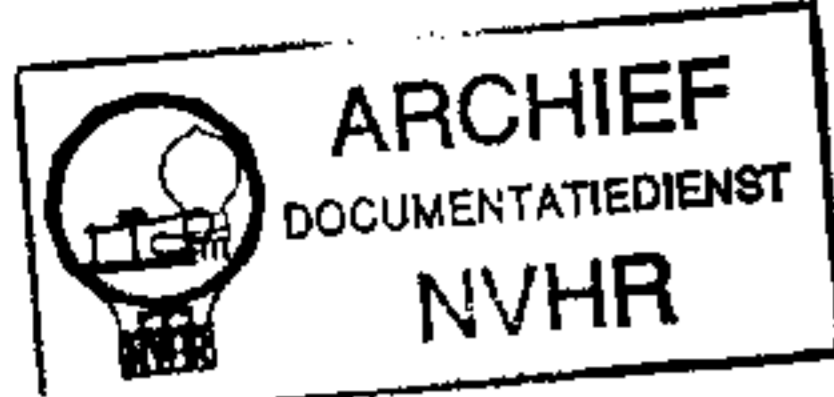


Ned. Ver. v. Historie v/d Radio



**S**EVEN transistors and a diode comprise the semiconductor complement of the KB Cobra and RGD Rover radio receivers. The outstanding features of these being modular construction of the circuit, a collector-bend a.m. detector operated in the common-emitter mode and bandspread on the medium waveband.

Three modules are used, r.f./mixer, i.f. amplifier and audio amplifier respectively, connection to each assembly being via multi-way connectors and p.v.c. insulated leads.



Transistor Table

Transistor	Emitter (V)	Base (V)	Collector (V)
TXm1	AF117	0.87	0.97
TXk1	AF117	1.58	1.66
TXk2	OC70	—	4.15
TXa1	AC127	4.15	0.6
TXa2	AC128	0.45	0.6
TXa3	AC128	4.7†	4.9
TXa4	AC127	4.7†	4.5

† Measured at the junction of Ra12 and Ra13. Quiescent current 15mA.

A ferrite rod internal aerial is used for reception on the m.w.1. (275-555m), m.w.2. (185-280m) and l.w. (1,333-1,900m) bands. An external socket provides for the connection of a car type aerial, while a second switched socket allows the output to be fed to an earphone for private listening, or a tape recorder input.

A transformerless four-transistor directly-coupled audio amplifier provides 400mW of audio power to a 5in 10Ω loudspeaker.

