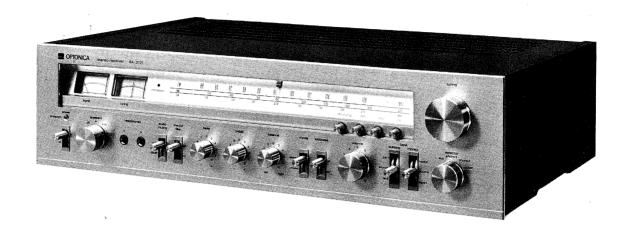
# OPTONICA SERVICE MANUAL &



# Stereo Receiver MODEL SA-2121H

In the interests of user-safety the set should be restored to its original condition and only parts identical to those specified be used.

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SHARP CORPORATION OSAKA, JAPAN

## **SPECIFICATIONS**

GENERAL DESCRIPTION

Power source:

AC 110/220/240V, 50/60Hz

Power consumption:

Circuit

Tuner:

Superheterodyne system,

LW/MW/FM 3-bands tuner, with P.L.L. stereo demodulation circuit,

FM muting circuit

Main amplifier:

Differential amplifier and all stage direct coupled pure complimentary O.C.L. (Output Capacitor-Less) cir-

cuitry.

460W

Tone amplifier: Equalizer:

"NF" type tone control circuit. Dual power supply IC amplifier

circuit

Semiconductors:

7-IC (Integrated circuit) 28-transistor (1-FET) 31-diode (4-Zener diode)

2-LED

Dimensions:

Width . . . . . 550 mm Height . . . . . 142 mm Depth . . . . 390 mm

Weight: 14.5 kg

FM SECTION

Tuning range:  $87.6 \sim 108 \text{ MHz}$ 

Intermediate

frequency:

10.7 MHz

Sensitivity:

 $1.8\mu V$  (at S/N 26 dB, 40 kHz

deviation, antenna terminal voltage)

Distortion (40 kHz deviation)

Mono: Stereo: 0.5% 0.8%

Image rejection ratio: I.F. rejection ratio:

50 dB 70 dB

Spurious frequency

rejection ratio:

60 dB

AM suppression ratio:

40 dB (modulated by 30% AM

and 75 kHz deviation FM)

Selectivity:

Capture ratio:

Stereo separation: Antenna input:

50 dB (IHF at 40 dB) 2 dB34 dB (1 kHz)

75 ohms unbalanced

240 ohms balanced

MAM SECTION

Tuning range:

MW 520  $\sim$  1620 kHz LW  $150 \sim 370 \text{ kHz}$ 

Intermediate

frequency:

MW/LW 455 kHz

Quieting Sensitivity:

MW  $400\mu V/m$  (at 1000 kHz)

LW  $400\mu V/m$  (at 220 kHz)

Image rejection ratio:

MW 34 dB (at 1400 kHz)

LW 30 dB (at 340 kHz)

I.F. rejection ratio:

MW 49 dB (at 600 kHz) LW 40 dB (at 340 kHz)

Distortion:

LW/MW 1.6%

Antenna:

Built-in ferrite bar antenna and external antenna terminal

● MAIN (POWER) AMPLIFIER

Continuous power output:

 $2 \times 45W/4$ -ohms, both channels driven at 1 kHz, 0.1% distortion 2 x 30W/8-ohms, both channels

driven at 1 kHz, 0.1% distortion

Total harmonic distortion:

0.05% at 20W (AUX IN)

Intermodulation distortion:

0.1% at 20W (AUX IN)

Damping factor:

More than 20 (at 1 kHz, 4-ohms)

Power bandwidth:

 $20 \text{ Hz} \sim 20 \text{ kHz}$ 

● PRE-AMPLIFIER

Input sensitivity and input impedance

PHONO 1: PHONO 2: 2.5 mV/50K ohms 2.5 mV/50K ohms

AUX:

150 mV/50K ohms

TAPE playback

1 and 2:

150 mV/50K ohms

Output level and loaded impedance

REC 1 and 2:

150 mV/50K ohms

REC 1 and 2 (DIN socket):

30 mV/80K ohms

Phono overload:

140 mV (R.M.S. 1 kHz,

0.1% T.H.D.)

"RIAA" curve deviation (Phono):

 $\pm$  1.5 dB (30 Hz  $\sim$  15 kHz)

10 Hz  $\sim$  50 kHz  $\pm$  1.5 dB (AUX., Frequency response:

TAPE playback)

Tone control

Bass. Treble: ± 10 dB at 100 Hz

Low cut filter:

± 10 dB at 10 kHz

-3 dB at 30 Hz, 6 dB/oct

Audio muting:

-20 dB

# **FEATURES**

- 1) The equalizer amplifier that operates on dual power supply (plus and minus) to allow the maximum 140 mV phono input.
- 2) With a built-in protection circuit, the loudspeaker remains always safe even if the amplifier circuit gets in trouble and reversely the amplifier is protected against a possible short-circuit of the loudspeaker cord.
- 3) Power source/circuit protection indicator making use of 2-color LED element, which will light up in red if there is something abnormal in the internal circuitry. In a normal condition, it is lit green.
- 4) Because of the circuit being ITL (Input Transformerless), OTL (Output Transformerless), OCL (Output Capacitorless) and pure-complementary system, low-distortion characteristic is more assured.
- 5) FET and 3-gang variable capacitor adopted at the FM front-end circuit more improve overall characteristics.
- 6) The PLL (Phase Locked Loop) demodulator circuit assures a stabilized characteristic.

# AC VOLTAGE SELECTION (Refer to Figure 1)

Check the preset voltage selector before inserting the mains plug to an mains outlet. If the voltage is different from your local voltage, change it in the following manner:

- 1. Disconnect the AC cord plug from the wall outlet in order to prevent an electric shock.
- 2. Loosen a screw and slide the cover as illustrated in Fig. 1.
- 3. Put a fuse in the fuse holder which has an indication of your local voltage.
  - In case the local voltage is 110V, two pieces of fuses should be used.
- 4. Replace the cover in its original position.

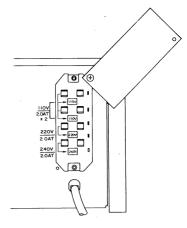


Figure 1

#### DISASSEMBLY

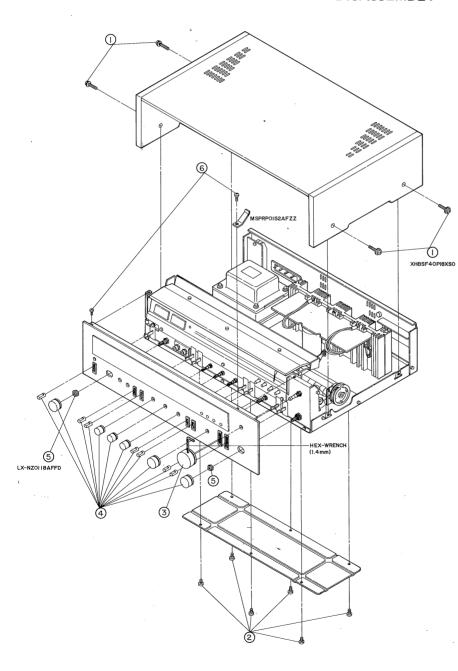


Figure 2 DISASSEMBLY

Prior to removing the chassis, be sure to draw the power supply plug from a wall outlet. Then, proceed with the removal work in the following order after disconnecting all of the connection cords at the rear of the set.

- To remove the cabinet:
   Remove 4 screws ① retaining the cabinet
   (2 screws each for the right and left sides), then the cabinet can be detached.
- 2) To remove the bottom board: Turn over the set and remove 6 screws(2) retaining the bottom board, then the bottom board can be detached.
- 3) To remove the front panel:
  - (1) Use a hexagonal wrench (1.4 mm) to loosen the screw retaining the tuning knob (3) at the front panel, and pull out the tuning knob.
  - (2) Pull out the remaining knobs (4) (13 knobs).
  - (3) Remove the nuts (5) retaining the speaker switch shaft and selector switch shaft.
- (4) Finally remove 2 screws 6 retaining the front panel, then the front panel can be detached.

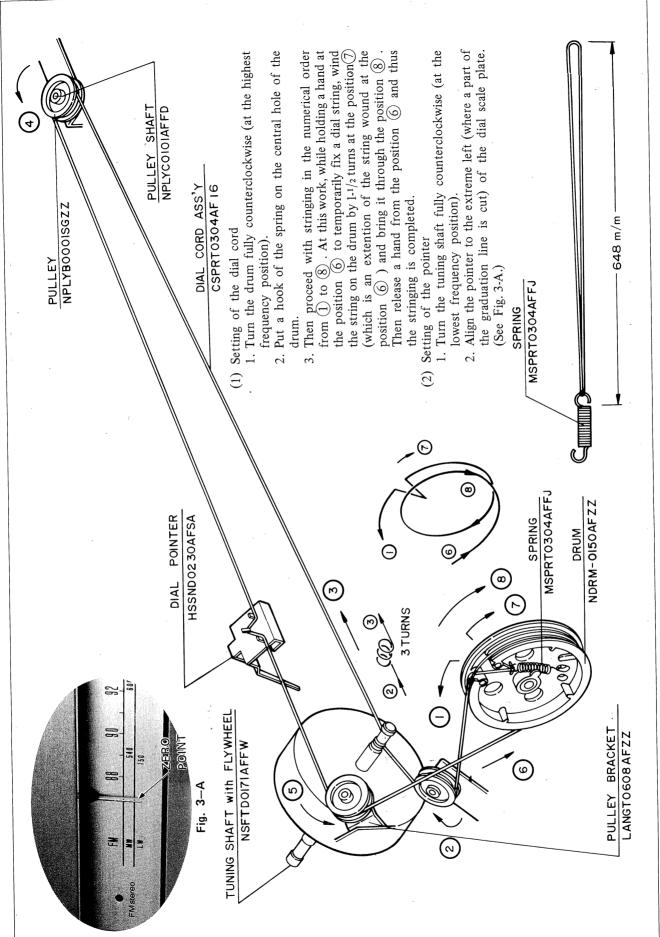
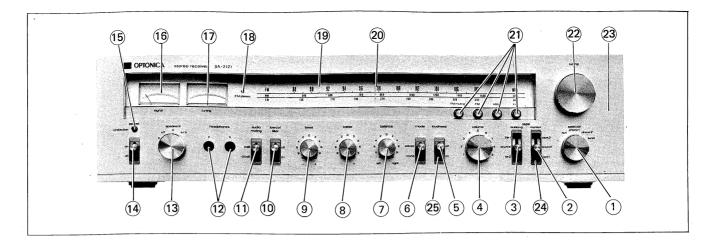


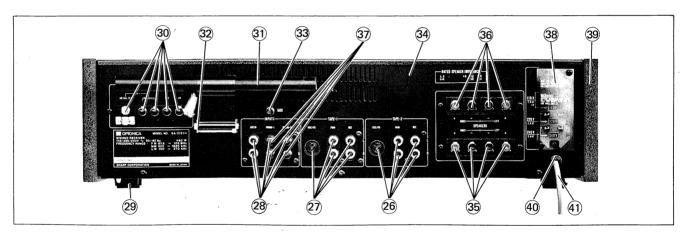
Figure 3 DIAL CORD STRINGING



- 1 Function selector knob (JKNBN0333AFSA)
- (2) Tape monitor switch knob (JKNBP0070AFSA)
- (3) Tape dubbing switch knob (JKNBP0070AFSA)
- (4) Volume control knob (JKNBN0333AFSA)
- (5) Loudness switch knob (JKNBP0070AFSA)
- (6) Mode selector knob (JKNBP0070AFSA)
- (7) Balance control knob (JKNBN0334AFSA)
- (8) Treble control knob (JKNBN0334AFSA)
- Bass control knob (JKNBN0334AFSA)
- (10) Low cut filter switch knob (JKNBP0070AFSA)
- (11) Audio muting switch knob (JKNBP0070AFSA)
- (12) Headphone jacks (a, b) (QJAKJ0057AFZZ)
- (13) Speakers selector knob (JKNBN0333AFSA)
- (14) Power switch knob (JKNBP0070AFSA)

