

SOLID STATE POWER AMPLIFIER

M-6000

SERVICE MANUAL

Emitter Follower Circuit

Output signals of a control amplifier etc. are led to the input terminals (MAIN IN) of this power amp, and level-controlled at the input level control of a detent volume equivalent to the high-grade attenuator with 22 contact-points of 1dB decrement.

Then fed into the Emitter Follower circuit, which is, unlike the ordinary one, composed by two transistors Q601 and Q602. The former is for emitter follower and the latter is for the constant current drive of the emitter follower of Q601. Signals are impedance-converted through this circuit, and therefore electrical isolation is made between the output stage of a control amp and the pre-driver circuit of this amplifier to eliminate interference between both circuits. Thus stable amplification with low distortion is attained.

Pre-Driver Circuit

Signals converted into low impedance at emitter follower circuit are then fed to the two-stage differential amplifier, a kind of balanced DC amplifying circuit, to meet voltage amplification. The differential amplifier is always stable against the fluctuation of mains voltage and temperature drift, and has been adopted widely in computers or measurement instruments etc. by means of IC's as Operational Amplifier.

The two transistors Q301, Q302 for the 1st stage differential amplifier are arranged quite symmetrically, and the emitter of the both transistors are connected to (+) power supply through a common resistor. The base of Q301 accepts the input signal, while that of Q302 accepts the feed back signal. Due to adoption of two transistors of the same characteristic, equivalent collector current and emitter current are available when the same signals are fed to the base of the both transistors. As emitter current for two pieces of resistors will flow through the emitter resistor, the emitter potential will rise up, which corresponds to the amount of negative feedback. On the other hand, if subtle (+) potential may appear at the speaker terminal by the drift of transistors caused by other factors but signals, e.g., the raise up of temperature, this (+) potential is led to the base of Q302 via the feedback circuit, when (+) signal of the same phase will appear at the emitter resistor. In this case, the potential at the emitter resistor varies to (+), which reduces the collector current to have (-) potential at collector. The voltage is amplified by the 2nd differential amplifier Q303, Q304, which makes the (+) potential stable at the speaker terminals, and helps keep balanced 0 potential.

The 2nd differential amplifier operates same as the 1st one, though not perfectly symmetrical. The constant current driven by Q305 is applied, since this stage aims at voltage amplification. The emitter follower circuit is arranged annexed to the differential amplifier with a pair of Q306 and Q307 which electrically isolates the "Class A" operation at the differential stage and the "Class B" operation at the power amp stage. (Q306 is for the emitter follower and Q307 is for its constant current driving.). Therefore, impedance fluctuation caused by the speaker loads would not affect the pre-driver stage. With this pre-driver circuit, stable driving with low distortion is feasible up to high frequency range with a slighter phase compensation comparing with conventional high power amplifiers.

As for the power supply circuit for the "Class A" operation sections up to the differential stage, a real automatic voltage regulator is adopted to avoid bad influence which may possibly be caused by the fluctuation of AC mains voltage or the current fluctuation in the power amplifier section.

Power Output Circuit

Adopted is a pure complementary push-pull circuit composed by the power transistors of NPN group and PNP group which are all specially developed for LUXMAN. In order to produce such a high power of 300W/ch, two parallel triple push-pull stages utilizing 12 power transistors designed for high power output are arranged at the final stage. And the parallel push-pull stage utilizing

4 driver transistors which are also exclusive for LUXMAN is arranged at the complementary driver stage. Thus sufficient driving of various type of the speaker systems is feasible.

With the M-6000 the total collector-dissipation of the power transistors in each channel is 900W, and the collector emitter breakdown voltage is 200V. The parallel push-pull connection is also adopted at the complementary driver stage, and therefore the distortion characteristic is improved just in the same way as the final stage.

The power supply for the final stage and the complementary driver stage is quite independent for the left channel and right channel, which ensures the same power output at each channel whether both channels are driven or single channel is driven. But bear in mind that when the full power output is fed into 4-ohm loads, a slight difference may be possible due to the regulation of the commercial electric power.

Bias Circuit

The adjustment of the quiescent current at the final stage is made by a thermal diode and the transistor Q113. These components directly touch the heat sink, and compensates the excessive heat and the temperature drift.

Protection Circuit

The OCL circuit, in which the speaker system is directly connected to the amplifier, is ideal in the point that the input signal is delivered most faithfully. But this circuit is always accompanied by the danger that any abnormal factors aroused in the amplifier will be delivered to the speaker system without barrier. On the other hand, electronic components will increase in number in proportion with improvements of the circuit design, and it is hard to foresee every trouble that may happen, even if the most severe selection is made for the superior components. Necessity is here to have the protection circuits.

The most important in the operation of the protection circuitry is reliability and speed. Therefore the sensitivity should be as high as possible in the range of the safety operation. The protection circuits of the M-6000 have to be designed not to be mis-functioned by the current of music reproduction signal. The block diagram will help you understand the outline of the protection circuits.

For the over-current sensing, the conventional one-point detection of the abnormal current will tend to induce mis-operation. With the M-6000, when two contradictory current conditions are sensed by the comparator, this sensing circuit operates and shuts off the mains power, for example, short-circuited at output - no output signal and a heavy DC current are sensed at the same time. Further, in order to attain more safety, when excessive current, which may break the power transistors, appears, the current is once restrained electronically to keep the operation of the power transistors in the S.O.A. (Safe Operation Area). And in case the restraint time lasts over the certain time, the mains power is shut off by an S.C.R. (Silicon Controlled Rectifier).

Other protection circuits are:

#D.C.-Drift Sensing --- This protects the speaker system by cutting off the output when some $\pm 3V$ is detected at the speaker terminals. This also operates as the muting circuit which safeguards the speaker system from transient phenomena caused by the mains being turned on.

#Power Transistor Failure Sensing --- This shuts off the mains power when even one fuse of any power transistors is ruptured.

#Abnormal High Temperature Sensing --- This shuts off the mains power when the temperature at the heat sink exceeds $100^{\circ}C$ under hard driving for a long time.

Thus the M-6000 is equipped with 4 protection circuits. One is for protection of speaker systems, and the other three are for protection of the amplifier.

V.U. Meter & Peak Indication Circuit

The purpose of the V.U. meter originally was just to show the reproduced signal visually, but today peak meters of high attack-speed and slow recovery etc. have been adopted to display the precise signal level. But the mechanical meters have difficulty to indicate accurately the pulse signals which are usually contained in the musical signals. In this sense the electronic display method is necessary.

Thus the M-6000 is equipped with electronic peak indicator together with the mechanical V.U. meter to make it easy to visually compare the difference between the average level and the peak level. Further ON-OFF switches are available for the operation of the both indicators.

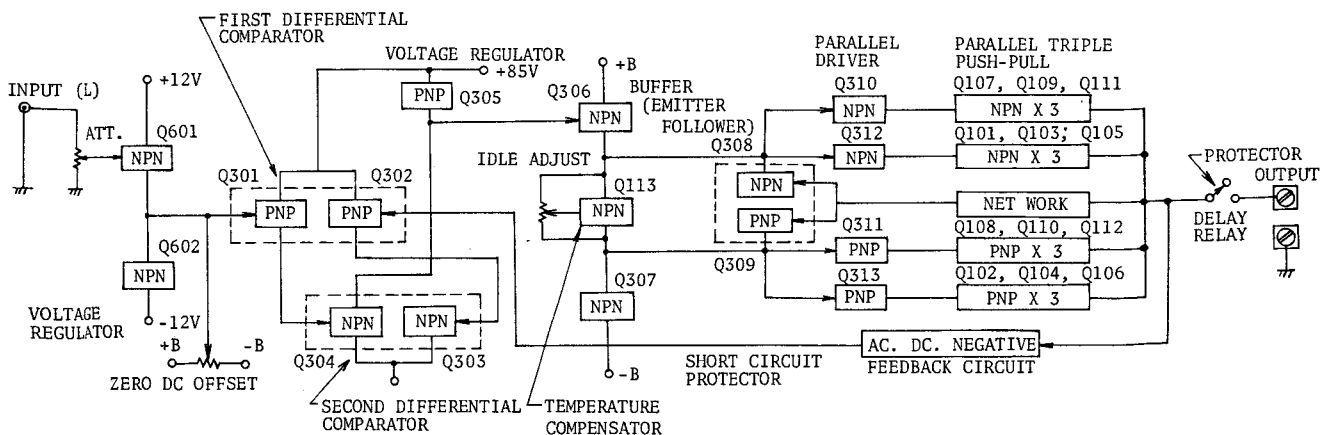
V.U. meter amp circuit, unlike the ordinary V.U. meters in which the needle is directly moved by the detection of signal current, adopts 2 transistors, and the meter is inserted in the NF loop of the meter amp circuit and is driven by constant current. Therefore the scale is made linear and easy-reading is attained.

In the peak indication circuit, after the output signal is detected, the signals flow into the differential Schmitt Circuitry, on which the voltage equivalent to the standard level is given, with a certain retaining time of the peak level, and the indication is made according to the standard level. For the peak indication, Light Emitting Diodes are adopted, which ensures high speed response against the pulsive input signals.