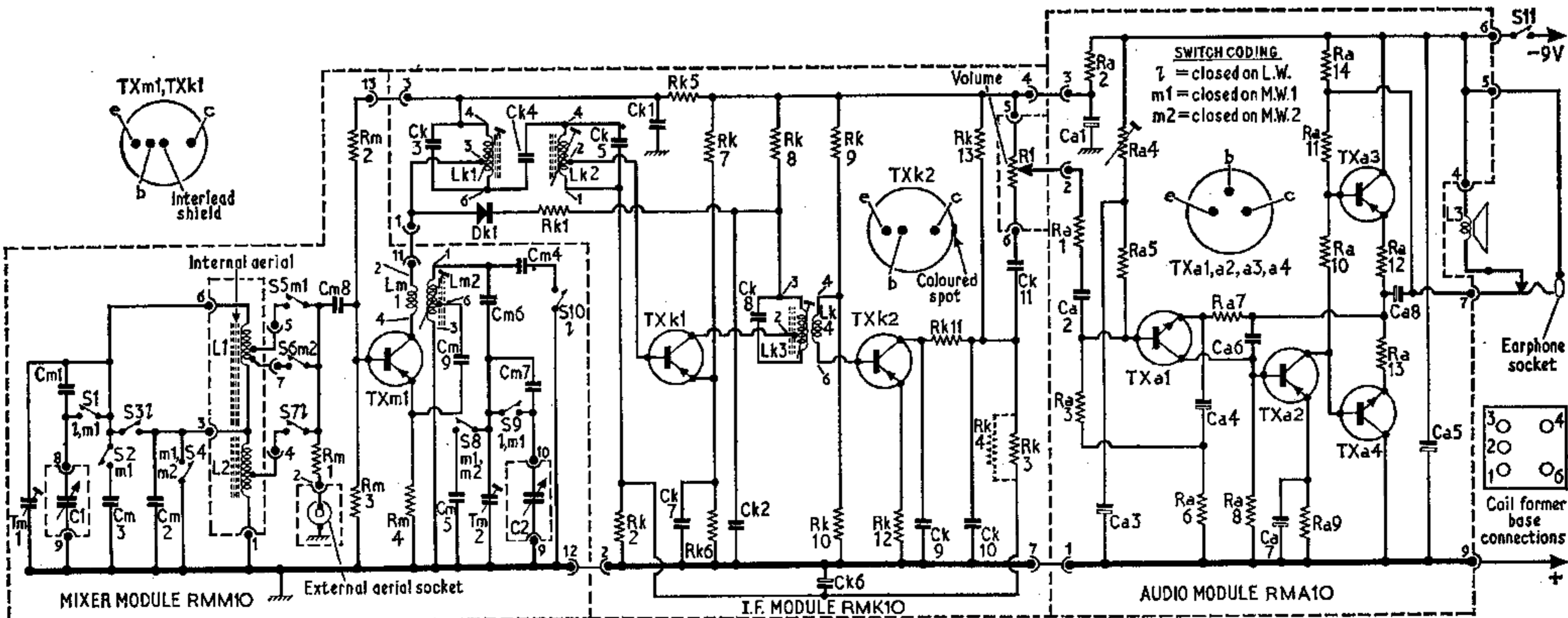
The power supply for the receiver is obtained from a 9V dry battery (Ever Ready PP7 or equivalent).