- (15) Power source/circuit protection indicator, LED (VHPGL-52RG/1F)
- (16) Signal strength meter, ME801 (RMTRL0135AFSA)
- (17) FM tuning (center) meter, ME802 (RMTRL0134AFSA)
- (18) FM stereo indicator, LED (VHPSR105D //-1)
- (19) Dial (HDALM0173AFSA)
- 20 Dial pointer (HSSND0230AFSA)
- (21) LW/MW/FM/FM muting knob (JKNBM0248AFSA)
- 22) Tuning control knob (JKNBB0059AFSA)
- (23) Front panel (HPNLC3276AFSA)
- Q4) Guide (Large), lever switch (GCOVA1070AFSC)
- 25) Guide (Small), lever switch (GCOVA1071AFSC)

Figure 4 FRONT PARTS LAYOUT



- 26 Tape-2 (REC/PBP) sockets and DIN (REC/PB) (QSOCZ2450AFZZ)
- (REC/PB) sockets and DIN (REC/PB) (QSOCZ2450AFZZ)
- 28 Aux./Phono1/Phono2 input sockets (QSOCJ2660AFZZ) \*37 Short plug (QPLGS0102AGZZ)
- 29 Leg (GLEGP0002SG00)

\* Short plug

- 30 Antenna terminals (QTANN0453AFZZ)
- (RCILA0403AFZZ)
- (2) Bracket of bar antenna (LANGQ0423AFZZ)

- (33) Grounding (Earth) terminal (QTANN0150AFZZ)
- (34) Rear panel (LANGQ0508AFSA)
- 35 Speaker terminals—B (QTANN0454AFZZ)
- 36 Speaker terminals—A (QTANN0454AFZZ)
- (\$\overline{38}\$) Fuse cover (PCOVP1158AFZZ)
- (39) Cabinet (GCAB-5090AFSA)
- 40 Bushing, power supply cord
- (41) Power supply cord

For noise prevention, be sure to insert a furnished short plug into the socket PHONO when not in use.

Figure 5 REAR PARTS LAYOUT

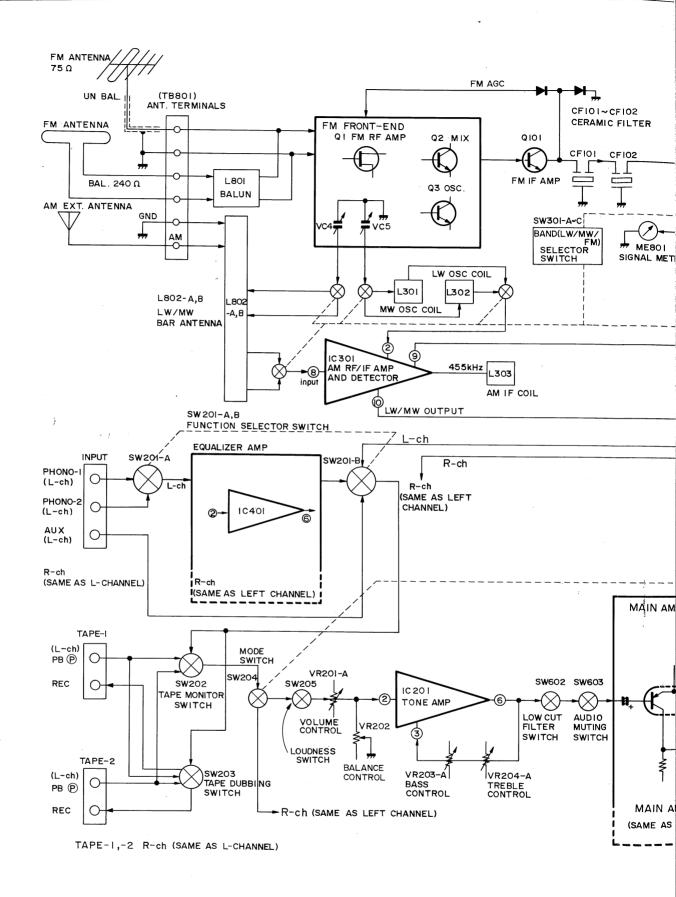
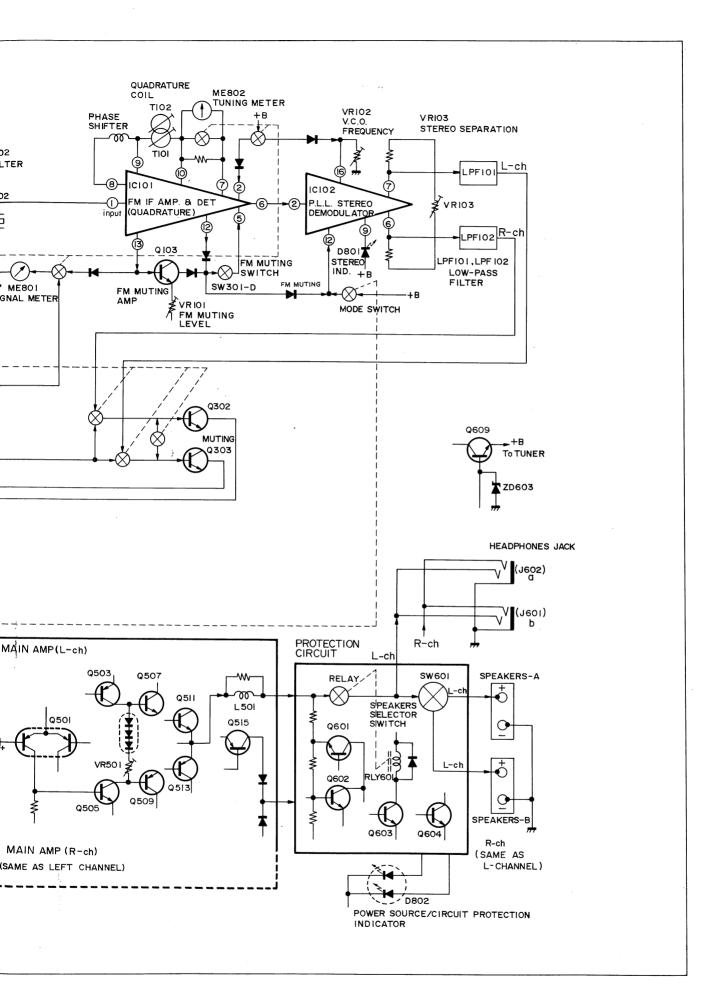


Figure 6 BLOCK DIAGI



**CDIAGRAM** 

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(1) B

(2)

FM

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signa

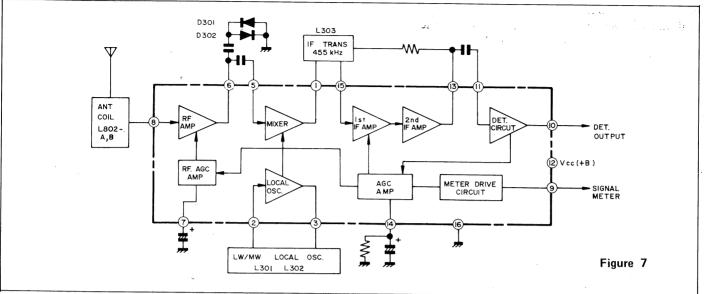
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# CIRCUIT DESCRIPTION

# AM SECTION

#### (1) Block Diagram of IC301



(2) Circuit Description

The block diagram of IC301 is indicated as above. AM broadcast signal caught by the antenna coil L802 enter the pin (8) of IC301 and is amplified by RF amplifier to be supplied to the mixer via the overload diodes D301 and D302. Intermediate frequency selection element making use of the ceramic filter L303 is employed as the load for the mixer. AM signal, after being amplified by 1st IF amplifier and 2nd IF amplifier, is detected by the detector circuit. Besides, this IC circuit IC301 incorporates signal meter drive circuit to facilitate the tuning and the output at the pin (9) of IC301 is connected to the signal meter (ME801).

# FM RF SECTION

FM antenna input circuit has two input terminals (75 ohms and 240 ohms) thanks to impedance converter (balun), coil L801. The 75 ohms input terminal is used when FM antenna is connected to the unit by using a coaxial cable. The 240 ohms input terminal is used when FM antenna is connected to the unit by using a balanced feeder. Fig. 8 shows FM Front-End circuit. RF amplifying section consists of 1 FET and 2 transistors.

Transistor Q1 is FET and its function is nearly the same as of vacuum tube. Due to the adoption of FET, crossmodulation characteristic and spurious characteristic are remarkably improved compared with conventional transistor type. It is so devised that AGC voltage is applied to the terminal  $\overline{K3}$  of FM Front-End circuit ..... this results in that when input signal to FM antenna is strong, amplification degree of transistor Q1 is lowered so as to stabilize FM reception.

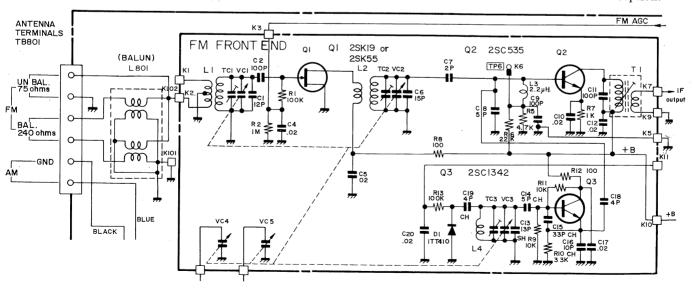


Figure 8 FM FRONT-END CIRCUIT

FET Q1 is FM high frequency amplifier. Transistor Q2 works as frequency mixer, in which high frequency signal coming from the FET Q1 and local oscillation frequency coming from the transistor Q3 are mixed to produce 10.7 MHz IF signal which will enter IF tuning transformer T1. The transistor Q3 is for the local oscillation and it applies oscillation voltage to the base of transistor Q2 via capacitor C18 (4pF).

Therefore, coil L1 is for antenna tuning, coil L2 is for FM RF amplification and tuning and coil L4 is for local oscillation.

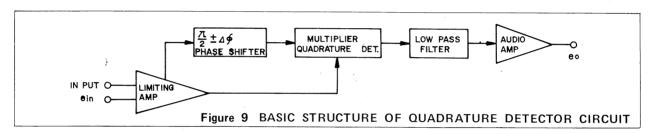
#### FM IF SECTION

FM IF section consists of 1 IC (integrated circuit), 1 transistor and 2 ceramic filters. Transistor Q101 is FM IF amplification and AGC amplification transistor, which is to amplify IF signal which has been converted into 10.7 MHz signal at FM front end section. This 10.7 MHz IF signal is given a higher selectivity since it runs through the concentrated selective elements, that is, ceramic filters CF101 and CF102. These filters function to amplify IF (intermediate frequency) signals giving no distortion and to assure a necessary selectivity. The IF signal is further supplied to the terminal ①of IC101, in which the gain of this signal is increased by about 66 dB by the three-stage differential amplifier thus being subjected to an appropriate limiter function.