Power Output

The power supply for the output stage of two parallel triple push-pull stage utilizes independent 2 power supplies by adopting separate power transformers for the right channel and the left channel. Therefore, the power output of 300W per channel into 8-ohm loads, 500W per channel into 4-ohm loads is possible.

MODEL: M-6000 BLOCK DIAGRAM



A L I G N M E N T P R O C E D U R E

1) Pilot lamp does not light up.

1. Protector Indicator lights up.

Causes: Power transistor (TO-3 or TO-66) in the Final stage and Driver stage of Class AB operation may be damaged.

Measures:

a) Check whether the damaged TR is in Left channel or Right channel.

For this check, remove the 2 fuses on one channel (right or left), and power switch should be at "on". By this procedure, when the pilot lamp lights up normally, the channel where the 2 fuses remain is free from failure. When the 2 fuses are inserted to the other channel, and if the PROTECTOR LAMP lights, the TR in this channel is damaged.

b) Remove the screws fixing the heat sink of the damaged channel. And remove this heat sink together with the power transistor (TO-3) block carefully from the main chassis. Then remove the fuse on the printed circuit board PB-680A or PB-681A, and check each transistor if short circuit might happen. Replace when damaged.

[Firstly remove plate-like heat sink block with flat-bladed driver through the round hole available at the side of printed circuit board. Then remove the TR fixing screws at the side of heat sink.]

N.B.

As for PB-680/PB-681, 12 power transistors (TO-3) are mounted on one board.

6 transistors of NPN type are arranged at the outer side and 6 transistors of PNP type at the inner side, in the fixed state of the each printed circuit board.

When replacement of the power transistor is finished, all the fuses removed should be set as they were.

Reconstruction procedure may simply be done in the reverse order. But bear in mind that the connector of the printed circuit board is flexible to obtain clearance, therefore ascertain that the connector contacts the chassis, by pressing the connector toward the board from the bottom of the chassis after the heat sink is mounted.

Now the procedure at Final stage has been finished.

Transistor (TO-66) check at Driver Stage

The printed circuit boards are PB-682A and PB-683A located in front of the PCB of final stage. Transistors are Q410, Q412 or Q310, Q312 for NPN type and Q411, Q413 or Q311, Q313 for PNP type, all of which are located in the vicinity of the fuse; outer ones (bottom) are NPN and center one are PNP.

Now all the check for the power transistors of Class AB has been finished. But the following further procedure is advisable before the power switch ON to prevent the breakage caused by omission of each check procedure.

- 1) Set a DC amperemeter between the No1 and No2 terminals of 4P terminal block at the back of the chassis. The current flows from the inner terminal toward the outer one.
- 2) Remove the short-circuited material connected between No1 and No2 as well as NO3 and NO4, by this, quiescent current may be measured.
- 3) Provisionally short-circuit the terminals of the Power Relays respectively with a certain clip or something like that.
- 4) Gradually increase the AC primary voltage.

- 5) When the swing of the Amperemeter falls abruptly near 1A and no more increase could be confirmed, each transistor is operating without failure.

CAUTION: Never try to turn on the power switch with the block of the Final stage kept removed, for instance, with only the PCB of Driver stage mounted. This may break the Driver transistors because the transistor for temperature compensation is on the PCB of Final stage. Therefore when this is disconnected the bias voltage between Base and Base of Driver TR becomes over-rated.

By this check procedure, when the quiescent current is found abnormally increased, short circuit between collector and emitter of the TR for bias compensation. If the amperage would decrease, the failure may be caused by this TR, and not the other TRs. In this occasion, treatment should be done in the same manner as the replacement of the components at Final stage. The collector and the emitter of this TR are connected to (J) and (L) terminal respectively of the center connector in the connector of the board for Final stage.

N.B.

In case (+) power and (-) power are not supplied at the same time (only for Class AB of Final stage), the Protector lamp will light up. Therefore bear it in mind not to forget that the short-circuited material removed should be soldered as it were after measuring quiescent current etc. is finished. Also note that the Protector lamp may light up when the fuse on the board for protection purpose is detached.

Pre-Driver Stage

In case the supply voltage of +85V is not supplied, failure of Driver PCB(PB-682, PB-683) may be suspected. Remove the Driver PCB and check the voltage again. When the rated voltage is not confirmed, transistors etc. on PB-684A may be damaged.

2. Protector Indicator does not light up.

a) Check the voltage at one end of the emitter-resistor (22-ohms) of Q700 and Q701 at AVR section on PB-687A. This is adjusted at 22.5V. When it is different, adjust the collector voltage of this TR, and confirm if the input voltage is available. In case this voltage is normal, check whether the AC switching relay on left channel is switched ----- if the relay operated, left channel is all right.

When left channel operates normally, right channel may be suspected which operates time-delayed. Check Q713 or Q714.

b) When AC relay on left channel is damaged by mal-contact etc, pre-driver voltage will not be supplied to right channel, therefore both channels will not operate.

c) When the muting Relay is damaged, signals will not be available at speaker terminals. In this case, TR's of Q724, Q725 or Q726 may be broken.

3. L.E.D. Indicator or the Swing of V.U. Meter operates abnormally.

These equipments as L.E.D. Indicator or V.U. Meter may be removed by losing the screws on the sub-panel after removing the attenuator knob. Inside the sub-panel housed are the printed circuit boards, namely, PB-688A, PB-689A, PB-690, PB-686A, PB-691A and PB-692A. These printed circuit boards operate as follows:

PB-686A ----- This is an input amplifier and adjust input signals for ATTENUATOR. Emitter-follower circuit is adopted. Gain: 1.

PB-689A ----- Amplifier for the Peak Indicator. As input level varies, so do the printed circuit boards. This means that one PCB of the same name is prepared for an L.E.D. Totally 8 boards are used to operate the whole L.E.D. Peak Indicator. Each board is of interchangeable type, and when found any mal-

function substitute each other. In case lighted-up level found to be varied, check the PCB.

PB-690 ----- This accomodates the Flip-Flop circuit for STAND-BY, First stage amp for L.E.D.

PB-688A----- This is equipped with sockets for level amp for the V.U. Meter and PB-689 A.

PB-691A----- This divides the speaker signal by use of the relay and the precision resistors.

PB-692A----- Each push-switch is mounted on this board. At "VU-PEAK" position, the relay on PB-691A will be operated at the same time.

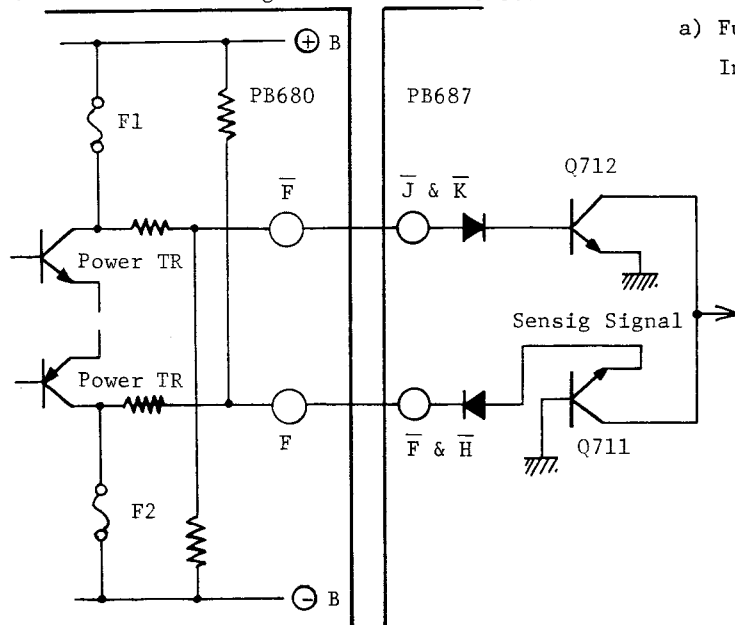
2) Operation of Power Supply Source

Manual turn-on of the power switch (A) makes the constant voltage section for protector operate, which operates each sensing section and at the same time the power switch (B) for the main amp is turned on, and the entire amplifier is put into operational condition. Then the speaker relay (C) is turned on to connect the circuit to speakers after some 5 seconds unless any trouble is detected at each sensing circuit.

In case some troubles are detected in the amplifier to operate any of the sensing circuits 1 - 3, the realy (B) provided at the primary side of the power transformer is instantly turned off to shut off the power supply to the entire amplifier, and the L.E.D. for protector indication lights up. (manual recovery)

When abnormal drift appears at the speaker terminals, the DC-drift sensing circuit is operated to cut off the speakers on load, and the Muting L.E.D. is made blinking continuously. In this case, however, the protector L.E.D. does not light up since the mains power supply is not shut off. (automatic recovery)

a) Fuse-blown Sensing for Power Transistor



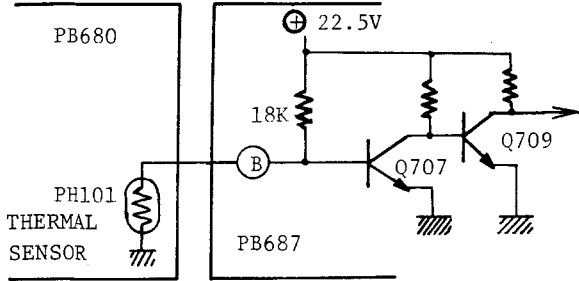
3) Operation of Each Sensing Section

a) Fuse-blown Sensing for Power Transistor

In case the fuse 5A provided to each power transistor is normal, (+) potential is appears at the (k) (J) terminal on PB-687, while (-) potential at the (F-bar) (H-bar) terminal. Therefore Q711 and Q712 are not turned on, and sensing signal is not generated.