**TRANSISTOR ANALYSIS**

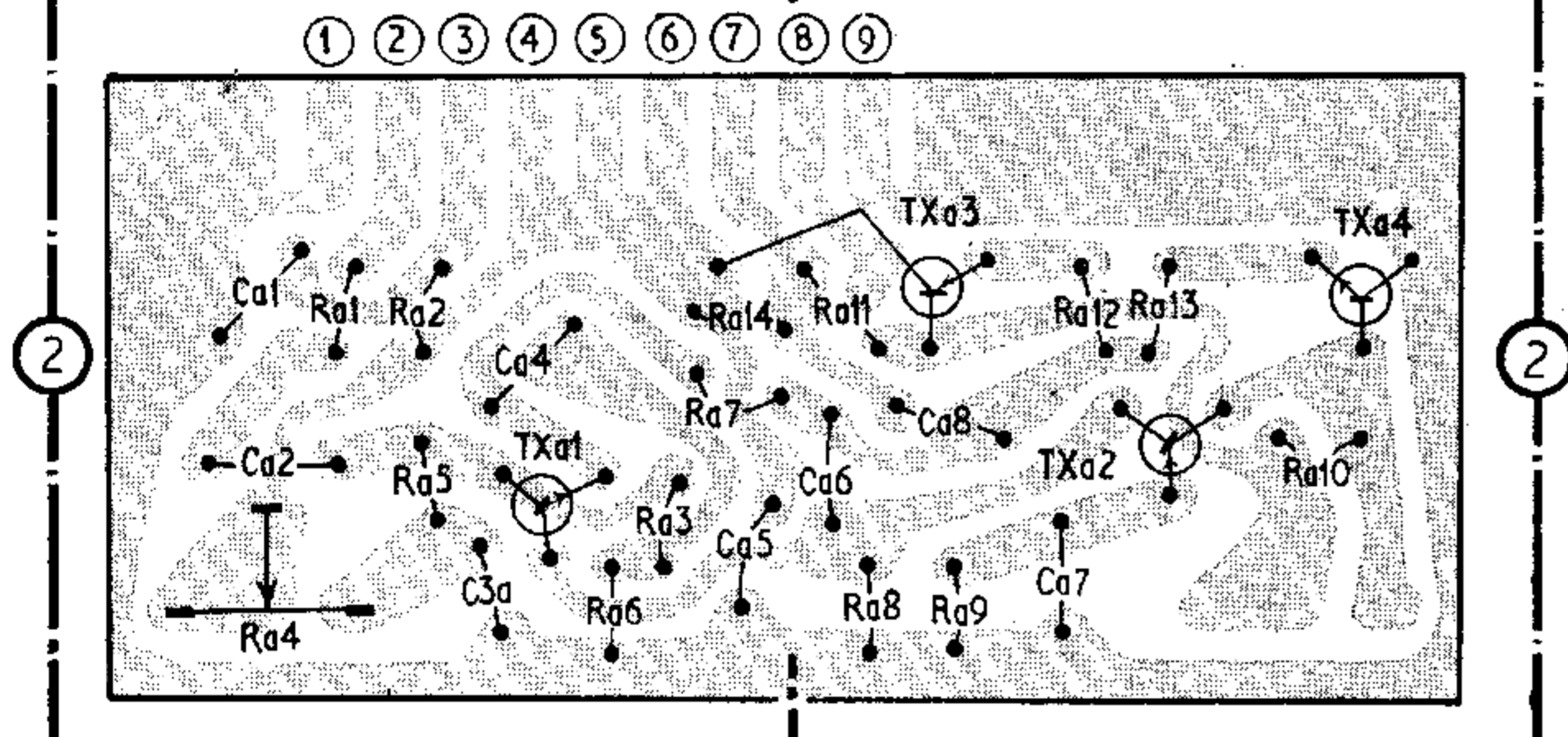
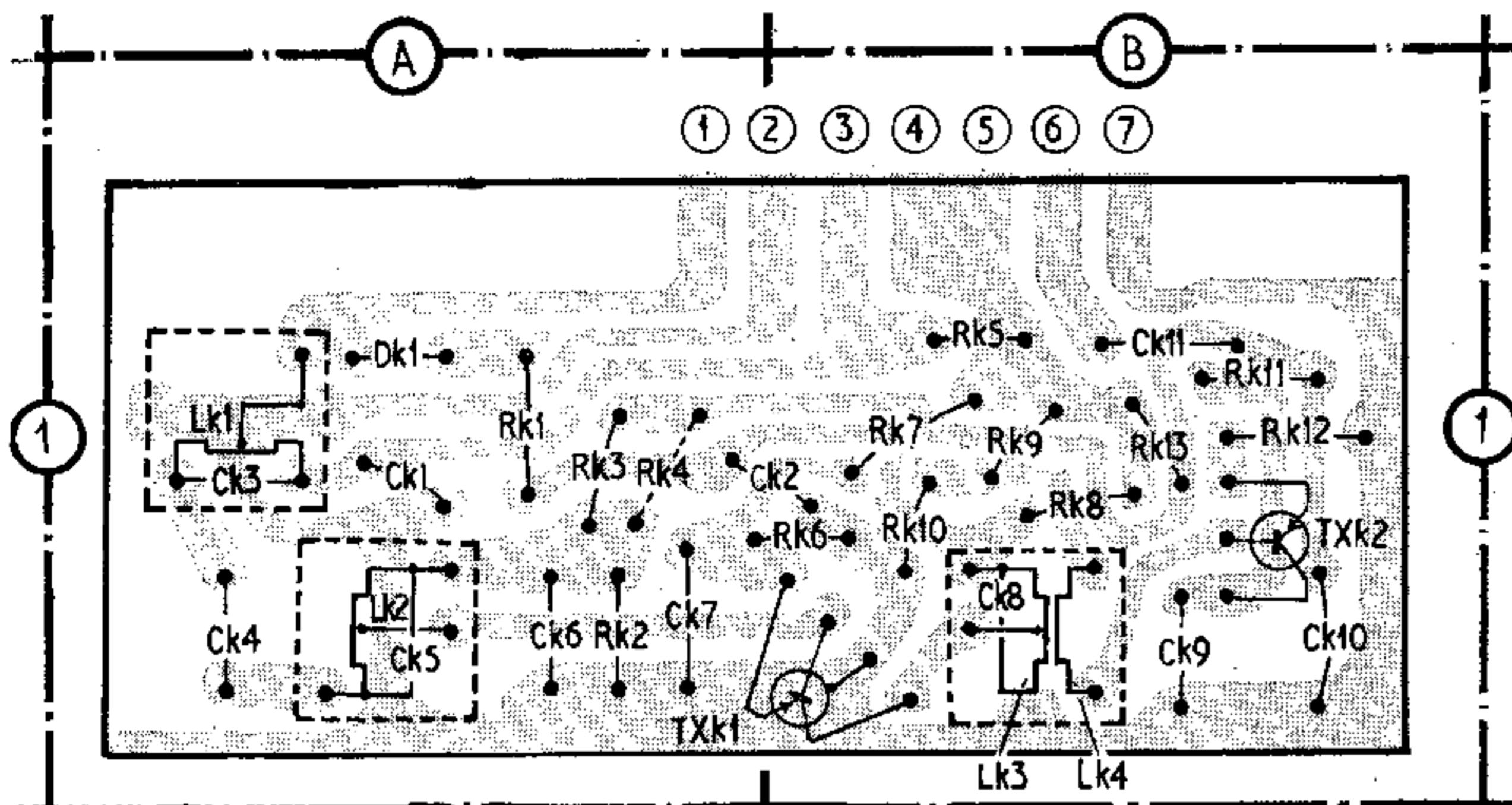
Transistor voltages given in the table Col. 1 were taken from information supplied by the manufacturers. They were measured on a 20,000Ω/V meter and are negative with respect to battery positive.