# FM DETECTION SECTIONS (Quadrature Detector Circuit)

#### (1) FM Detector Circuit

This unit employs "Quadrature Detector" based on newly developed IC (Integrated Circuit), which is substituted for ratio detector and Foster-Seeley's detector that have been so far used. The basic structure of quadrature detector circuit is as shown in Fig. 9.



With this detection system, the multiplier (quadrature detector) circuit receives two types of input signals, one is the signal which has been amplified by the limiting amplifier and another which has passed through the phase shift circuit. (about  $\pi/2$ ). Thus, the quadrature detector circuit produces demodulation signal.

The term "quadrature" is resulted from that the phase difference between these two signal is  $\pi/2$ . The multiplier consists of doubly balance circuit as shown in the following circuit drawing. Phase characteristic of the phase shift circuit is as shown in Fig. 11.

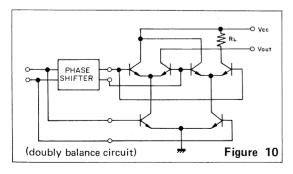
This circuit is featured by:

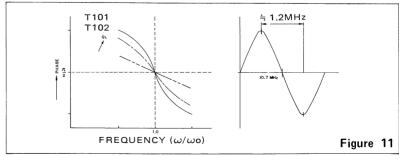
- (1) Good linearity and low distortion.
- (2) Operates on small signal and less higher harmonics.
- (3) Wide-band detection of as much as 1.2 MHz.

Therefore, this circuit assures low distortion even with the overmodulation of more than 100% thereby reproducing high quality sound.

Actually saying, the detecting circuit SA-2121H uses L104 as phase-shift coil. T101 and T102 are 10.7MHz tuning quadrature coil.

Detection output appears at the terminal 6 of IC101 and it is supplied to the terminal 2 of P.L.L. multiplex integrated circuit IC102.





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1) Features of P.L.L. stereo demodulator circuit.

This set incorporates a stereo demodulator circuit that comprises IC's with the PLL (Phase Locked Loop) system applied. The PLL (Phase Locked Loop) FM demodulator circuit is provided with such characteristics as mentioned below.

In order to demodulate stereo composite signals, it is necessary to take a 19 kHz pilot signal out of the stereo composite signals and to make it a 38 kHz signal.

Most of the conventional methods to obtain such a 38 kHz signal are frequency doubling ones which utilize a nonlinearity of the elements. Compared with the conventional type, the recently developed IC-ed demodulator provides more sufficient separation effects. However, since it also requires 2 or 3 coils like the conventional one, if even one of them is dislocated from the initially adjusted point due to a secular change the separation effects will be deteriorated. Moreover there is such a contradiction that the more the efficiencies of the coils are increased enough to withstand the outer pulse signals like automobil ignition noises, the more the coils suffer secular changes.

To eliminate such disadvantages as above, PLL (Phase Locked Loop) system is employed in the method to make a 38kHz signal using a 19kHz pilot signal.

The PLL system stereo demodulator gives such three merits as:

- 1. Since the phases of a pilot signal and a 38kHz signal are automatically made the same with each other, the deterioration of separation effect is strongly minimized.
- 2. Since only one of variable resistor, being newly employed, plays the role of 2 to 3 pieces of conventional coils, troubles of the parts due to secular changes are decreased. In addition, even if this variable resistor is slightly dislocated, the separation effect will never be deteriorated because of the merit as mentioned in 1 by which the automatic phase adjustment is assured.
- 3. Compared with the conventional one, the PLL system demodulator shows a more noise withstanding characteristic since it has such performances as the selection of frequencies and the continuity of oscillation frequencies (short-time memory), thus assuring a stable stereo demodulation.

# 2) FM stereo demodulator circuit of SA-2121H.

IC102 is an integrated circuit for P.L.L. stereo demodulation and its block diagram is as shown in Fig. 12. V.C.O. free-running frequency is to be adjusted to 76 kHz by adjusting semi-fixed resistor VR102 (10K ohm). TP107 is the test point for frequency observation. (See the paragraph "Adjustment" described later.) During LW/MW reception, +B voltage is supplied to the terminal 16 of IC102 through diode D106 and resistor R138 so that oscillation frequency of V.C.O. will be stopped. Semi-fixed resistor VR103 (220K ohm) aims at the adjustment of stereo separation and with this resistor it is possible to minimize crosstalk to the opposite channel. +B voltage is supplied to the terminal 12 to force stereo signals to become monaural ones.

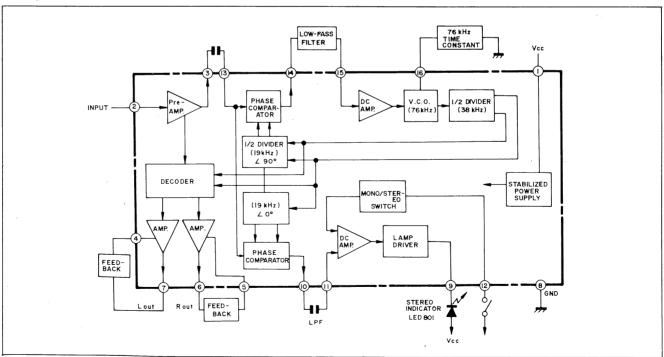


Figure 12

# MUTING CIRCUIT

SA-2121H, IC101 incorporates muting circuit and this circuit is so igned that if FM input signal to the antenna becomes about 20 dB en the muting switch (SW301-D) is kept at "ON", the muting is released the signal appears at the output without undergoing muting. The ting release signal is produced by addition of two signals, one is the put signal at the pin (12) of IC101 and another is signal meter signal at pin (13) which will undergo polarity inversion by the transistor Q103 these two signals are applied to the pin (5) of IC101 via the muting ch (SW301-D).

i-fixed resistor VR101 is adjustable to release the muting when the t signal from the antenna terminal becomes about 20 dB. 13 shows the output voltage of two outputs, one is at the pin (12) C101 and another, at the collector of transistor Q103, to be added ach other.

signal (to release the muting) is then supplied to the terminal (12) of . stereo multiplex demodulator integrated circuit IC102 to make o signal be forced to monaural signal.

# PASS FILTER

01 and LPF102 are low-pass filters to remove carrier s (19 kHz and 38 kHz) leaking from the stereo olex IC102. The characteristic is as shown in the

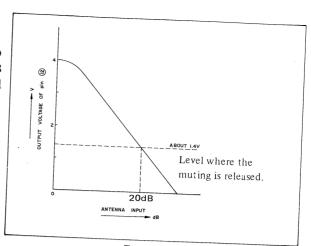


Figure 13

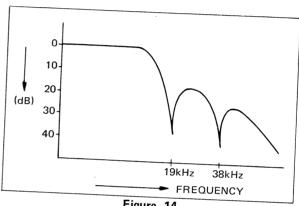


Figure 14

# TONE A

The tone differentia both highe The power in which designated and outpu reduction to control in particula condition s can be min

# **EQUALIZER**

The equalizer 1-stage and higher gain an The power sup in which the designated to 1 and output sig reduction of re Signal coming the function se capacitor C401 IC401 to be out of the term capacitor C415 switch (SW201is applied to circuit used for Composed of re which are precis aiming at "RIA deviation to ± Resistor R417 from discharging at the time of Capacitors C407 interference nois

#### TONE AMPLIFIER CIRCUIT

The tone amplifier circuit is an integrated circuit (IC) of differential 1-stage and directly-coupled 3-stage, which assures both higher gain and lower distortion factor.

The power supply is of 2-power (positive and negative) system, in which the voltage at the input and output terminals is designated to be 0V. The coupling capacitor used for input and output signals is of the low leak type which enables reduction of residual noises. The variable resistor aimed to control bass and treble is able to control the resistance in particular when the set is kept in "mechanical center" condition so that beat characteristic at the tone flat mode can be minimized.

Signal coming from the function selector switch is once supplied to the tape monitor switch, mode switch, loudness switch, volume control (VR201-A, B) and balance control (VR202), and then to the terminal ② of IC201 via the capacitor C205. The signal is amplified in the IC201 to come out of the terminal ⑥ and it is applied to the filter circuit via the capacitor C217.

A part of the output signal of the coupling capacitor C217 is applied to the terminal ③ of IC201 through the tone NF circuit. The tone NF circuit consists of the bass control (VR203-A, B) and the treble control (VR204-A, B) which are to carry out intensification or attenuation respectively of bass and treble ranges. Each of the controls is adjustable every 2 dB.

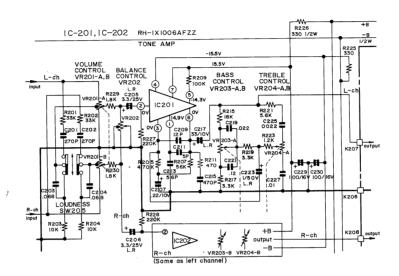


Figure 15

# **EQUALIZER AMPLIFIER CIRCUIT**

The equalizer circuit is an integrated circuit of differential 1-stage and directly-coupled 3-stage, which assures both higher gain and lower distortion factor.

The power supply is of 2-power (positive and negative) system, in which the voltage at the input and output terminals is designated to be 0V. The coupling capacitor used for input and output signals is of the low leak type which enables reduction of residual noises.

Signal coming from the terminal PHONO is applied, via the function selector switch (SW201-B), resistor R401 and capacitor C401, to the terminal ② of the integrated circuit IC401 to be amplified. The signal thus amplified comes out of the terminal ⑥ of IC401 and it will be applied, via the capacitor C415 and resistor R415, to the function selector switch (SW201-A). By the way, a part of such output signal is applied to the terminal ③ of IC401 through the NF circuit used for increase of "RIAA" characteristic.

Composed of resistor R413 and capacitors C411 and C413 which are precision parts having too small error. NF element aiming at "RIAA" characteristic is able to restrict "RIAA" deviation to ± 1.5 dB.

Resistor R417 is respectively to prevent capacitor C415 from discharging and to eliminate noise generation caused at the time of selecting the switches.

Capacitors C407 and C409 are for the purpose to prevent interference noises due to SW broadcasts, etc.

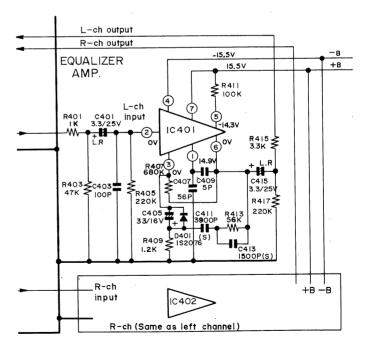


Figure 16

#### MAIN AMPLIFIER SECTION

The main amplifier consists of all-stage direct-coupled pure complementary output capacitorless circuit.

This main amplifier is designed to operate on the 2-power (positive and negative) supply system and so the speaker terminal output voltage becomes earth potential (0V) in terms of DC component. Therefore, with this amplifier it is not necessary to use a coupling capacitor for cutting off DC component although it has so far been required when the speaker is connected to the amplifier. Besides, it enables the amplification in a wider range from lower frequency to higher frequency. This is an origin of the term OCL (Output Capacitor-Less).

#### FEAUTURE OF PURE COMPLEMENTARY OCL CIRCUIT

Since this circuit is not using output capacitor, the frequency characteristic is kept uniform even at very low frequency band and the output impedance is low in any of frequency bands resulting in that the value of damping factor is made larger so that the braking efficiency of speaker is increased. With this circuit, since a 100 percent NF is assured when the frequency of signal is zero and the value of NF is determined at only one place when the frequency of signal is at low band, the function of circuit is stabilized.

#### MAIN AMPLIFIER

The main amplifier is OCL (Output Capacitor-Less) circuit in which the class "A" drive circuit consists of 1-stage differential amplifier circuit.

