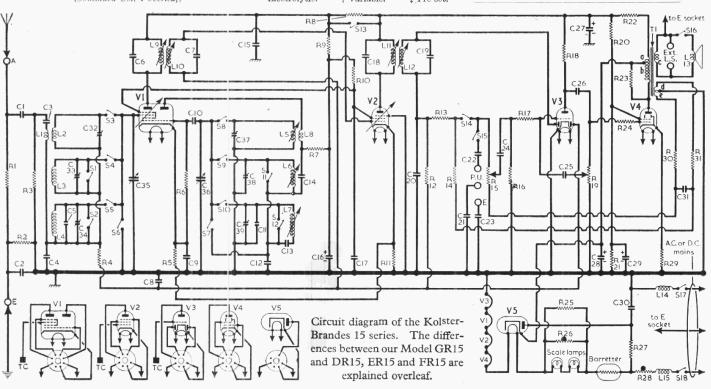
	CAPACITORS	Values	Loca- tions
C1	Aerial and earth	0·001μF	G4
C2	isolators	$0.01 \mu F$	F4
C3	April apprilar	$0.005 \mu F$	G4
C4	Aerial couplers {	$0.003 \mu F$	G3
C5	L.W. aerial trim.	25 pF	G4
C6	$\begin{cases} 1st \text{ I.F. trans. tun-} \\ ing & \dots \end{cases}$	$200 \mathrm{pF}$	A1
C7	∫ ing }	$200 \mathrm{pF}$	A1
C8	A.G.C. decoupling	$0.02\mu\mathrm{F}$	F4
C9	V1 cath, by pass	$0.1 \mu F$	F4
C10	V1 osc, C.G	$100 \mathrm{pF}$	F3
C11	L.W. osc, trim	$20 \mathrm{pF}$	F4
C12	M.W. osc. tracker	330pF	F4
C13	L.W. osc. tracker	$200 \mathrm{pF}$	F4
C14	Reaction coupling	$200 \mathrm{pF}$	F4
C15	} H.T. decoupling {	$0.02 \mu F$	F3
C16*	H.T. decoupling	$8\mu F$	E4
C17	S.G. decoupling	$0.02 \mu \mathrm{F}$	F3
C18	2nd I.F. trans.	$200 \mathrm{pF}$	B1
C19	$\begin{cases} 2nd I.F. trans. \\ tuning \end{cases}$	$200 \mathrm{pF}$	B1
C20	I.F. by-pass	$100 \mathrm{pF}$	F3
C21		$0.02 \mu F$	F4
C22	P.U. isolators {	$0.005 \mu F$	F4
C23		$0.01 \mu F$	F4
C24	A.F. coupling	$0.005 \mu F$	D3
C25	Part tone control	$100 \mathrm{pF}$	D3
C26	A.F. coupling	$0.02 \mu F$	E4
C27*	} H.T. smoothing {	$24 \mu F$	D4
C28*	)	$16\mu F$	D4
C29*	V4 S.G. decoup	$4\mu F$	E4
C30	Mains R.F. filter	$0.01 \mu F$	E3
C31	Neg. feed-back	$0.25 \mu F$	E3
C32‡	S.W. aerial trim	$40 \mathrm{pF}$	G4
C33‡	M.W. aerial trim	$40 \mathrm{pF}$	G4
C34‡	L.W. aerial trim,	$40 \mathrm{pF}$	G4
C35†	Aerial tuning		A2
C36†	Oscillator tuning	-	A1
C37‡	S.W. osc, trim	40 pF	G4
C38‡	M.W. osc. trim	40 pF	G4
C39‡	L.W. osc, trim	80 pF	G4



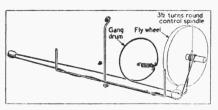


The appearance of the K-B GR15.