If the fuse F1 for NPN power transistor is blown off, (-) potential appears at the (k) (J) terminal, which turns Q712 on. Also when the F2 for PNP power transistor is blown off, (+) potential appears at the (F-bar) (H-bar) terminal, which turns Q711 on. Thus in these cases sensing signal is generated.

b) Thermal Sensing on the Heat Sink



b) Thermal sensing on the Heat Sink

In case the temperature of the heat sink is below 100°C, Q707 is OFF and Q709 is ON since PH101 has sufficiently low resistance, therefore sensing signal is not available.

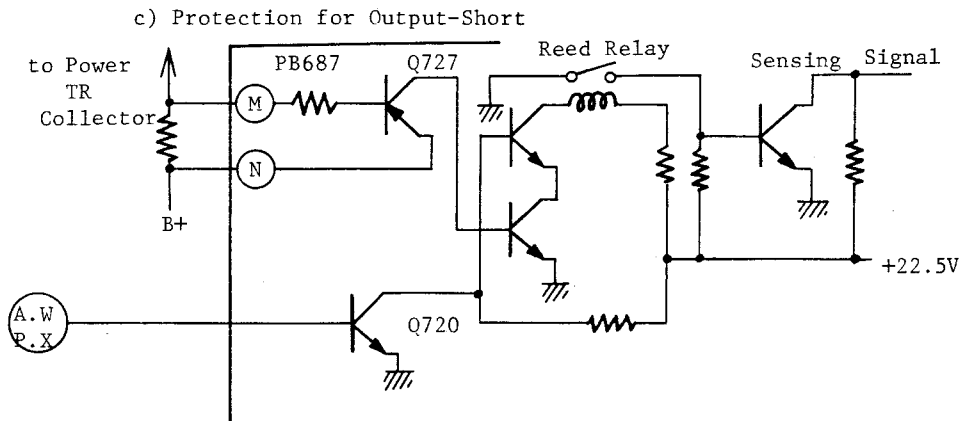
But when it exceeds 100°C, the PH101 is turned to be of high resistance,

which makes Q707 to be ON, and Q709 to be off, and incidentally the sensing signal is generated.

c) Protection for Output-Short

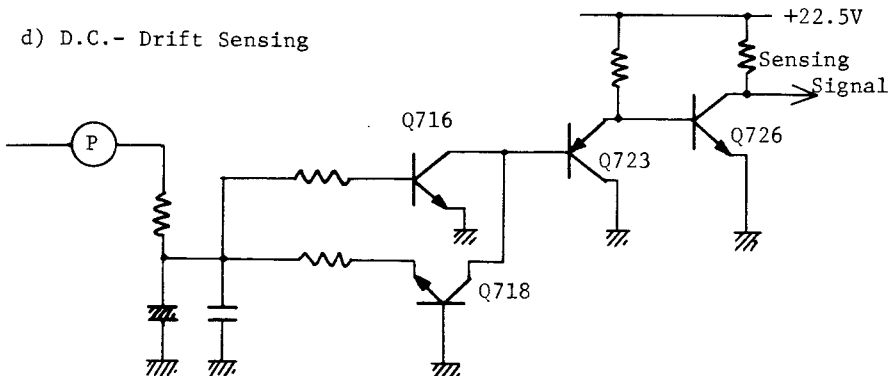
Q727 repeats ON and OFF in accordance with the collector current of the power transistor. Q720 is ON only when the output signal is available at the amplifier output.

Both Q730 and Q731 compare these two states, and generate sensing signal only when large current appears without any music signal at the output terminals. The sensing signal is not generated by such large current as music signals.

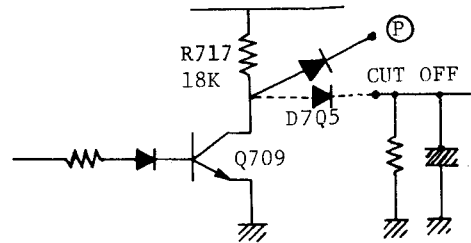


d) DC-Drift Sensing

When the DC-drift appeared at the point P is (+), Q716 is turned ON, while in case the potential is (-), Q718 is turned ON, which turns Q726 OFF. Further +22.5V is generated as the sensing signals.



Protector L.E.D. lights up instantaneously at the time of turning the power switch on.



When PB687 is replaced, normal operation is obtained.

YES

Something wrong with the Amp.
Refer to No. 2.

NO

Remove one end of D705 on PB687
(Regard it as the point P)
Some +22V is available at P.
(See the chart above.)

YES

When Q705 on PB687 is removed, +22V is available at P.

YES

Replace them and then adjust VR700 so as to get +22.5V at the L terminal.
(L terminal is the L of 12P connector on PB687.)

Defective on Q700 - Q703 or on SCR (A - K short-circuited)

NO

+22V is available at P when Q710 is removed with placing Q705 again.

NO

C - E short-circuited on Q706 - Q708 or C - E open-circuited on Q709.

YES

+22V is available at P even when R756 (jumper) on PB687 is cut off.

NO

C - E short-circuited on Q710 - Q712.

YES

+22V is available at P even when R758 (jumper) on PB687 is cut off.

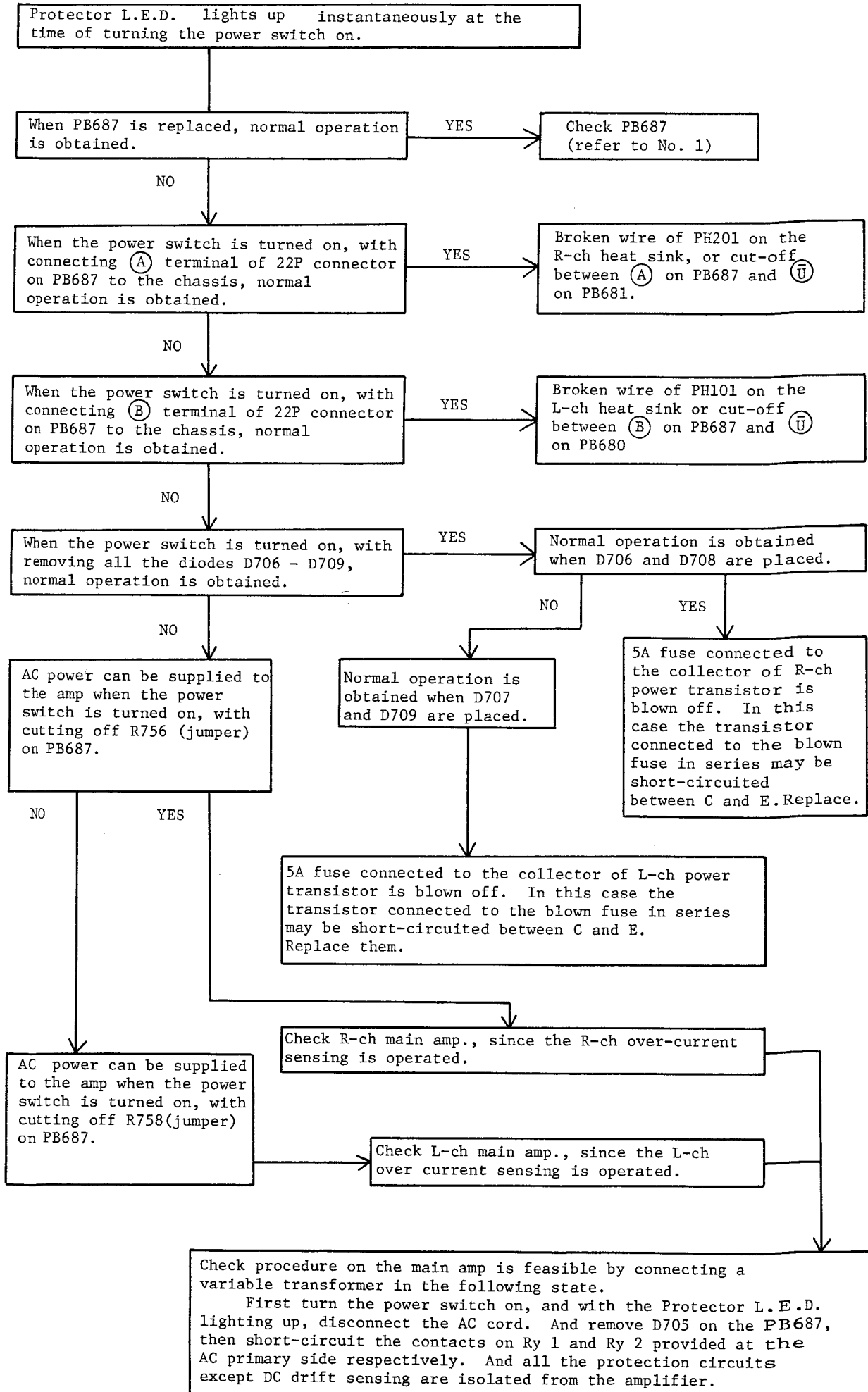
NO

C - E short-circuited both on Q729 and Q732.