The signal coming from the filter circuit is amplified by differential amplifier Q501 (or Q502) via resistor R503 (or R504) and capacitor C501 (or C502). The transistor used in this differential amplifier is a PNP type low noise dual transistor (2SA798 ©) the characteristic of which is almost not affected by fluctuations of temperature so that the voltage resulted in the speaker terminal is protected against such fluctuations and it is kept always to minimized.

Signal thus amplified by the differential amplifier is further amplified by the class "A" audio amplifier Q505 (or Q506). Moreover, the signal is amplified for the half cycle at the driver amplifier stage consisting of NPN type transistor Q507 (or Q508) and PNP type transistor Q509 (or Q510). Then, the signal is further amplified for the half cycle at NPN type transistor Q511 (or Q512) and PNP type transistor Q513 (or Q514) to be supplied to the speaker. Transistor Q503 (or Q504) is constant-current circuit and its amperage is determined by D503. Transistor Q503 (or Q504) is constant-current circuit to supply constant current so that the load applied to the class "A" driver Q505 (or Q506) will be reduced thus the gain being increased. As a result of the gain of Q505 (or Q506), being increased by Q503 (or Q504), plenty of NF is produced and so that distortion is lessened. NF factor of NF circuit is determined by resistors R513 (or R514) and R521 (or R522), and the higher NF factor, the higher is the gain. NF factor at the low frequency band is determined by capacitor C507 and resistor R513.

Transistor Q503 (or Q504) and Diode D503 (or D504) are to cause the bias of class "B" drive stage and to produce idling current of  $33 \sim 100$  mA so that cross-over distortion due to class "B" operation is eliminated. The idling current is to be adjusted by semi-variable resistor VR501 (or VR502).

Resistor R553 (or R554) and capacitor C513 (or C514) are to keep the power amplifier stabilized when given no load. Coil L501 (or L502) functions to prevent of high-frequency oscillation. Transistor Q515 (or Q516) works as protection circuit.

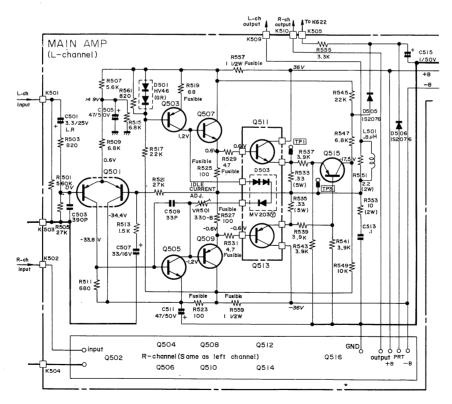


Figure 17 MAIN AMPLIFIER CIRCUIT

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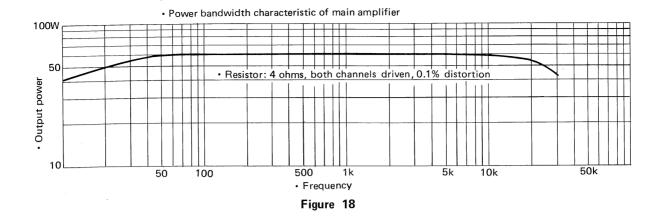
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# PROTECTION CIRCUIT (RELAY CIRCUIT)

The protection circuit used in this set is so designed as to function in the following instances:

- (1) It protects the speaker against possible shock noise caused when the power switch is turned on.
- (2) It protects the speaker against possible shock noise caused when the power switch is turned off.
- (3) It functions when DC voltage is generated at the speaker terminal (for instance, when DC voltage gets unbalanced due to a trouble inside the amplifier.)
- (4) It functions when the speaker terminals are shorted and the load impedance is lowered (for instance, when several speakers are connected in parallel to the amplifier.)

Next, we will explain the basic operations of the protection circuit.

The protection circuit is made of two circuits, namely.

Schmitt trigger circuit consisting of transistors Q603 and Q604 and abnormality detection circuit consisting of transistors Q601, Q602, Q515 and Q516.

As to Schmitt trigger circuit, when the base voltage of the transistor Q603 is lower, the transistor Q603 does not function; in other words, the relay does not function since it is given no current so that the speaker circuit is shut off. D802 is 2-color LED (Light Emitting Diode) and it is so designed that it will light up green when the relay is turned on and red when the it is turned off.

Transistors Q601 and Q602 are detection circuits respectively of negative signal and positive signal and each of the two is turned on when given the signal to discharge the potential charged in the capacitor C605, so that the base voltage of the transistor Q603 is decreased and the relay is turned off.

Capacitors C603 and C604 and resistors R606 and R605 are a low-pass filter which prevents mis-operation of the relay due to sound signal. And diode D603 is to absorb the voltage possibly induced when the relay turns on or off.

The above will be further described in detail:

(1) When the power switch SW801 is set to "on" position, the base voltage of Schmitt trigger transistor Q603 is increased by means of resistors R609 and R608 to have the transistor Q603 be turned on, and thus the relay starts to function. During this process, it is so designed that: since capacitor C605 is being inserted to the base of the transistor Q603, the base voltage of Q603 is kept lower than its emitter voltage until the power supply voltage to the protection circuit will become stabilized and so, during that time, the transistor Q603 is kept off so that the relay does not function since it is given no current. Thus time constant of the relay is determined so that the relay begins to function about 3 to 5 seconds after the power switch is turned on --- in a while the circuits are stabilized to make alive the speakers' connection.

Simultanecously with the above operation, another Schmitt trigger transistor Q604 is turned on and a current runs in the direction which makes the light emitting diode D802 be lit in red.

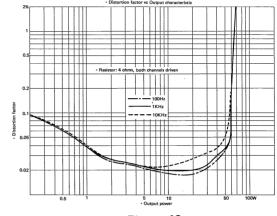


Figure 19

When the power supply voltage is thus stabilized, voltage is charged in the capacitor C605 via resistors R609 and R607 to make the base voltage of the transistor Q603 reach the working point so that the transistor Q603 becomes turned on (at the time, the transistor Q604 is turned off.) A current runs in the relay and the relay begins the operation so that amplifier output will be connected to the speaker terminal. At the time, a current coming from the transistor Q603 runs in the direction which makes the light emitting diode D802 be lit in green.

- (2) The protection circuit is so designed that when the power switch is kept at "on" position, the transistor Q602 is unable to be turned on because a negative voltage coming from the negative rectifier circuit composed of diode D602 and resistor R604 is balanced to a positive voltage coming from the resistor R601. Contrary to the above, when the power switch is set to "off" position, the protection circuit is so designed that: a negative voltage is attenuated faster than a positive one as result of the determination of time constant and so the positive voltage is supplied to the base of transistor Q602 and thus the transistor Q602 is turned on. Then the capacitor C605 begins to discharge so that the base voltage of transistor Q603 is decreased and the transistor Q603 is turned off --- no current runs in the relay and connection of the amplifier output to the speaker terminal is cut off. In short, the protection circuit functions to cut off connection between the amplifier output and the speaker terminal as soon as the power switch is switched off.
- (3) If there appears DC voltage (positive or negative) at the speaker terminal, positive or negative voltage is applied to the transistors Q601 and Q602 through the resistors R605 and R606. As to the positive voltage, it is applied to the base of transistor Q602 via the resistor R603 to have the transistor Q602 be turned on. As to the negative voltage, the emitter voltage of transistor Q601 becomes lower than its base voltage to make the transistor Q601 be turned on. This results in that no current runs in the relay so that connection of the amplifier output to the speaker terminal will be cut off.
- (4) If the speaker terminals are shorted or the load impedance is lowered (for instance, due to connection of the speakers of less than 4 ohms), this can cause a large current to run through the power transistor to be damaged. This trouble can also be avoided by the protection circuit.

If it is supposed that a current of more than the rated value runs in the power transistor, the protection circuit tends to detect abnormal voltage caused at the emitter resistors R533 and R535 (R534 and R536) of the power transistor so that the transistor Q515 (or Q516) is turned on. The voltage thus produced is applied to the base of transistor Q602 via the diode D505 (or D506) and resistor R555 and so the transistor Q602 is turned on. In this way, the protection circuit provides the same effect as said hereinbefore.

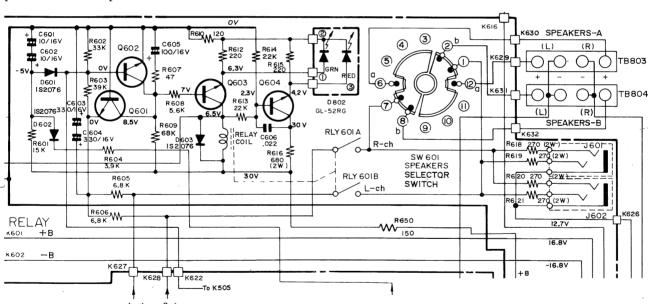


Figure 20 PROTECTION CIRCUIT (RELAY CIRCUIT)

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Power voltage of dio DC voripple Beside stability Capaciand tl

# POWER SUPPLY CIRCUIT

Power supply to the main amplifier section is depended upon the 2-power supply system. With this 2-power supply system, AC voltage coming from the power transformer T801 is subjected to rectification by the bridge full-wave rectifier circuit consisting of diodes D507, D508, D509 and D510 and then be smoothed by the low impedance dual-capacitor C520 and C521 to become DC voltage to finally be supplied to the main amplifier circuit section. The DC voltage thus smoothed is further applied to the ripple filter circuit to become stabilized so that it will be supplied to the tone circuit and equalizer circuit.

Besides, to both the FM circuit section and AM circuit section is also supplied the power voltage thus smoothed after it has been stabilized by the ripple filter circuit (transistor Q609).

Capacitors C516 to C519 are for the purpose to eliminate noise possibly caused with switching of the diodes D507 to D510 and that arising from the power transformer primary side.

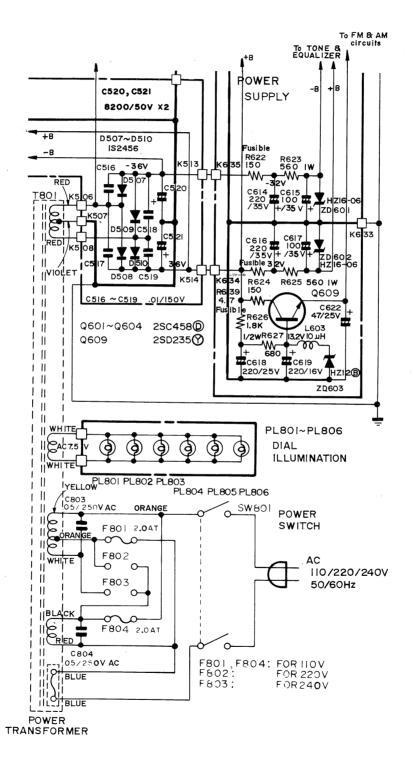


Figure 21 POWER SUPPLY CIRCUIT

# **ALIGNMENT INSTRUCTIONS**

Alignment is an exacting procedure and should be undertaken only when necessary. If alignment of AM (LW, MW) and FM is required, either section may be done first. The FM stereo section, however, should be done only if the FM monaural section is properly adjusted.

#### REQUIRED EQUIPMENT

- 1. Signal generator with a frequency range of 145 kHz to 1650 kHz; AM (MW, LW)
- 2. Signal generator with a frequency range of 86.1 MHz to 109.2 MHz; FM
- 3. Signal generator with a frequency output of 10.7 MHz ±0.5 MHz; FM
- 4. Vacuum tube voltmeter (AC-VTVM)
- 5. Sweep signal generator with a sweep range of at least 500 kHz and center frequency of 10.7 MHz with at least a 10.7 MHz marker may be used.
- 6. Oscilloscope with a wide range amplifier of approximately 100 kHz.
- 7. Test loops, a coil of any size wire, one turn or more; AM (MW, LW)
- 8. Vacuum tube voltmeter (DC-VTVM)
- 9. FM stereo signal generator.
- 10. Audio signal generator with a frequency range of 20 Hz to 100 kHz.
- 11. Frequency counter with a frequency range of approximately 100 kHz.