	RESISTORS	Values	Loca- tions
R1	} Anti-static leaks {	1MΩ	G4
R2	1)	$470 \mathrm{k}\Omega$	G4
R3	Mod. hum shunt	$1k\Omega$	G4
R4	A.G.C. decoupling	$100 \mathrm{k}\Omega$	G4
R5	V1 G.B	$100\Omega$	F3
R6	V1 osc. C.G	$47 \mathrm{k}\Omega$	F4
R7	Osc. anode feed	$10 \mathrm{k}\Omega$	F4
R8	Radio muting	$10 \mathrm{k}\Omega$	G3
R9	H.T. feed	$2.2 \mathrm{k}\Omega$	F3
R10	S.G. H.T. feed	$4.7 \mathrm{k}\Omega$	F3
R11	V2 G.B	$47\Omega$	F3
R12	A.G.C. decoupling	$-2.2 \mathrm{M}\Omega$	F3
R13	I.F. stopper	$47 \mathrm{k}\Omega$	F3
R14	Signal diode load	$2.2 \mathrm{M}\Omega$	<b>E</b> 3
R15	Volume control	$500 \mathrm{k}\Omega$	C1
R16	V3 C.G	$10M\Omega$	D3
R17	V3 C.G. stopper	$100 \mathrm{k}\Omega$	D3
R18	V3 anode load	$470 \text{k}\Omega$	E4
R19	Tone control	$500 k\Omega$	D3
R20		$6.8 k\Omega$	E4
R21	V4 S.G. pot.	$10k\Omega$	E3
R22	H.T. smoothing	$1.5 \text{k}\Omega$	E3
R23	No-load limiter	$47k\Omega$	E3
R24	V4 C.G. stopper	47kΩ	E4
R25	Scale lamp shunt	$680\Omega$	E3
R26	Brimistor CZ3		E3
R27	V5 surge limiter	$150\Omega$	E3
R28	Brimistor CZ3	10022	E3
R29	V4 cath, G.B	180Ω	E4
R30	)	$240\Omega$	E3
R31	Neg. feed back {	240Ω 1kΩ	E3



OT	HER COMPONENTS	Approx. Values (ohms)	Loca- tions
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13	S.W. aerial coup  Aerial tuning coils  Oscillator tuning coils Osc. reaction coup.  1st I.F. trans. { Pri. Sec. Pri. Speech coil  O.P. trans. { a b c d e e	2:96 21:06 3:06 8:47 5:2 5:2 5:2 5:2 5:2 10:0 380:0 0:35 1:7	G4 G4 G4 G4 F4 F4 F4 A1 A1 B1 B1
\$15 \$16 \$17 \$18	Waveband switches Speaker switch Mains s.w., g'd R19		G3 D4 D3



Sketch of the tuning drive cord system.

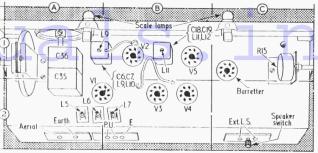
Circuit Description—continued
D.C. potential developed across R14 is fed back as bias to V1 and V2 giving automatic gain control. The A.G.C. line is connected to the second diode anode, which prevents it from going positive.

gain control. The A.G. line is connected across the second diode anode, which prevents it from going positive.

Resistance-capacitance coupling by R18, C26 and R19 between V3 triode and beam tetrode output valve (V4, Brimar 35L6GT). Variable tone control by negative feed-back via R19, C25 between V3 and V4 control grid circuits. The voltage developed in a third winding d, e on T1 is fed back in anti-phase via a balanced bridge circuit formed by the two halves of the winding, R14, R15, R30 and R31, thus ensuring that no negative feed-back voltage is applied to C20 and to the detector diode, which is connected across the zero potential corners of the bridge, while a portion of the available feed back, that across section e of the feed-back winding, is applied to V3 grid. Provision is made for the connection of a low impedance external speaker across speech coil winding c on T1.

## GENERAL NOTES

Switches.—\$1-\$12 are the waveband switches, and \$13-\$15 are the radio/gram change-over switches, ganged in two rotary units beneath the chassis. These are indicated in our underside view of the chassis, and shown in detail in the diagrams inset beside the plan view, where they are drawn as seen from the rear of an inverted chassis.



The table below them gives the switch position for the four control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed.

Scale Lamps.—These are two M.E.S.-type lamps, with large clear spherical bulbs, rated at 4.5 V, 0.15 A. They are shunted by R25 and a type C23 Brimistor R26.

External Speaker.—Two sockets are provided at the rear of the chassis on a panel with S16 for the connection of a low impedance (about 2.4 Ω) external speaker.

Drive Cord Replacement.—About 4ft 6in of high-grade flax fishing line is required for a new drive cord, which leaves an ample margin for tying off. It should be run as shown in, the accompanying sketch, where the system is shown as seen from the front right-hand corner of the chassis, neglecting obstructions.

Associated Models.—The electrical differences in the FR15 as compared with the GR15 conconsist of the omission of C5, C11 and R25. In the ER15, there are additional differences: R5 becomes 300Ω and goes directly to chassis, while R11 is omitted; C15 and R24 may be omitted and C9 is 0.02 μP. The DR15 is like the ER15, but it has a 0.004 μF S.W. osc. tracker; also C6, C7, C18 and C19 are 150 pF, while C8 is 0.1 μF.