Resistors		Capacitors		Coils and Transformers*	
R1	20kΩ	D4		Ca2	0.22μF
Rm1	1kΩ	C3		Ca3	50μF
Rm2	39kΩ	C3		Ca4	320μF
Rm3	6.8kΩ	C3		Ca5	160μF
Rm4	1kΩ	C3		Ca6	1,800pF
Rk1	680Ω	A1		Ca7	100μF
Rk2	12kΩ	A1		Ca8	320μF
Rk3	15kΩ	A1		<b>Miscellaneous</b>	
Rk4	15kΩ	A1		S1-S10	—
Rk5	100Ω	B1		S11	—
Rk6	330Ω	B1		Dk1	CG64H
Rk7	4.7kΩ	B1		* Approximate d.c. resistance in ohms.	
Rk8	820Ω	B1			
Rk9	47kΩ	B1			
Rk10	100Ω	B1			
Rk11	100Ω	B1			
Rk12	270Ω	B1			
Rk13	18kΩ	B1			
Ra1	10kΩ	A2			
Ra2	180Ω	A2			
Ra3	12kΩ	A2			
Ra4	10kΩ	A2			
Ra5	10kΩ	A2			
Ra6	10Ω	A2			
Ra7	1kΩ	A2			
Ra8	1kΩ	B2			
Ra9	68Ω	B2			
Ra10	47Ω	B2			
Ra11	620Ω	B2			
Ra12	2.2Ω	B2			
Ra13	2.2Ω	B2			
Ra14	390Ω	A2			
C1	166pF	D4			
C2	166pF	D4			
Cm1	49pF	C3			
Cm2	35pF	C3			
Cm3	23pF	C3			
Cm4	175pF	C3			
Cm5	23pF	C3			
Cm6	190pF	C3			
Cm7	49pF	C3			
Cm8	0.047μF	C3			
Cm9	0.02μF	C3			
Tm1	30pF	C3			
Tm2	30pF	C3			
Ck1	0.047μF	A1			
Ck2	0.047μF	B1			
Ck3	250pF	A1			
Ck4	2.7pF	A1			
Ck5	250pF	A1			
Ck6	25μF	A1			
Ck7	0.47μF	A1			
Ck8	250pF	B1			
Ck9	2,200pF	B1			
Ck10	4,700pF	B1			
Ck11	0.22μF	B1			
Ca1	160μF	A2			