Notes: Allow the set at least five minutes to warm up before attempting alignment. During alignment keep the signal generator output at the lowest level that will maintain a usable output from the set.

For the adjustment of stereo separation, the FM stereo generator output is usually  $1,000\mu V$ . Incorrect grounding to the metal chassis may pick up an unwanted 10.7 MHz signal from the final IF stage, which will cause a regenerative sweep response on the sweep curve and result in misalignment.

Therefore always connect a ground to point.

Ground connection of signal generator

Chassis ground

Generator modulation (AM)

30%, 400 Hz

Generator modulation (FM)

40 kHz, 400 Hz

Generator modulation (FM stereo)

Ch. L. or Ch. R. 40 kHz, 1,000 Hz Mod.

### THE INSTRUCTION OF FM FREQUENCY ADJUSTMENT

In order to comply with FTZ rule: Nr. 358 S757, please fix the low end of dial frequency (87.5 MHz) and high end of dial frequency (107.9 MHz) on FM band, by adjusting oscillation coil (L4) and oscillation trimmer (TC3), repectively, as illustrated in Figure 22.

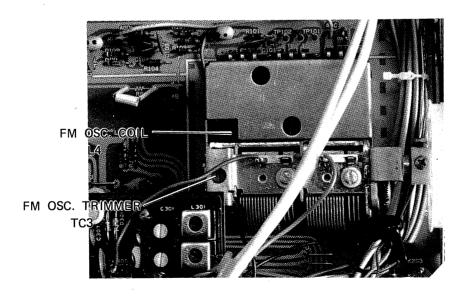


Figure 22 FM FRONT-END

# AF ALIGNMENT

- 1) Set the volume control to the position "minimum" and other switches to the position "normal".
- 2) Turn on the power switch of the set.
- Use DC VTVM to make sure that the voltage between TP3 and K515 (ground) and that between TP4 and K515 (ground) are within the range of  $\pm$  30 mV.
- 4) Only after the above check, it is possible to proceed with the next adjustments.

PROCEDURE NUMBER	ALIGNMENT	METER	OUTPUT INDICATOR	SETTING	ADJUSTMENT	REMARKS
1	Idle Current	DC V.T.V.M.	DC V.T.V.M. is connected between TP1 (TP2) and TP3 (TP4)	Volume is mini- mum position. Other knobs are normal position	VR501 (VR502)	15 mV

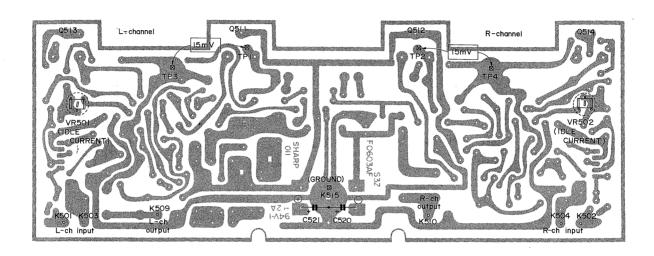


Figure 23 ALIGNMENT POINTS OF POWER AMP. BOARD

# AM IF ALIGNMENT (MW,LW)

PROCEDURE	SWEEP GENERATOR		DIAL POINTER	SELECTOR	SCOPE	ADJUSTMENT	REMARKS
NUMBER	CONNECTION	FREQUENCY		SETTING	CONNECTION	ADJUSTMENT	KEMAKKS
1	Connect AM sweep generator to the test point TP303 (VC4) and variable capacitor case (ground). Keep the input be closed as much as possible.	455 kHz	High end of Dial	Band Selector (MW)	Oscilloscope is connected between TP301 and TP302 (ground)	L303	Maximum response at 455 kHz Repeat 2 or 3 times.

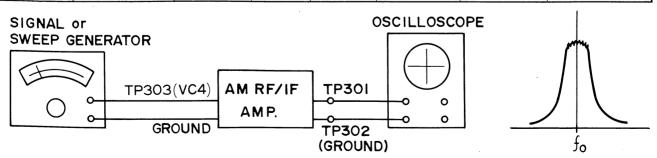
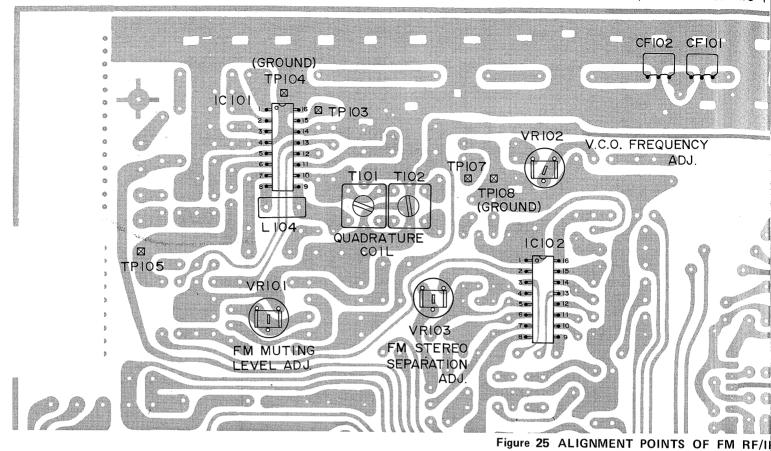


Figure 24 AM IF ALIGNMENT EQUIPMENT CONNECTIONS

PROC DURI NUM



CN302

TP302

TP302

TP302

TP302

TRIMMER

TTC304)

TC302

LW OSC

TRIMMER

TTC304)

TC302

LW OSC

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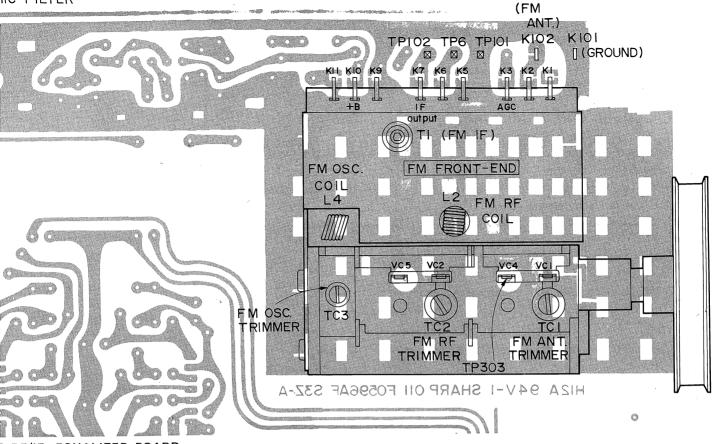
TRIMMER

TRIMMER

XA9

TVAP-A03

Figure 26 ALIGNMENT POINTS OF AM RF/IF BOARD



1 RF/IF, EQUALIZER BOARD

## MW RF ALIGNMENT

Rotate the core of LW oscillation coil L302 fully clockwise.

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PROCE- DURE NUMBER	TEST STAGE	SIGNAL GI	ENERATOR FREQUENCY	DIAL POINTER SETTING	SELECTOR SETTING	SCOPE CONNECTION	ADJUSTMENT	REMARKS
1	Band	Radiated signal as small as possible	515 kHz Modulated	Low end of Dial	Band Selector (MW)	Oscilloscope is connected between TP301 and TP302 (ground)	Oscillator Coil L301	Adjust for maximum output
2	Coverage	Radiated signal as small as possible	1650 kHz Modulated	High end of Dial	Same as above	Same as above	Oscillator Trimmer TC303	Same as above Repeat steps 1 and 2,2 or 3 times.
3	m 1 i	Radiated signal as small as possible	1400 kHz Modulated	1400 kHz	Same as above	Same as step 1	Antenna Trimmer TC301	Same as step 1
4	Tracking	Radiated signal as small as possible	600 kHz Modulated	600 kHz	Same as above	Same as step 1	Antenna Coil L802-B	Same as above Repeat steps 3 and 4, 2 or 3 times.

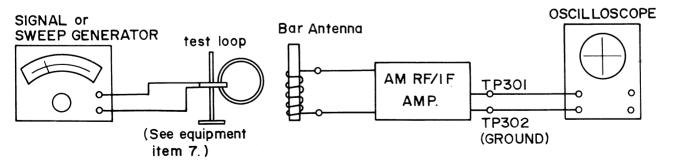


Figure 27 MW/LW RF ALIGNMENT EQUIPMENT CONNECTIONS

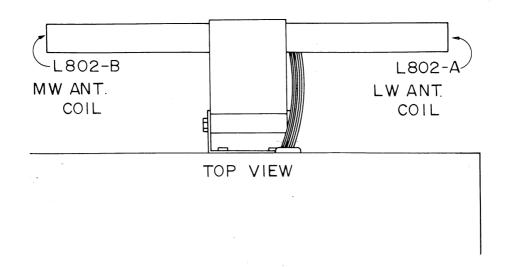


Figure 28 LW/MW BAR ANTENNA

# LW RF ALIGNMENT

PROCE-	TEST	SIGNAL GENERATOR		DIAL	SELECTOR	SCOPE	A D HIGENENE	REMARKS	
DURE NUMBER	STAGE	CONNECTION	FREQUENCY	POINTER SETTING SETTING		CONNECTION	ADJUSTMENT	REMARKS	
1	Band	Radiated signal as small as possible	145 kHz- Modulated	Low end of Dial	Band Selector (LW)	Oscilloscope is connected between TP301 and TP302 (ground)	Oscillator Coil L302.	Adjust for maximum output	
2	Coverage	Radiated signal as small as possible	385 kHz Modulated	High end of Dial	Same as above	Same as above	Oscillator Trimmer TC304	Same as above Repeat steps 1 and 2,2 or 3 times.	
3	2	Radiated signal as small as possible	340 kHz Modulated	340 kHz	Same as above	Same as step 1	Antenna Trimmer TC302	Same as step 1	
4	Tracking	Radiated signal as small as possible	170 kHz Modulated	170 kHz	Same as above	Same as step 1	Antenna Coil L802-A	Same as above Repeat steps 3 and 4, 2 or 3 times.	
5		Same as above	145 kHz Modulated	145 kHz	Same as above	Same as step 1	Same as above	Same as above	

# **FM ALIGNMENT**

Set the FM Muting switch (SW301-D) at "OFF" position.

num

PROCE-	TEST	SIGNAL GENE	RATOR	DIAL	SELECTOR SETTING	METER CONNECTION	ADJUSTMENT	REMARKS
DURE NUMBER	STAGE	CONNECTION	FREQUENCY	POINTER SETTING				
1	IF (NOTE 1 and 2)		10.7MHz±500 kHz as small as possible.	High end of dial	Band Selector(FM), and mono	Connect an oscillo- scope to the test points TP103 and TP104 (ground).	T1	Rotate the core of T1 to adjust so that the waveform becomes symmetrical in right and left and attains the maximum in height and width.
. 2	Detector	Connect FM sweep generator, through 6PF capacitor, to the test point TP102. Connect the ground to the test point TP101.	Same as above	Same as above.	Band Selector(FM) and mono	Connect an oscillo- scope to the test points TP105 and TP104 (ground).	T101, T102	Rotate the core to adjust so that the waveform (Fig. 31)becomes symmetrical in the upper and lower with the best linearity.
З̀°	Band Coverage	FM Antenna	88MHz as small as possible (Modulated)	Low end of dial.	Band Selector(FM) and mono	Connect VTVM to the test points TP105 and TP104 (ground)	Oscillator coil L4	Adjust for maximum output.
4	(NOTE 1)	FM Antenna	108MHz (Modulated) as small as possible	High end of dial.	Band Selector(FM) and mono	Same as above	Oscillator trimmer TC3.	Same as above 3~4. Repeat 2 or 3 times.
5	Tracking	FM Antenna	90MHz (Modulated) as small as possible	90MHz	Band Selector(FM) and mono	Same as step 3	Antenna coil L1 and RF coil L2	Same as step 3
6	(NOTE 1)	FM Antenna	106MHz (Modulated) as small as possible	106MHz	Band Selector(FM) and mono	Same as step 3	Antenna trim- mer TC1 and RF trimmer TC2	Same as above 5~6. Repeat 2 or 3 times.