YES

C - E of Q704 open-circuited or broken wire of D701.

C - E short-circuited both on Q730 and Q731.



Protector L.E.D. lights up instantaneously at the time of turning the power switch on.

When PB687 is replaced, normal operation is obtained.

YES

Check PB687 (refer to No. 1)

NO

When the power switch is turned on, with connecting (A) terminal of 22P connector on PB687 to the chassis, normal operation is obtained.

YES

Broken wire of PH201 on the R-ch heat sink, or cut-off between (A) on PB687 and (U) on PB681.

NO

When the power switch is turned on, with connecting (B) terminal of 22P connector on PB687 to the chassis, normal operation is obtained.

YES

Broken wire of PH101 on the L-ch heat sink or cut-off between (B) on PB687 and (U) on PB680

NO

When the power switch is turned on, with removing all the diodes D706 - D709, normal operation is obtained.

YES

Normal operation is obtained when D706 and D708 are placed.

NO

YES

AC power can be supplied to the amp when the power switch is turned on, with cutting off R756 (jumper) on PB687.

NO

YES

Normal operation is obtained when D707 and D709 are placed.

5A fuse connected to the collector of R-ch power transistor is blown off. In this case the transistor connected to the blown fuse in series may be short-circuited between C and E. Replace.

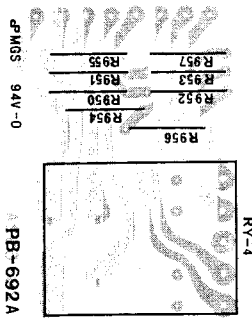
5A fuse connected to the collector of L-ch power transistor is blown off. In this case the transistor connected to the blown fuse in series may be short-circuited between C and E. Replace them.

AC power can be supplied to the amp when the power switch is turned on, with cutting off R758(jumper) on PB687.

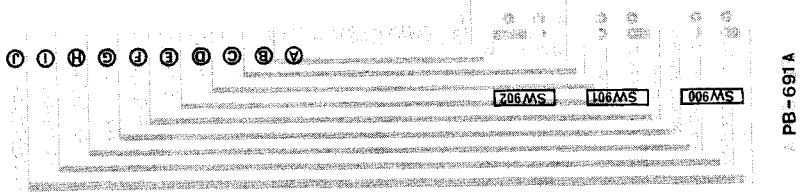
Check R-ch main amp., since the R-ch over-current sensing is operated.

Check L-ch main amp., since the L-ch over current sensing is operated.

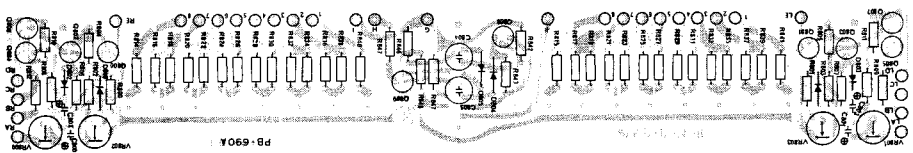
Check procedure on the main amp is feasible by connecting a variable transformer in the following state.
 First turn the power switch on, and with the Protector L.E.D. lighting up, disconnect the AC cord. And remove D705 on the PB687, then short-circuit the contacts on Ry 1 and Ry 2 provided at the AC primary side respectively. And all the protection circuits except DC drift sensing are isolated from the amplifier.



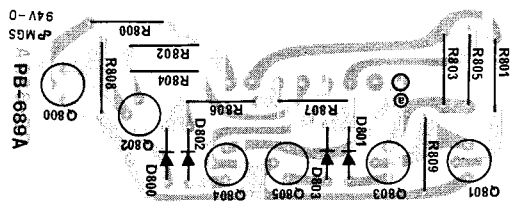
PB692A



PB691A



PB690A



PB689A

REPLACEMENT PARTSPB-680A

SYMBOL NO.				LOCATION				SYMBOL NO.				LOCATION			
R101	10	1W	X-B	R123	330K	1/2W	Y-B	R145	10	1W	Y-C				
102	2.2K	1/2W	X-B	124	10	1W	X-A	146	330K	1/2W	Y-C				
103	0.47	5W	X-B	125	2.2K	1/2W	X-A	147	330K	1/2W	Y-A				
104	0.47	5W	X-D	126	0.47	5W	X-A	148	56K	1W	X-C				
105	2.2K	1/2W	X-D	127	0.47	5W	X-C	149	56K	1W	X-B				
106	10	1W	X-D	128	2.2K	1/2W	X-C	150	330K	1/2W	Y-C				
107	330K	1/2W	X-B	129	10	1W	X-C	Q101	2SD424-R,	0	X-B				
108	10	1W	Y-B	130	330	1/2W	X-D	102	2SB554-R,	0	X-D				
109	2.2K	1/2W	X-B	131	330	1/2W	X-A	103	2SD424-R,	0	X-B				
110	0.47	5W	X-B	132	10	1W	Y-A	104	2SB554-R,	0	X-D				
111	0.47	5W	X-D	133	2.2K	1/2W	X-A	105	2SD424-R,	0	Y-B				
112	2.2K	1/2W	X-D	134	0.47	5W	X-A	106	2SB554-R,	0	Y-D				
113	10	1W	Y-D	135	0.47	5W	X-C	107	2SD424-R,	0	X-A				
114	330K	1/2W	X-D	136	2.2K	1/2W	X-C	108	2SB554-R,	0	X-C				
115	330K	1/2W	X-B	137	10	1W	Y-C	109	2SD424-R,	0	X-A				
116	10	1W	Y-B	138	330K	1/2W	X-C	110	2SB554-R,	0	X-C				
117	2.2K	1/2W	Y-B	139	330K	1/2W	X-A	111	2SD424-R,	0	Y-A				
118	0.47	5W	Y-B	140	10	1W	Y-A	112	2SB554-R,	0	Y-C				
119	0.47	5W	Y-D	141	2.2K	1/2W	Y-A	113	2SC1745-BL		Y-C				
120	2.2K	1/2W	Y-D	142	0.47	5W	Y-A	PH101	487A01BD471TS		Y-B				
121	10	1W	Y-D	143	0.47	5W	Y-C								
122	330K	1/2W	X-D	144	2.2K	1/2W	Y-C								