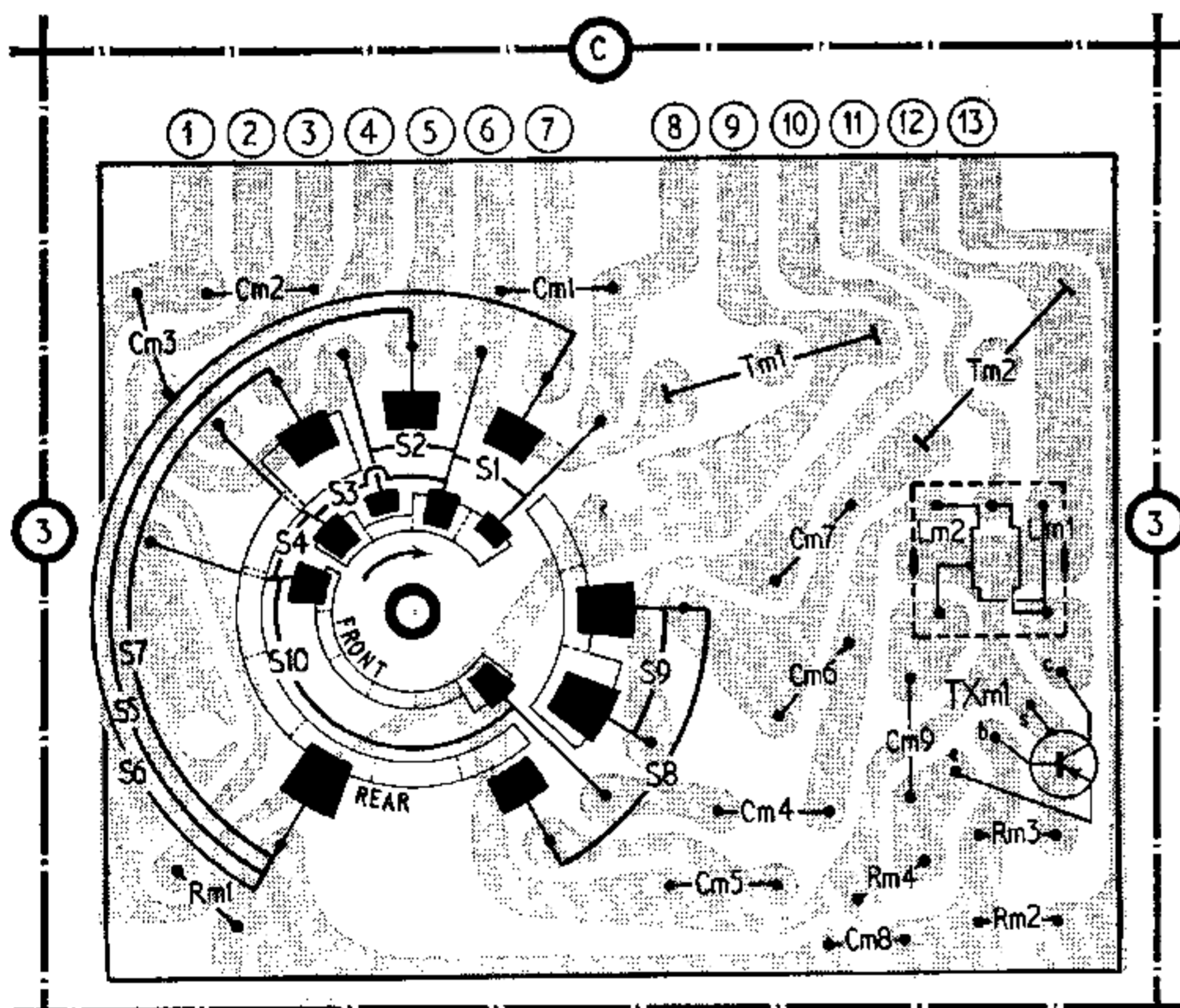
(Continued overleaf col. 1)