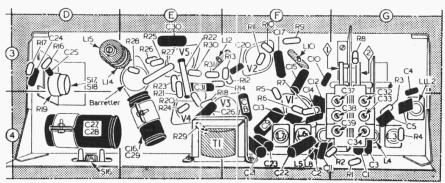
### VALVE ANALYSIS

Valve voltages and currents given in the table below are those measured in our receiver when it was operating from 230 V A.C. mains. The receiver was tuned to the high wavelength end of M.W. with the volume control set to maximum, but there was no signal input.

Voltage readings were measured with an Avo Electronic Testmeter, and as this instrument has a very high internal impedance, allowance should be made for the greater current drawn by other types of meter. Chassis was the negative connection.

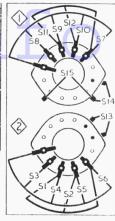
Valve	And	ode	Ser	een	Cath.
vaive	V	mA	V	mA	V
V1 12K8GT	$\begin{cases} 160 \\ \text{Oscil} \\ 105 \end{cases}$	$\left\{\begin{array}{c} 2\cdot2\\ \text{lator}\\ 2\cdot8 \end{array}\right\}$	100	6.5	2.2
V2~12K7GT	160	7.9	100	2.5	1.0
$V3\ 12Q7GT$	53	0.25			
V4~35L6GT	200	35.0	95	9.0	6.3
V5~35Z4GT	195†				215.0

† A.C.reading.



Underside view of the chassis. Switch units 1, 2 are detailed at the head of col. 3.

Plan Above:chassis drawing. Right: Waveband switch unit diagrams.



Switches	Gram	L.W.	M.W.	S.W.
S1				С
S2			C	Č
S3				Ċ
84			С	
S5		C		
86	C			
S7	С			
88		-		C
S9			С	
S10		С		
811		-		С
S12		-	С	č
S13		C	Č	č
S14		C	C	Č
S15	С	-		

# CIRCUIT ALIGNMENT

Remove chassis from cabinet and stand it on

Remove chassis from cabinet and stand it on its volume control end on the bench.

1.F. Stages.—Connect output of signal generator, via an O.1.µF capacitor in each lead, to control grid (top cap) of V1 and chassis. Switch receiver to M.W., and turn gang to maximum. Feed in a 470 kc/s (638.3 m) signal and adjust the cores of L12, L11, L10 and L9 (location references E3, B1, F3, A1) for maximum output. Repeat these adjustments.

R.F. and Oscillator Stages.—Transfer signal generator leads, via a dummy aerial to A and E sockets. As the tuning scale remains fixed in the cabinet when the chassis is withdrawn reference must be made to the calibration marks printed on the scale backing plate. If calibration marks are not provided they should be measured out on the backing plate as follows. First of all a datum line should be drawn 2½ in to the right of the rivet in the middle of the scale backing plate (viewed from front). The calibration marks are then measured off to the left of the datum line, starting with 50 m (0.19in), 500 m (1.08in), 1,714 m (1.47in), 20 m (3.63in), 860 m (3.72in) and 214 m (3.815in). M.W.—Switch receiver to M.W., tune to 214 m

M.W.-Switch receiver to M.W., tune to 214 m M.W.—Switch receiver to M.W., tune to 219 in mark, feed in a 214 m (1,400 kc/s) signal and adjust C38 (G4) and C33 (G4) for maximum output. Tune receiver to 500 m mark, feed in a 500 m (600 kc/s) signal and adjust the core of L6 (A2) for maximum output. Repeat these adjustments until no further improvement results. results.

-Switch receiver to L.W., tune to 860 m

L.W.—Switch receiver to L.W., tune to 860 m mark, feed in an 860 m (350 kc/s) signal and adjust C39 (G4) and C34 (G4) for maximum output. Tune receiver to 1,714 m mark, feed in a 1,714 m (175 kc/s) signal and adjust the core of L7 (B2) for maximum output. Repeat these operations until no further improvement results. S.W.—Switch receiver to S.W., tune to 20 m mark, feed in a 20 m (15 Mc/s) signal and adjust C37 (G3) and C32 (G3) for maximum output, rocking the gang while adjusting C32 for optimum results. Tune receiver to 50 m mark, feed in a 50 m (6 Mc/s) signal and adjust the core of L5 (A2) for maximum output. Repeat these adjustments until no further improvement results. results.

Sensitivity.—Overall sensitivity should be better than 250  $\mu V$  for 50 mW output on all