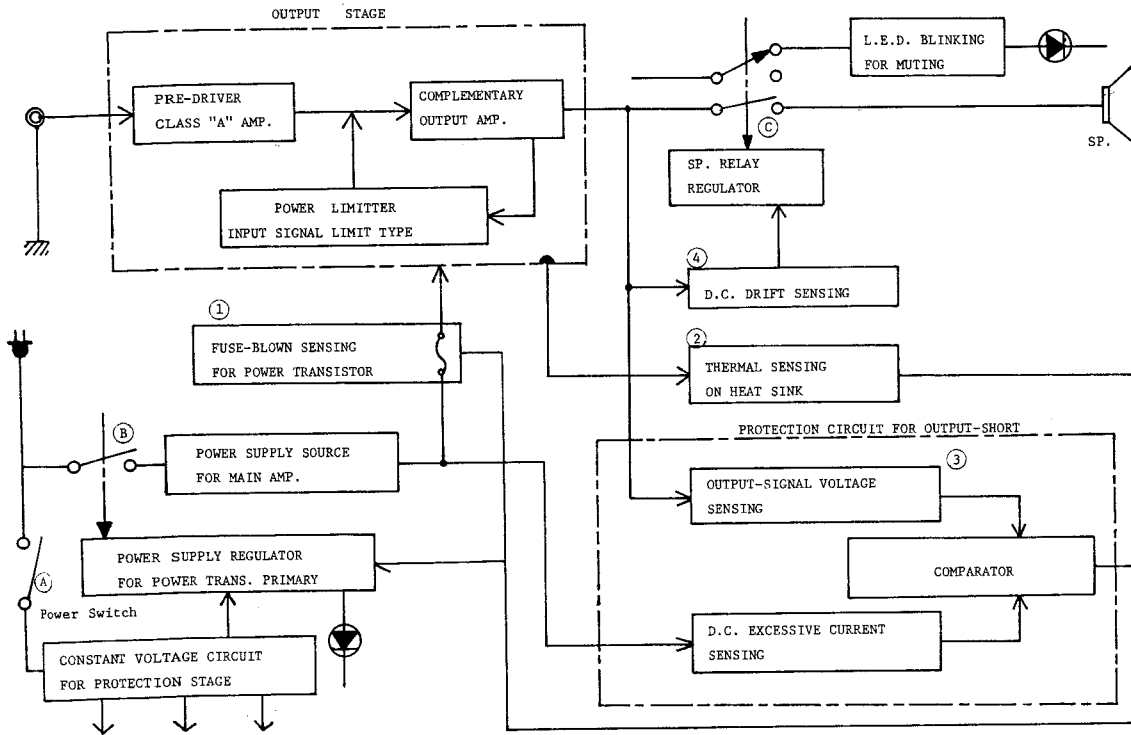
PB-681A

SYMBOL NO.				LOCATION				SYMBOL NO.				LOCATION			
R201	10	1W	X-D	R224	10	1W	X-C	R247	330K	1/2W	Y-C				
202	2.2K	1/2W	X-D	225	2.2K	1/2W	X-C	248	56K	1W	X-B				
203	0.47	5W	X-D	226	0.47	5W	X-C	249	56K	1W	X-C				
204	0.47	5W	X-B	227	0.47	5W	X-A	250	330K	1/2W	X-C				
205	2.2K	1/2W	X-B	228	2.2K	1/2W	X-A	Q201	2SD424-R,	0	X-D				
206	10	1W	X-B	229	10	1W	X-A	202	2SB554-R,	0	X-B				
207	330K	1/2W	X-D	230	330K	1/2W	Y-B	203	2SD424-R,	0	X-D				
208	10	1W	Y-D	231	330K	1/2W	X-C	204	2SB554-R,	0	X-B				
209	2.2K	1/2W	X-D	232	10	1W	Y-C	205	2SD424-R,	0	Y-D				
210	0.47	5W	X-D	233	2.2K	1/2W	X-C	206	2SB554-R,	0	Y-B				
211	0.47	5W	X-B	234	0.47	5W	X-C	207	2SD424-R,	0	X-C				
212	2.2K	1/2W	X-B	235	0.47	5W	X-A	208	2SB554-R,	0	X-A				
213	10	1W	Y-B	236	2.2K	1/2W	X-A	209	2SD424-R,	0	X-C				
214	330K	1/2W	X-B	237	10	1W	Y-A	210	2SB554-R,	0	X-A				
215	330K	1/2W	X-D	238	330K	1/2W	X-A	211	2SD424-R,	0	Y-C				
216	10	1W	Y-D	239	330K	1/2W	Y-C	212	2SB554-R,	0	Y-A				
217	2.2K	1/2W	Y-D	240	10	1W	Y-C	213	2SC1745-BL		Y-B				
218	0.47	5W	Y-D	241	2.2K	1/2W	Y-C	PH201	487A01BD471TS		Y-C				
219	0.47	5W	Y-B	242	0.47	5W	Y-C								
220	2.2K	1/2W	Y-B	243	0.47	5W	Y-A								
221	10	1W	Y-B	244	2.2K	1/2W	Y-A								
222	330K	1/2W	X-B	245	10	1W	Y-A								
223	330K	1/2W	X-D	246	330K	1/2W	X-A								

PB-682A

SYMBOL NO.				LOCATION				SYMBOL NO.				LOCATION			
R301	4.7K	1/4W	Y-A	R311	3.9K	1/2W	X-A	R324	22	2W	Y-B				
302	47	1/2W	Y-A	312	1.2K	1/2W	Y-A	325	15	1/2W	X-C				
303	330	1/2W	Y-A	313	56K	1/2W	Y-A	326	330	1/2W	Y-B				
304	33K	1W	Y-A	314	220	1/2W	X-A	327	330	1/2W	Y-C				
305	330	1/2W	Y-A	315	220	1/2W	Y-B	328	47	1/2W	Y-B				
306	56K	1/2W	Y-A	317	82K	1/2W	X-B	329	47	1/2W	Y-B				
307	33K	1W	X-A	318	47	1W	Y-C	330	3.3K	1/2W	Y-B				
308	3.9K	1/2W	X-A	319	100K	1/2W	Y-B	331	100	1W	Y-A				
309	10K	1W	Y-A	321	100	2W	Y-C	332	3.3K	1/2W	Y-B				
310	8.2K	1/2W	Y-A	322	270	1/2W	X-C	333	100	1W	Y-C				

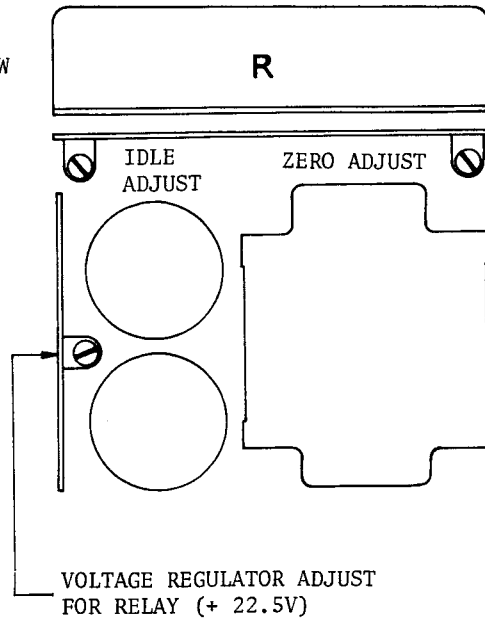
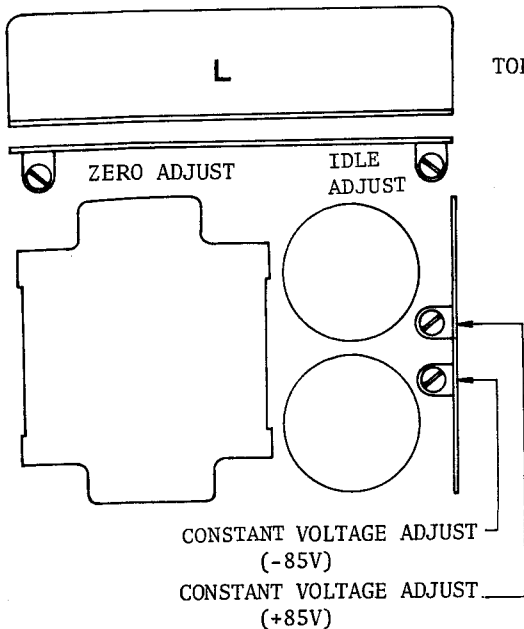
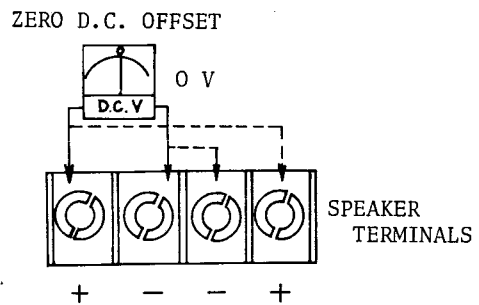
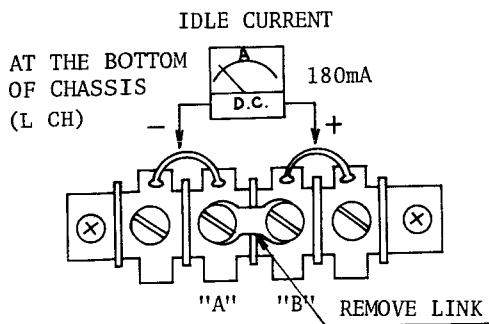
BLOCK DIAGRAM (PROTECTION)