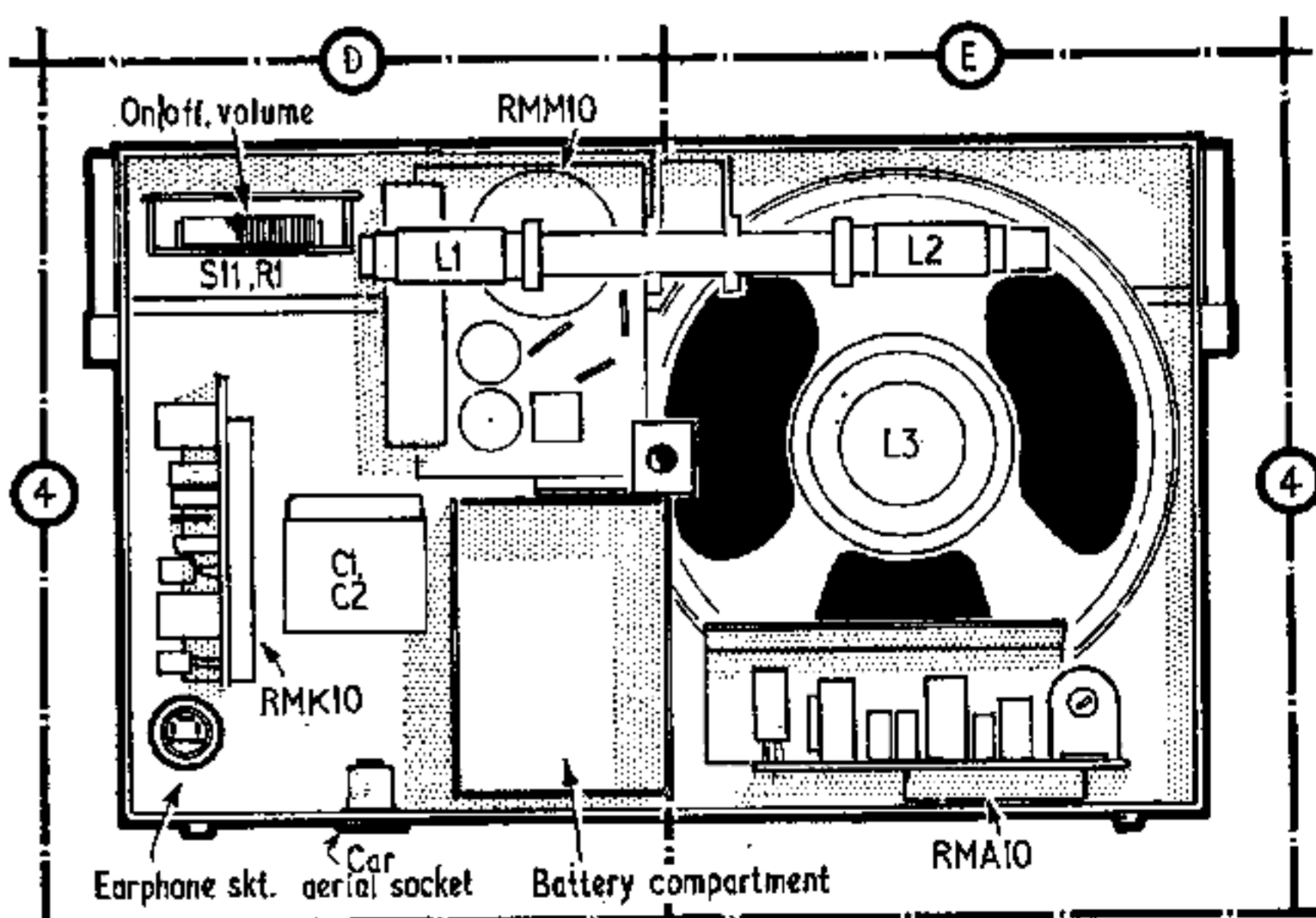
Circuit diagram of the KB KRO21 and RGD RR221.