As to FM high frequency section (front-end section), there is no need to readjust the coil and trimmer since it has been factory-adjusted. It is allowed to readjust them only when there occurs a significant deviation about the preadjustment.

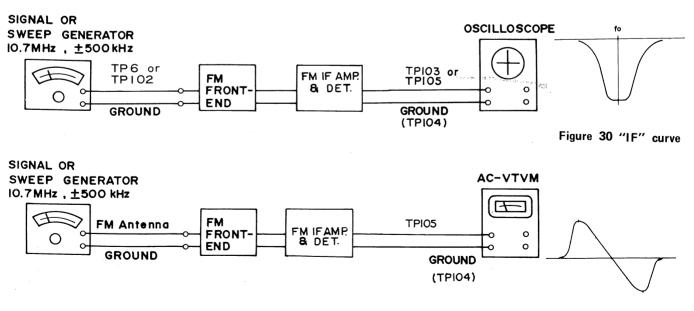


Figure 29 FM ALIGNMENT EQUIPMENT CONNECTIONS

Figure 31 "S" curve

# Note 2

The ceramic filter used for this set is available in 5 types and each of them is given a color indication to differentiate the central frequency from that of the others, as described below. In the actual use, be sure to make 2 ceramic filters of the same type (the same color) as a pair to put them in the set. When other ceramic filters than that given a red color indication (with the central frequency of 10.7 MHz) are used, note that with such filters the marker (10.7 MHz) of FM sweep generator will be deviated; therefore be sure to cut off the marker at the time of the adjustment.

Central Frequency (fo)	Green Black Red White Yellow	10.60 MHz ± 30 kHz 10.65 MHz ± 30 kHz 10.70 MHz ± 30 kHz 10.75 MHz ± 30 kHz 10.80 MHz ± 30 kHz
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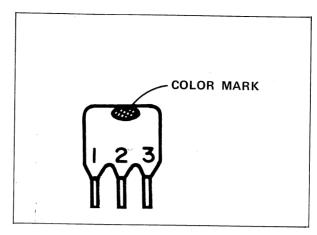


Figure 32

# FM TUNING METER ADJUSTMENT AND DISTORTION FACTOR ADJUSTMENT

- 1) Set the frequency of FM signal generator to 98 MHz (75 kHz deviation), fully close the output and connect such signal to the FM antenna terminal of the set through a dummy resistor of 240 ohms.
- 2) Connect a dummy resistor of 4 ohms to the speaker terminal of the set.
- 3) Set the switches and controls of the set to the respective positions shown below and turn on the power switch. [Audio muting-0dB, Low cut filter-off, Bass, Treble and Balance controls-center (zero), Mode-mono, Loudness-off, Volume control-min., Tape (monitor/dubbing)-source, Function selector-tuner, Band selector-FM, FM muting-off)
- 4) Keeping the output of FM signal generator be fully closed (that is, with no signal given), rotate the core of T101 to have the pointer of the tuning meter indicate the center (around "98 MHz" position.)
- 5) Adjust the output of FM signal generator to 60 dB, make the set be tuned to this signal so that the tuning meter indicates its center and under the condition, adjust the core of T102 so that the distortion will be minimized.
- Fully close the output of FM signal generator and make sure the pointer of the tuning meter is at the center.
- 7) Repeat the steps 1) to 6) until the best point will be found.

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## FM MUTING ADJUSTMENT AND FM STEREO V.C.O., SEPARATION ADJUSTMENT

- 1) Connect FM signal generator, through a dummy resistor of 240 ohms, to the FM antenna terminal of the set.
- 2) As to setting of the switches and controls, take the same procedures as in the step 3 "FM TUNING METER ADJUST-MENT AND DISTORTION FACTOR ADJUSTMENT".
- 3) Set the frequency of FM signal generator to 98 MHz (40 kHz deviation, 400 Hz) and the output to 20 dB.
- 4) Have the set be tuned in 98 MHz signal, turn on FM muting switch, rotate the semi-fixed resistor VR101 to adjust so that the muting is able to be cleared with the output of FM signal generator being 20 dB.
- 5) Set the output of FM signal generator to 60 dB (mono signal), place the mode switch of the set to the position "stereo" and let the set be exactly tuned to such signal. (FM muting switch is kept to the position "muting off".)
- 6) Connect VTVM between the test points TP107 and TP108 (ground) and further connect a frequency counter to output terminal of the said VTVM.
  - Make the test points TP105 and TP104 (ground) of the set be connected (shorted). Rotate the semi-fixed resistor VR102 to adjust so that the frequency counter will read 76.00 kHz ± 200 Hz. (After the adjustment; reset the connection between the test points TP105 and TP104.)
- 7) Connect FM stereo modulator to FM signal generator. At the time, the following should be set: modulation frequency; 1kHz (L + R; 20kHz, L-R; 20kHz, pilot (19kHz); 6kHz deviation).
- 8) Set the frequency of FM signal generator to 98 MHz and its output to 60 dB, tune the set in such signal so that the tuning meter will indicate the position "center". Set the modulator so as to cause modulation only in L-channel and consider the output of L-channel as 0 dB. Connect VTVM to the output terminal (R-channel side only) of the set and adjust semi-fixed resistor VR103 so that the separation becomes maximum (the output leaking to the opposite channel is minimized.)

Take the above procedures also for checking the separation of R-channel, then, adjust so that the separations of both channels will be equal to each other.

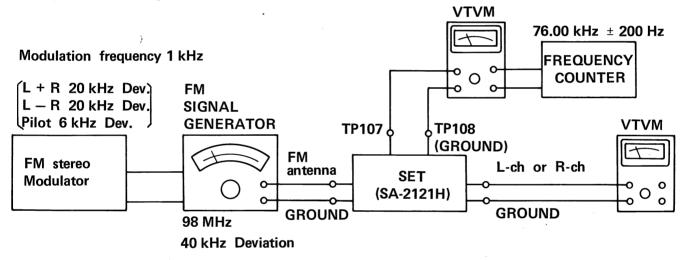
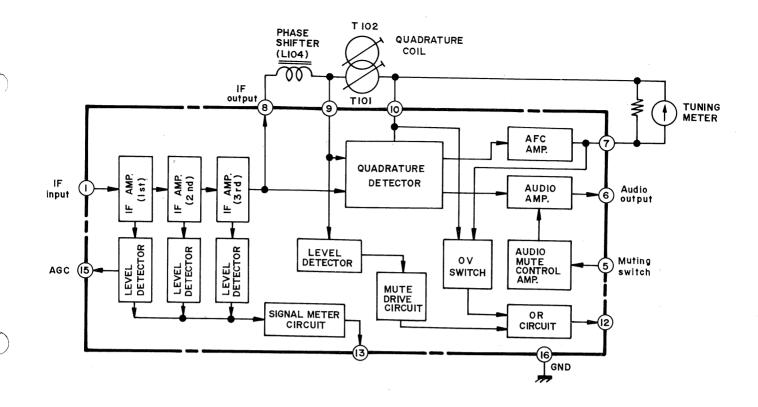


Figure 33 FM STEREO ALIGNMENT EQUIPMENT CONNECTIONS



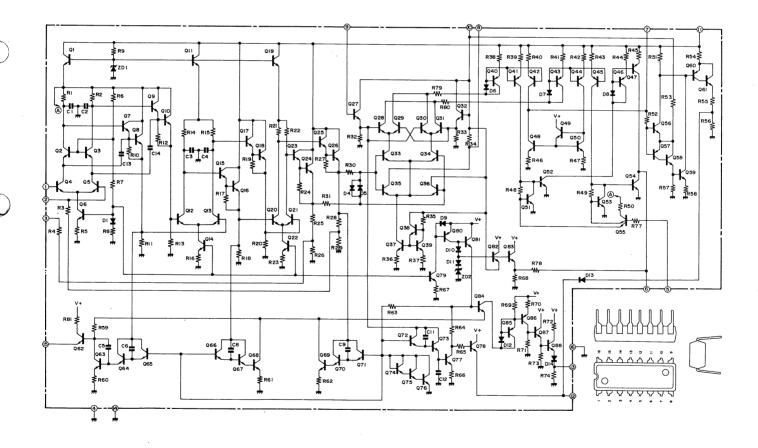
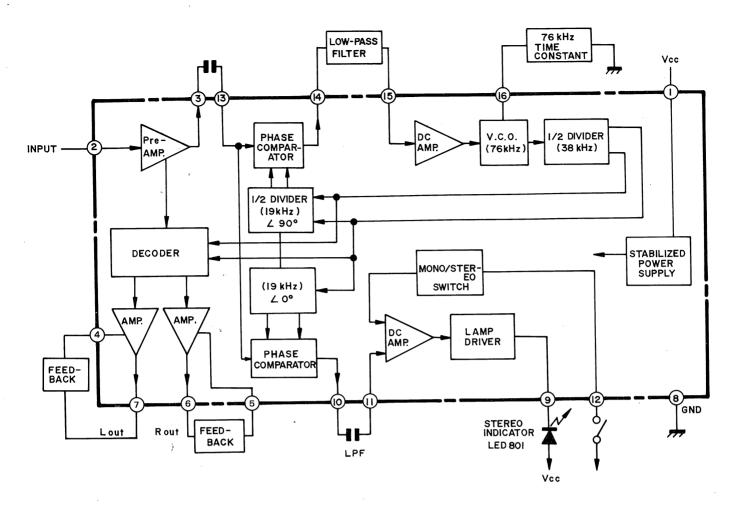


Figure 34 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC101)