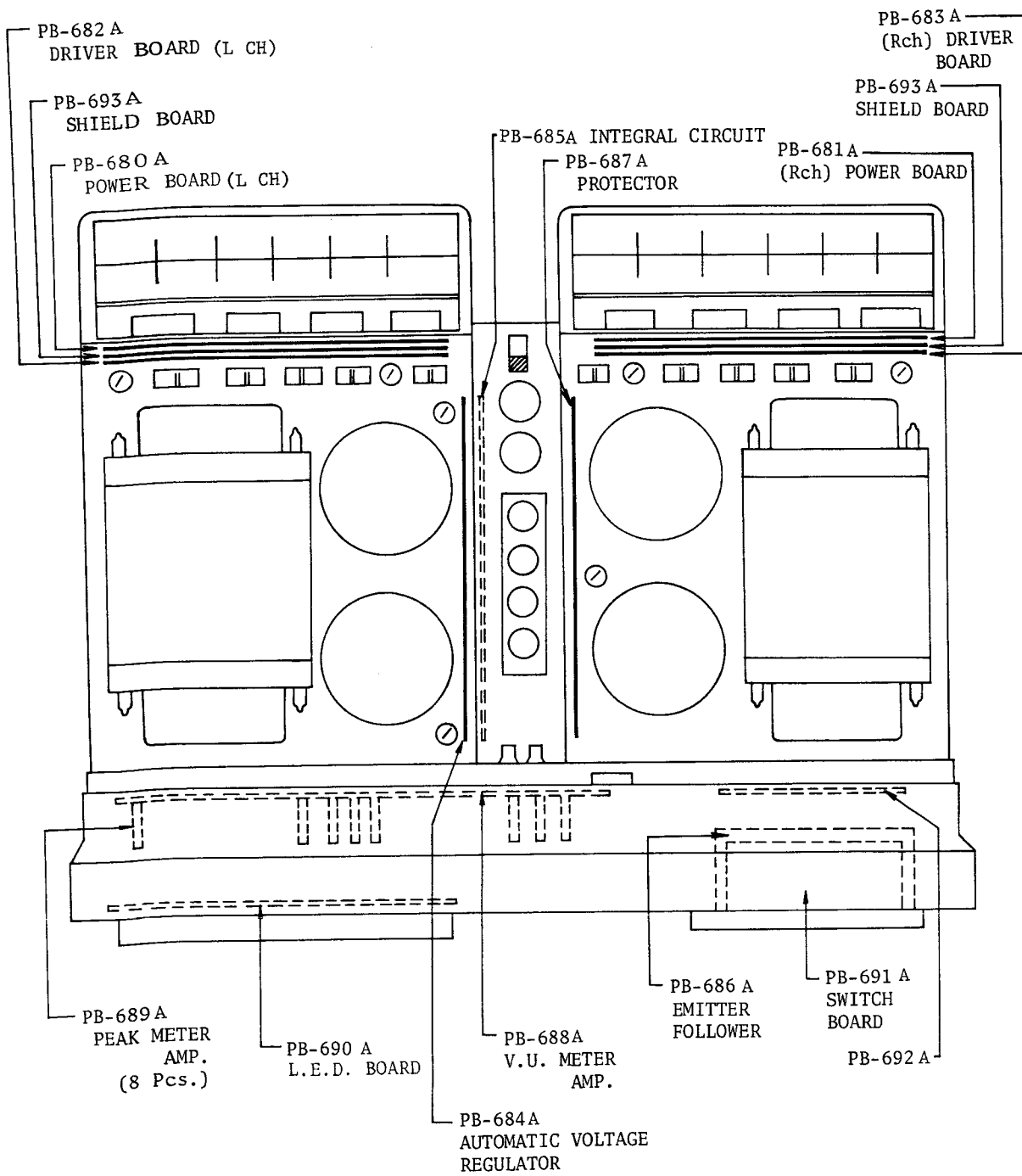
IDLE CURRENT AND ZERO D.C. OFFSET

CAUTION: Set level controls to ∞ position

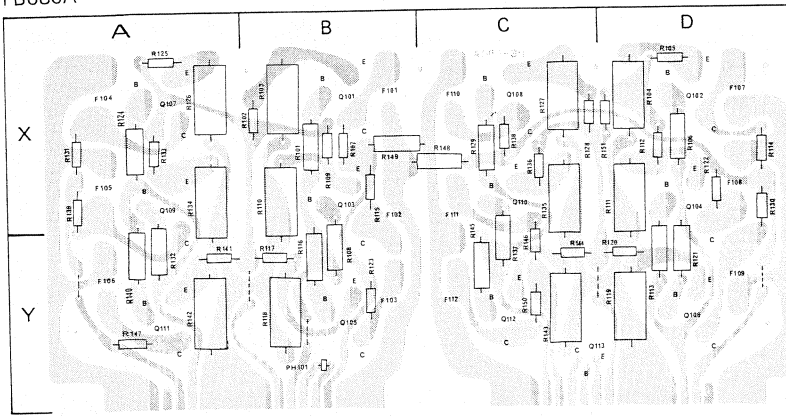
- 1) Do not operate with no "Amp meter" or "Link" connected across points "A & B".
- 2: Final adjustment of the idle current should be set after 30 minutes of operation.