Above: The i.f. and a.f. printed panels.



Below: General view with the back cover removed. Left: The r.f. printed panel and waveband switch details.



- 3.—Connect the signal generator to the test coil and position the coil co-axially with the ferrite rod and 5in from the m.w. end (L1 end). Switch receiver to m.w.1. and tune to 500m. Feed in a 600kc/s signal and adjust Lm2 and L1 for maximum output.
- 4.—Switch receiver to m.w.2. and tune to 200m. Feed in a 1,500kc/s signal and adjust Tm2 and Tm1 for maximum output.
- 5.—Repeat operations 3 and 4 in the order given, for optimum results.
- 6.—Switch receiver to l.w. Feed in a 225kc/s signal and accurately tune receiver to this signal then adjust L2 for maximum output.

**MANUFACTURERS SERVICE DEPARTMENT**

Combined Radio & Television Service Limited  
Regent Works, Foots Cray, Sidcup, Kent  
(Telephone 01-300 3333)

**CIRCUIT NOTES**

The demodulator circuit employed in this receiver incorporates a transistor TXk2 operated in the common-emitter mode and biased towards cut-off. Operated in this condition the transistor is used as a collector-bend detector, analogous to an anode-bend detector when using a valve.

A potential divider Rk9, Rk10 is used to provide d.c. stabilization and the value of the emitter resistor Rk12 is chosen to give the required value of collector and emitter current. The value of the emitter current is particularly important for rectification and, in fact, its value must be a compromise between two conflicting requirements.

On the one hand, in order to provide efficient rectification the emitter-base function must be biased to a point on the dynamic characteristic where the curve has a sharp knee; at this point, the emitter current is reduced to a low level.

On the other hand, the transistor is expected to provide some audio gain, and as an audio amplifier the transistor emitter current should be of the order of 1mA.

**Circuit Alignment—continued**

Adjust the signal generator attenuator to obtain 400mW output (indicated on output meter), then adjust Ra4, together with the signal generator attenuator for equal clipping of the displayed waveform.

Disconnect the a.f. signal generator and oscilloscope.

**Alignment Procedure.**—All r.f. and i.f. measurements are to be made with an a.m. signal modulated to a depth of 30 per cent at 1kc/s. The signal input

should be progressively attenuated with increasing sensitivity so as to maintain an output of approximately 50mW with the volume control at maximum.

1.—Switch receiver to m.w.2. and rotate tuning gang to maximum capacitance. Connect audio output meter in place of loudspeaker (if not already connected).

2.—Connect the signal generator via the 0.1μF capacitor to the base of mixer/oscillator TXa1, or via car aerial socket, whichever is more convenient. Feed in a 470kc/s a.m. signal and adjust

The potential difference across Rk13 under quiescent conditions is approximately 3.75V. When an input signal is applied, the mean collector current rises thereby increasing the potential difference across Rk13. The collector potential will therefore become less negative as the magnitude of the applied signal increases, and this variation of potential is fed back to TXk1 as a.g.c. bias.

Because the emitter current (in this application) is much smaller than is usual with a common-emitter configuration, the input resistance is therefore much higher and does not impose excessive damping on the tuned circuit feeding it.

Components Ck9, Rk11 and Ck10 comprise the normal i.f. filter network and the audio signal component developed across Rk13 is fed via Ck11 (d.c. blocking) to the top of the volume control R1.