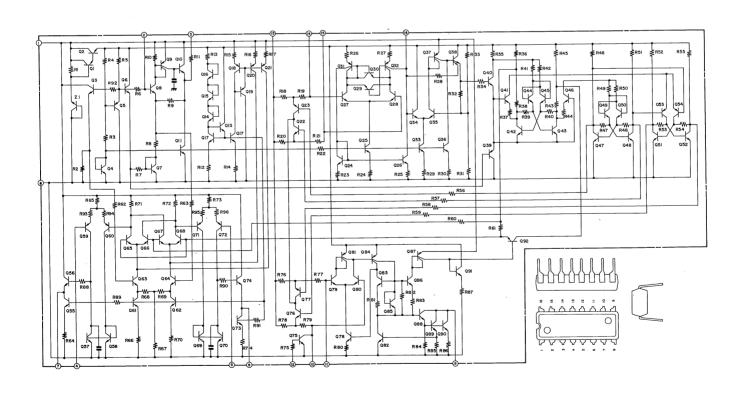
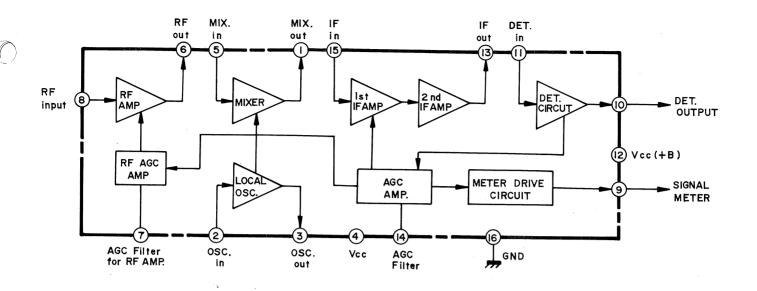
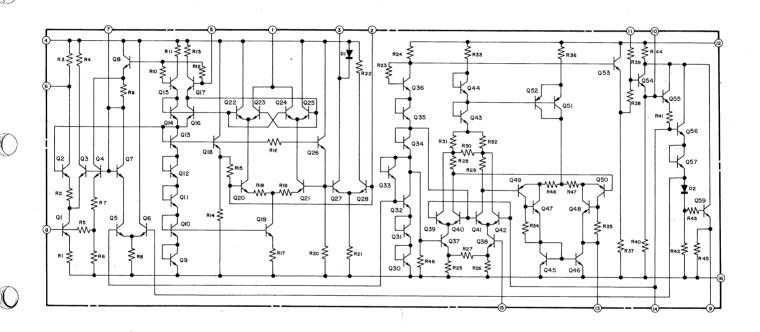


Figure 35 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC102)





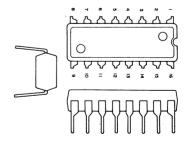


Figure 36 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC301)

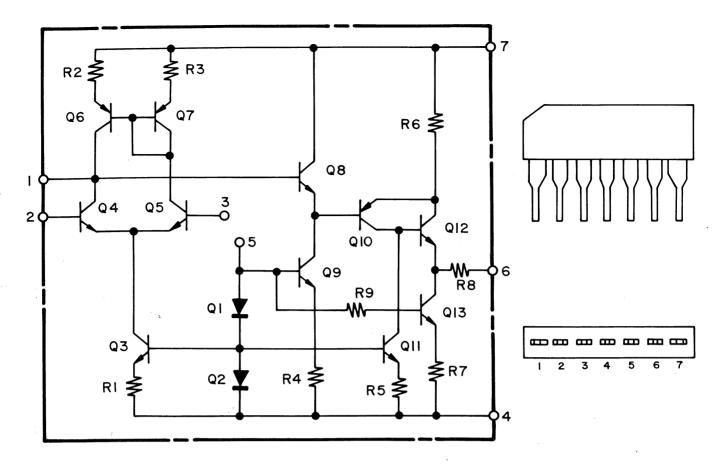


Figure 37 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC 201, IC 202, IC401 and IC402)

# NOTES ON SCHEMATIC DIAGRAM

1. Frequency range: FM; 76.5 to 108 MHz

MW; 520 to 1620 kHz

LW; 150 to 370 kHz

2. IF: FM 10.7 MHz, MW/LW 455 kHz

3. Resistor: To differentiate the units of resistors, such symbols as K and M are used: the symbol K means

 $K\Omega$  and the symbol M means  $M\Omega$  and the resistor without any symbol is  $\Omega$ -type resistor.

Besides, the one with "Fusible" is a fuse type.

4. Capacitor: To indicate the unit of capacitor, a symbol P is used; this symbol P means pF and the unit of

the capacitor without such symbol is  $\mu F$ . As to electrolytic capacitor, the expression "capacitance/withstand voltage" is used. The symbols LL and LR for the electrolytic capacitor respectively

mean low-leak type.

5. SW 201: It is Function selector (aux./phono-1/phono-2/tuner) switch ("aux." position)

6. SW 202: It is Tape monitor (tape 2/source/tape 1) switch ("source" position)

7. SW 203: It is Tape dubbing (2 + 1/source/1 + 2) switch ("source" position)

8. SW 204: It is Mode (stereo/mono) switch ("stereo" position)

9. SW 205: It is Loudness (off/on) switch ("off" position)

10. SW 301-A  $\sim$  C

(interlocked): It is Band selector (LW/MW/FM) switch ("MW" position)

SW 301-D: It is FM muting switch ("off" position)

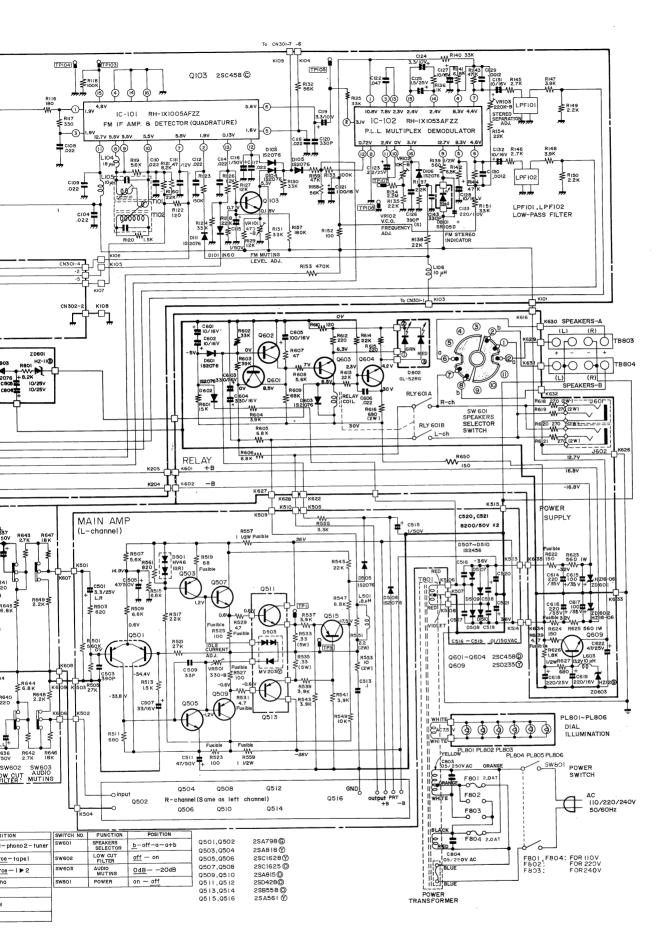
11. SW 601: It is Speakers selector (b/off/a/a+b) switch ("b" position)

12. SW 602: It is Low cut filter (off/on) switch ("off" position)

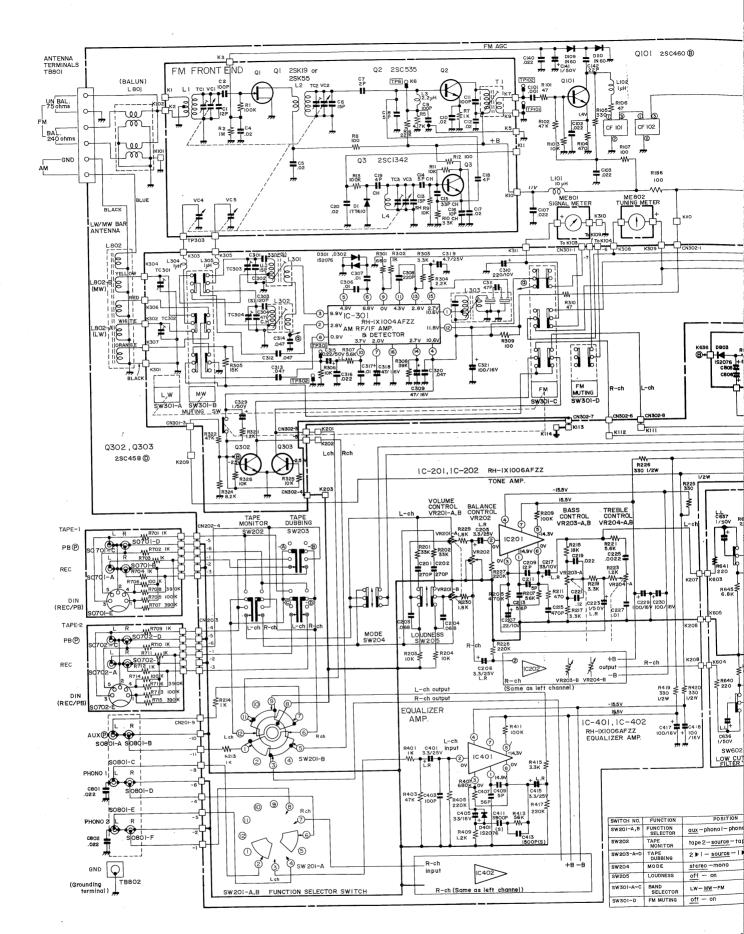
13. SW 603: It is Audio muting (0 dB/-20 dB) switch ("0dB" position)

14. SW 801: It is Power (on/off) switch ("off" position)

15. The indicated voltage in each section is the one measured by VTVM between such a section and the chassis with no signal being given.



notice.) C DIAGRAM



(Specifications or wiring diagrams of this model are subject to change for the improvement without prior noti

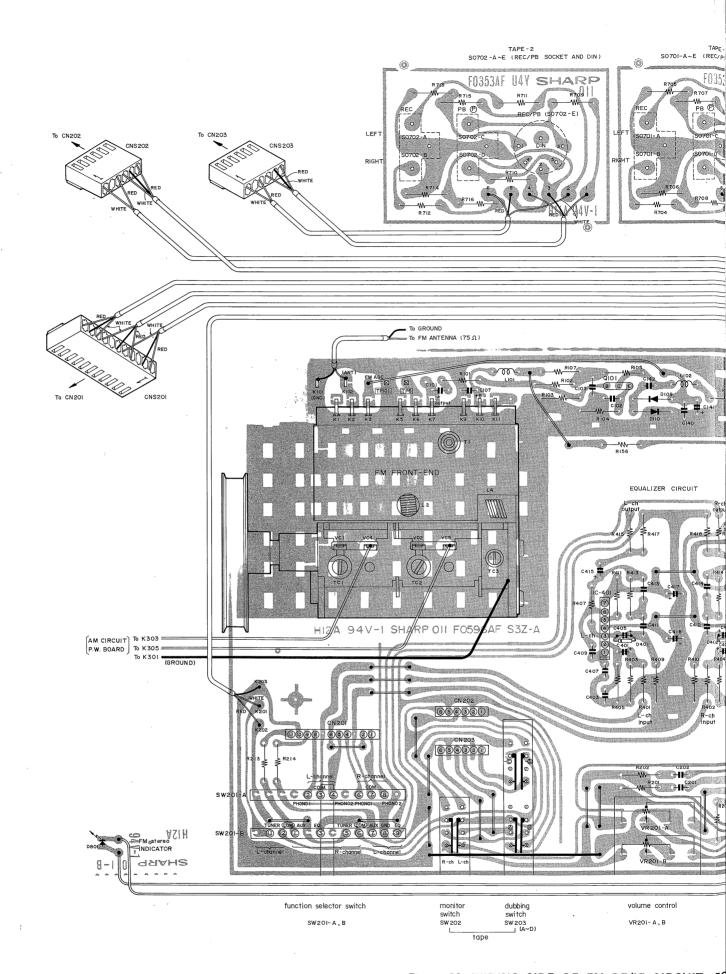
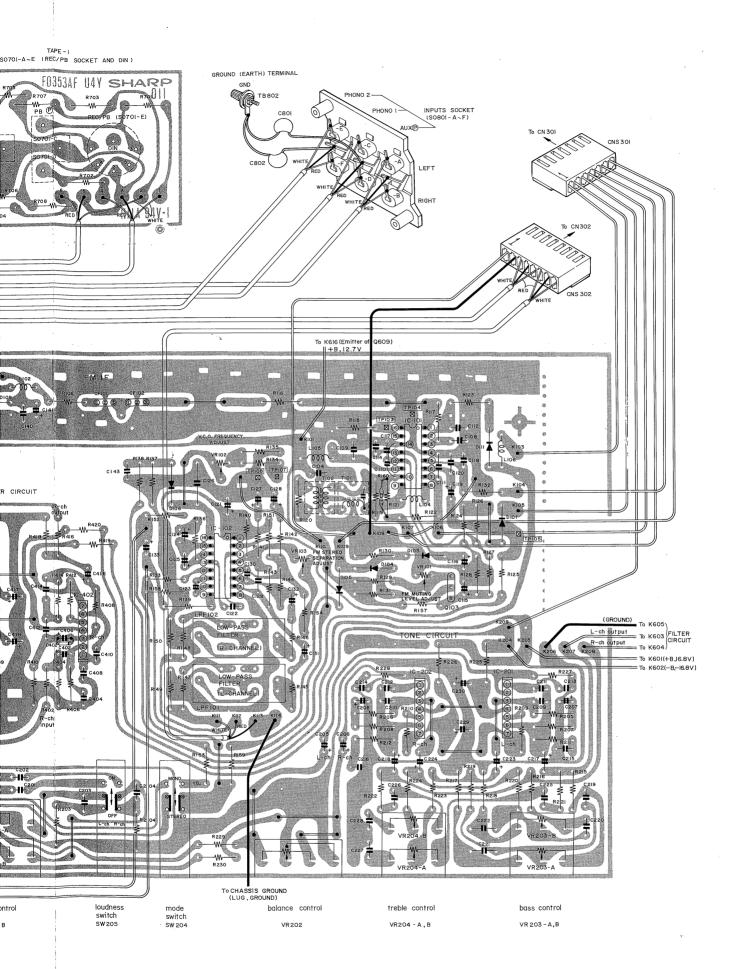