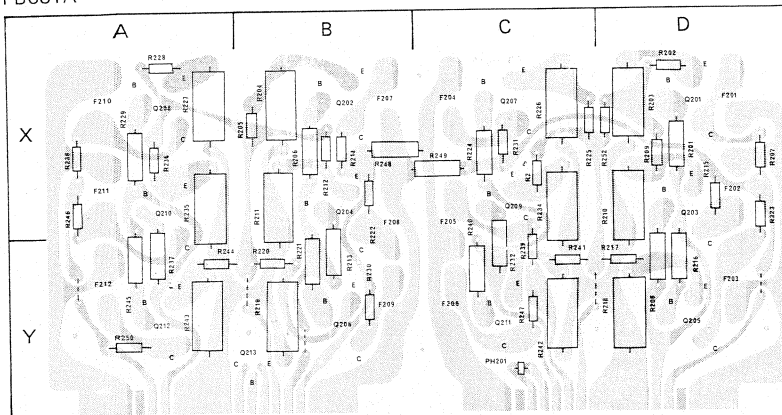
P.B. LOCATION



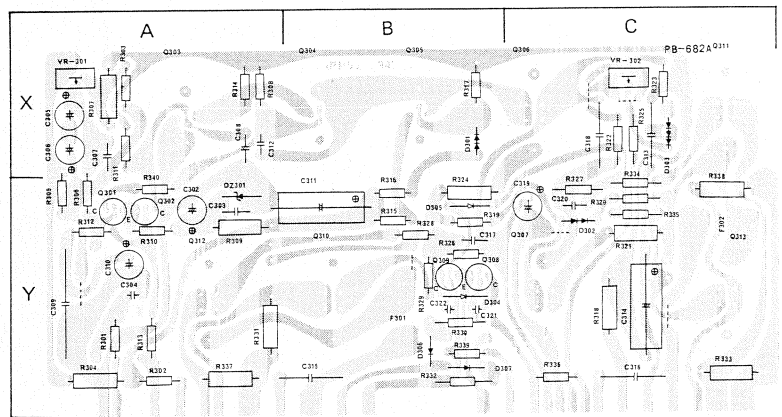
PB680A



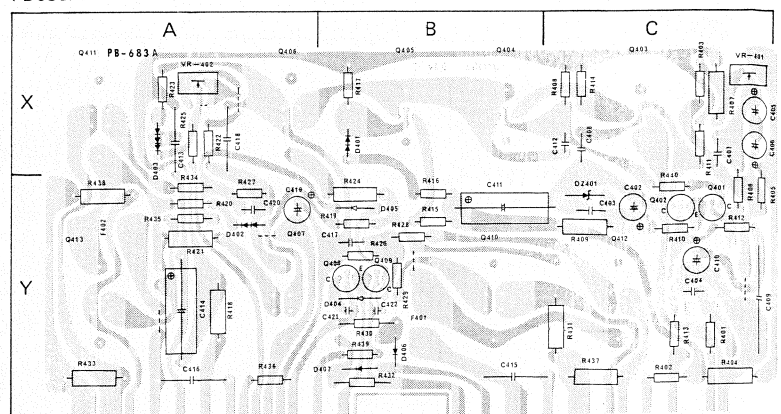
PB681A



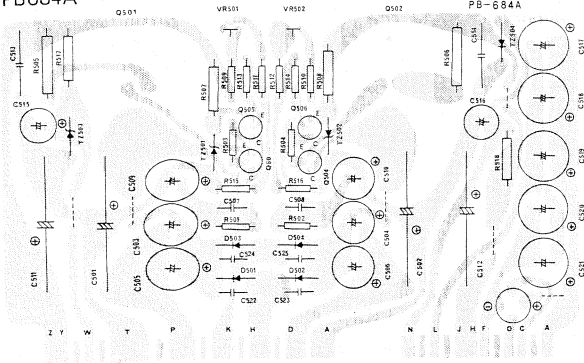
PB682A



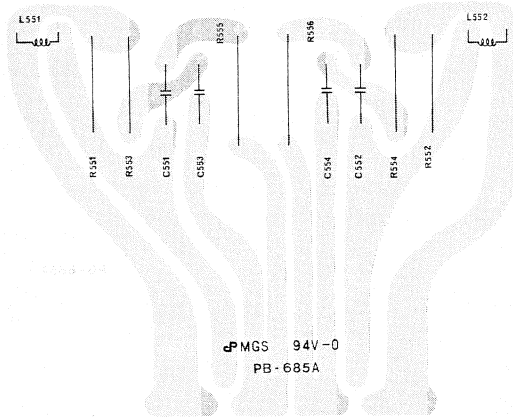
PB683A



PB684A

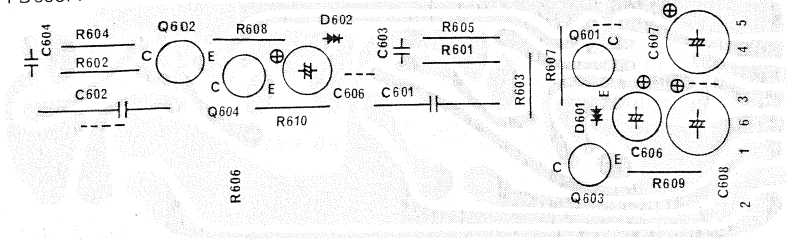


PB685A

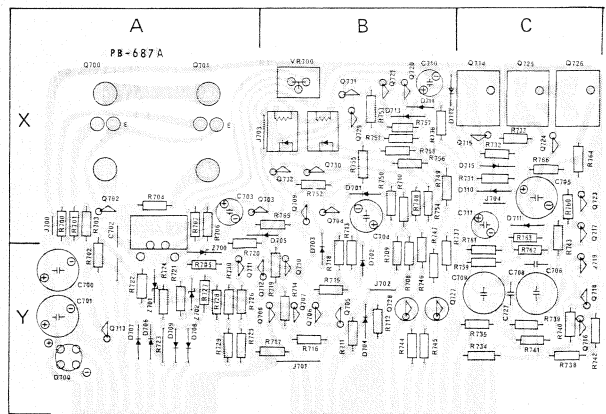


MG5 94V-0
PB-685A

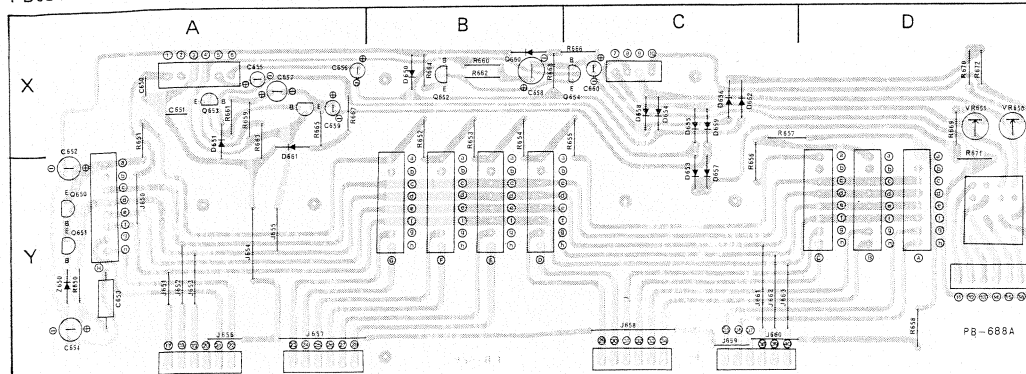
PB686A



PB687A



PB688A



This servicing section should be applied to the models with the serial No. up to Serial No.A6100317.

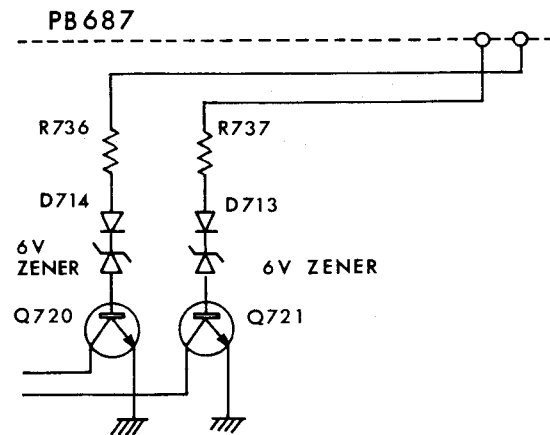
Referring to Power Transistor Breakage

CAUSE: Durability of the transistors manufactured by N.E.C. is found relatively poor as compared with these manufactured by TOSHIBA, and incidentally they may be damaged before the protector is operated. And further the protector does not happen to operate on a certain level of the output and on a certain frequency.

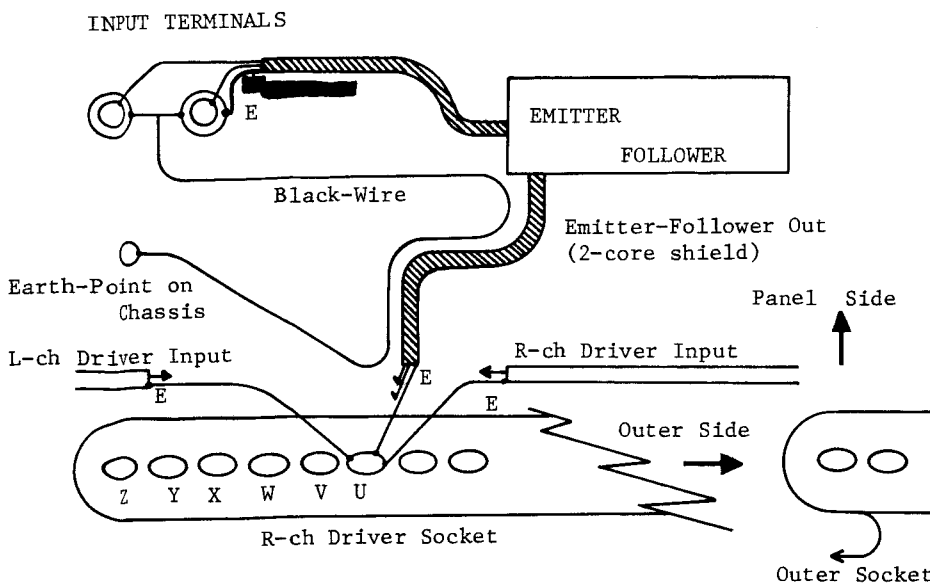
COUNTER-MEASURE: # The poor transistors should be changed from N.E.C. to TOSHIBA brand.

To expand the operational range of the protector circuit, and at the same time to let it operate more speedily.

- MODIFICATION:
- 1) All power transistors should be changed into TOSHIBA.
 - 2) A 6V zener diode should be added in between the base of Q720 and the existing diode D714, and the same zener in between the base of Q721 and D713.
(To expand the operational range of the protector versus output level.)
 - 3) An electrolytic of 100uF 10V should be added in parallel with the coil of the reed-relay on PB687. (A reed-relay is adopted instead of the photo-coupler in the models for the U.S.A. market.)
(To expand the operational range of the protector versus output frequency.)
 - 4) An electrolytic of 4.7uF 10V should be adopted for C704 on PB687.
(To obtain shorter operational time of the protector.)



Counter-measure against the trouble of the anti-oscillation resistor (2.2-ohm) which is inserted into the input line.



MODIFICATION:

- 1) Remove the cold side of the Emitter Follower Out (2-core shield) and the input of the driver board of both L-ch and R-ch (single-core shield) from the earth terminal on the chassis, and connect these three wires to the U terminals of the inner socket on the R-ch driver board.
- 2) Prepare another black-wire, and connect the earth terminal of the input terminal and that on the chassis. Note that the black-wire should be in parallel with the Emitter Follower Out (2-core shield).

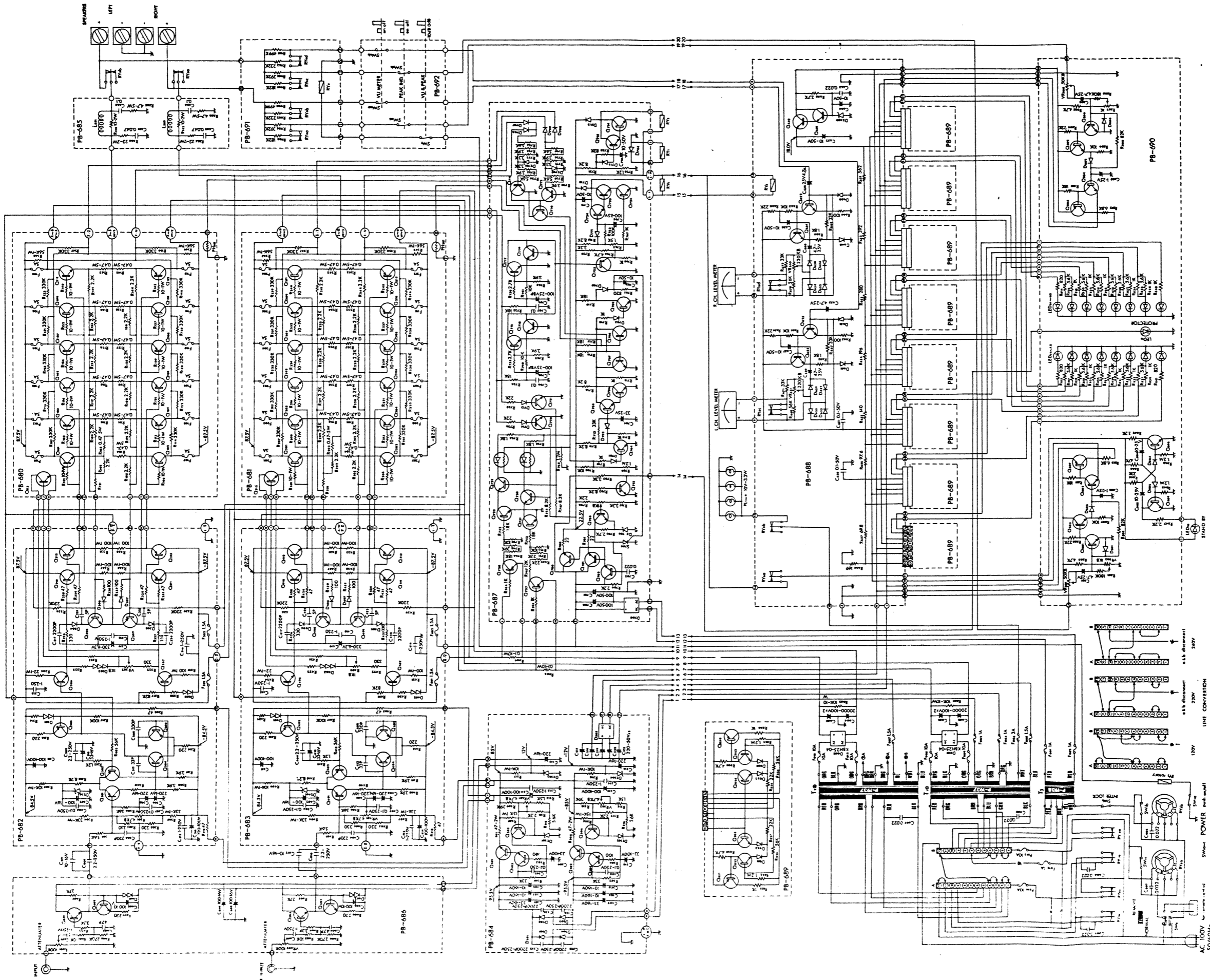
3) Remove the resistor (2.2-ohm) inserted into the cold-side of the input line.

PB-687A

SYMBOL NO.				LOCATION				SYMBOL NO.				LOCATION			
R700	22	1/2W	X-A	R746	18K	1/2W	Y-B	D711	IK188FM-1		X-C				
701	22	1/2W	X-A	747	12K	1/2W	Y-B	712	IN4003		X-B				
702	1.8K	1/2W	Y-A	748	39K	1/2W	X-B	713	IS1586		X-B				
703	3.3K	1/2W	X-A	749	22K	1/2W	X-B	714	IS1586		X-B				
704	2.2K	1/2W	X-A	750	10K	1/2W	X-B	715	IK188FM-1		X-C				
705	2.7K	1/2W	Y-A	751	22K	1/2W	X-B	Z700	BZ-120	1W	Y-A				
706	2.2K	1/2W	X-A	752	1.8K	1/2W	X-B	701	WZ-061	1/2W	Y-A				
707	3.3K	1/2W	X-A	753	1.8K	1/2W	X-B	702	WZ-061	1/2W	Y-A				
708	10K	1/2W	Y-B	754	8.2K	1/2W	X-B	Q700	2SC1025-E		X-A				
709	1.5K	1/2W	Y-B	755	10K	1/2W	X-B	701	2SC1025-E		X-A				
710	1K	1/2W	X-B	756	1.8K	1/2W	X-B	702	2SC734-Y		X-A				
711	8.2k	1/2W	Y-B	757	8.2K	1/2W	X-B	703	2SC734-Y		X-B				
712	1K	1/2W	Y-B	758	1.8K	1/2W	X-B	704	2SC734-Y		X-B				
713	33K	1/2W	Y-B	759	3.3K	1/2W	Y-C	705	2SC734-Y		Y-B				
714	8.2K	1/2W	Y-B	760	1K	1/2W	X-C	706	2SC734-Y		Y-B				
715	1K	1/2W	Y-B	761	8.2K	1/2W	Y-C	707	2SC734-Y		Y-B				
716	18K	1/2W	Y-B	762	1.5K	1/2W	Y-C	708	2SC734-Y		Y-B				
717	18K	1/2W	Y-B	763	100K	1/2W	X-C	709	2SC734-Y		X-B				
718	1K	1/2W	Y-B	764	1K	1/2W	X-C	710	2SA561-Y		Y-B				
719	18K	1/2W	Y-B	765	820	1/2W	X-B	711	2SC734-Y		Y-A				
720	1.5K	1/2W	Y-A	766	4.7K	1/4W	X-C	712	2SC734-Y		Y-B				
721	3.3K	1/2W	Y-A	VR700	1K-B		X-B	713	2SC734-Y		Y-A				
722	3.3K	1/2W	Y-A	C700	100mfd	50V	Y-A	714	2SD331-E		X-C				
723	5.6K	1/2W	Y-A	701	100mfd	50V	Y-A	715	2SC734-Y		X-C				
724	3.9K	1/2W	Y-A	702	0.022mfd	100V	Y-A	716	2SC734-Y		Y-C				
725	3.9K	1/2W	Y-A	703	10mfd	50V	X-A	717	2SC734-Y		X-C				
726	5.6K	1/2W	Y-A	705	100mfd	25V	X-C	718	2SC734-Y		Y-C				
727	5.6K	1/2W	Y-A	706	0.1mfd	50V	Y-C	719	2SC734-Y		Y-C				
728	3.9K	1/2W	Y-A	708	100mfd	25V	Y-C	720	2SC734-Y		X-B				
729	5.6K	1/2W	Y-A	709	100mfd	25V	Y-C	721	2SC734-Y		X-B				
730	3.9K	1/2W	Y-A	710	10mfd	50V	X-B	723	2SA561-Y		X-C				
731	8.2k	1/2W	X-C	711	10mfd	50V	X-C	724	2SC734-Y		X-C				
732	82K	1/2W	X-C	712	0.1mfd	50V	Y-C	725	2SD331-E		X-C				
733	1.2K	1/2W	X-C	D700	W04		Y-A	726	2SD331-E		X-C				
734	18K	1/2W	Y-C	701	IS1586		X-B	727	2SA809-V, B		Y-B				
735	18K	1/2W	Y-C	702	IK188FM-1		Y-B	728	2SA809-V, B		Y-B				
736	22K	1/2W	X-B	703	IS1586		Y-B	729	2SC734-Y		X-B				
737	22K	1/2W	Y-B	704	IN4003		Y-B	730	2SC734-Y		X-B				
738	2.7K	1/2W	Y-C	705	IS1586		X-B	731	2SC734-Y		X-B				
739	2.7K	1/2W	Y-C	706	IS1585		Y-A	732	2SC734-Y		X-B				
740	10K	1/2W	Y-C	707	IS1585		Y-A	SCR	SFIR3D41		X-A				
741	10K	1/2W	Y-C	708	IS1585		Y-A								
742	3.9K	1/2W	Y-C	709	IS1585		Y-A								
743	3.9K	1/2W	X-C	710	IN4003		X-C								
744	1K	1/2W	Y-B												
745	1K	1/2W	Y-B												

PB-688A

SYMBOL NO.				LOCATION				SYMBOL NO.				LOCATION			
R650	2.7K	1/2W	Y-A	R670	100K	1/2W	X-D	D653	IS1555		Y-C				
651	562	1/2W	X-A	671	33K	1/2W	Y-D	654	IS1555		X-C				
652	392	1/2W	X-B	672	33K	1/2W	X-D	655	IS1555		X-C				
653	280	1/2W	X-B	VR650	220K-B		X-D	656	IS1555		X-C				
654	196	1/2W	X-B	651	220K-B		X-D	657	IS1555		Y-C				
655	140	1/2W	X-C	C650	0.1mfd	50V	X-A	658	IS1555		X-C				
656	97.6	1/2W	Y-C	651	0.1mfd	50V	X-A	659	IS1555		X-C				
657	69.8	1/2W	X-C	652	10mfd	50V	Y-A	660	IS1586		X-B				
658	169	1/2W	Y-D	653	0.022mfd	100V	Y-A	661	IS1586		X-A				
659	22K	1/2W	X-A	654	10mfd	50V	Y-A	Z650	BZ-192	1W	Y-A				
660	22K	1/2W	X-B	655	4.7mfd	25V	X-A	Q650	2SC496-Y		Y-A				
661	10K	1/2W	X-A	656	4.7mfd	25V	X-A	651	2SC734-Y		Y-A				
662	10K	1/2W	X-B	657	10mfd	50V	X-A	652	2SC734-Y		X-B				
663	100	1/2W	X-A	658	10mfd	50V	X-B	653	2SC734-Y		X-A				
664	100	1/2W	X-B	659	4.7mfd	25V	X-A	654	2SC734-Y		X-C				
665	1.8K	1/2W	X-A	660	4.7mfd	25V	X-C		2SC734-Y		X-A				
666	1.8K	1/2W	X-C	D650	IS1586		X-B								
667	33K	1/2W	X-A	651	IS1586		X-A								
668	33K	1/2W	X-B	652	IS1555		X-C								
669	100K	1/2W	X-D												



- 1 UNLESS OTHERWISE SPECIFIED, ALL RESISTORS ARE IN OHMS
- 2 TUBE SOCKETS ARE IN MICRO-BOARD
- 3 TRANSFORMERS ARE TO BE REPLACED WITH ANY EQUIVALENTS OF COMPARABLE RATINGS
- 4 DUE TO CONTINUED IMPROVEMENTS, WE RESERVE THE RIGHT TO ALTER THE CIRCUIT OR SPECIFICATIONS

Part No.	Quantity	Part No.	Quantity
PB-680	1	PB-684	1
PB-681	1	PB-685	1
PB-682	1	PB-686	1
PB-683	1	PB-687	1
PB-684	1	PB-688	1
PB-685	1	PB-689	1
PB-686	1	PB-690	1
PB-687	1	PB-691	1
PB-688	1		
PB-689	1		
PB-690	1		
PB-691	1		

ULTIMATE HIGH FIDELITY

M-6000

AC 100V 50/60HZ

POWER

LINE CONVERSION

120V

230V

240V

STAND BY