Figure 39 WIRING SIDE OF FM RF/IF CIRCUIT, EC



IRCUIT, EQUALIZER CIRCUIT, TONE CIRCUIT AND TAPE BOARDS

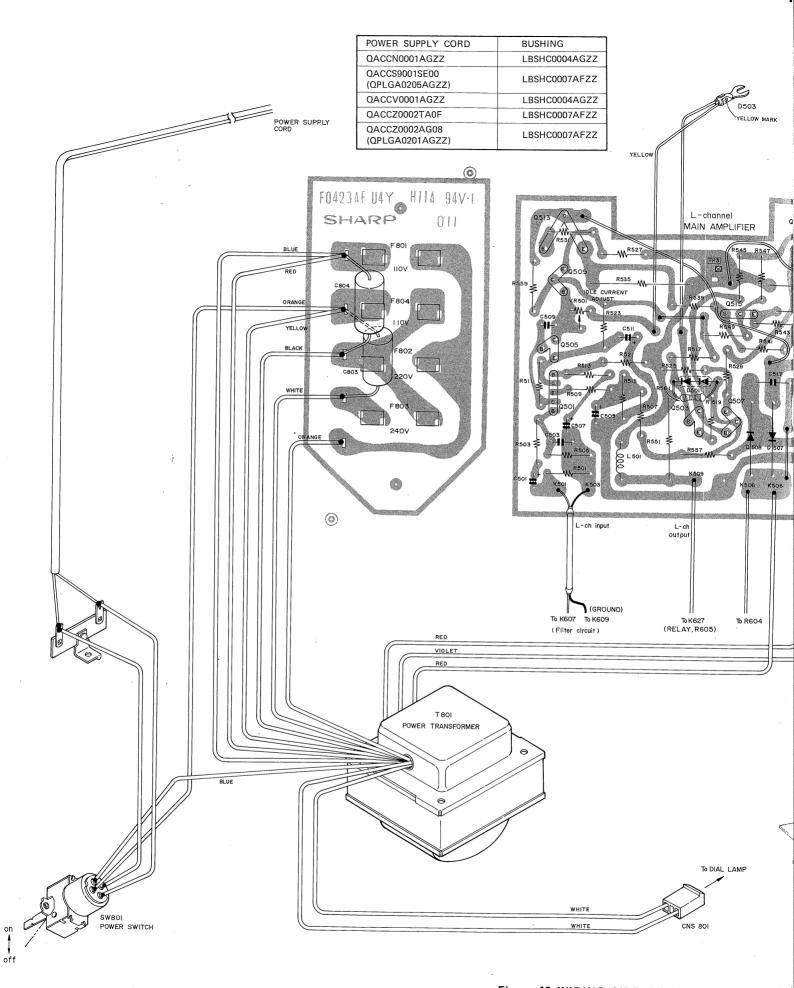
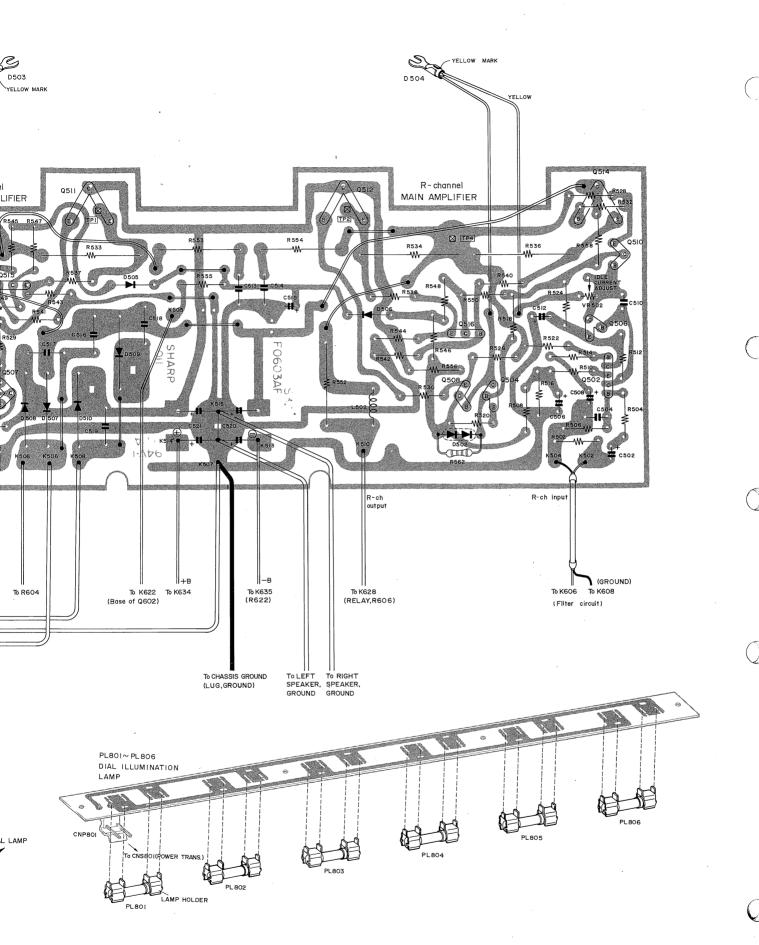


Figure 40 WIRING SIDE OF POWER AMP. AND I



AMP. AND LAMP BOARDS

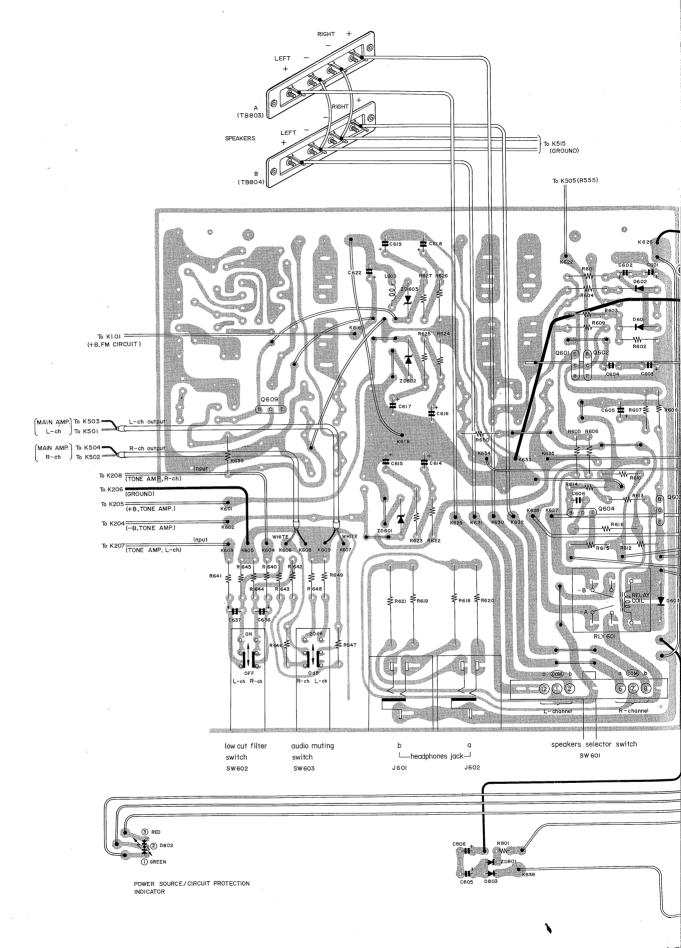
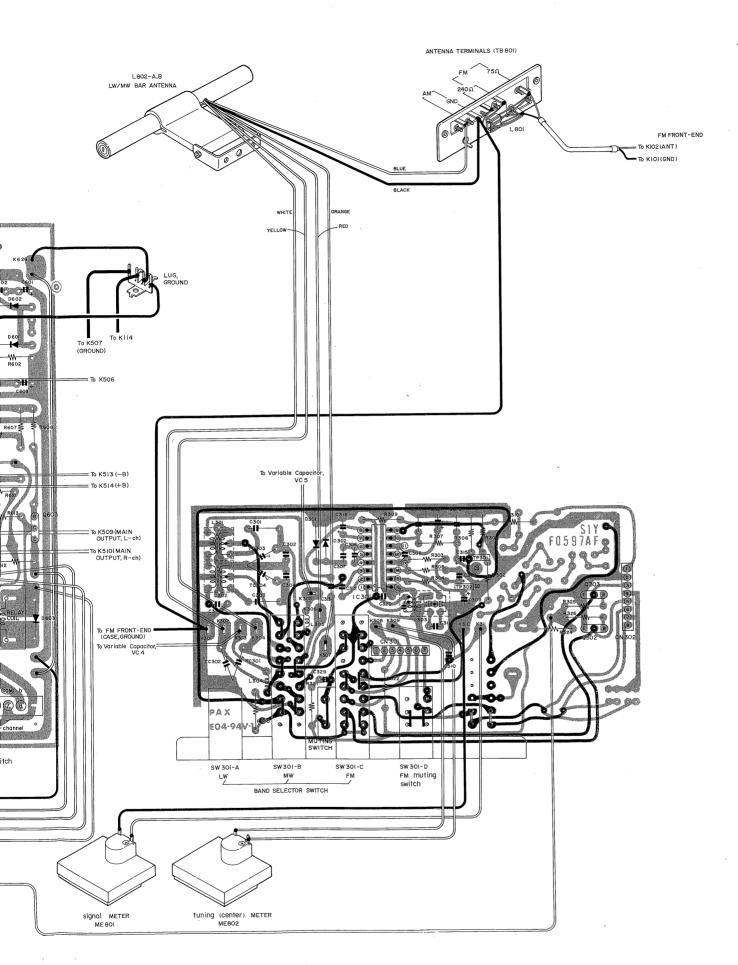


Figure 41 WIRING SIDE OF AM RF/IF



AM RF/IF CIRCUIT AND POWER SUPPLY BOARDS

### POWER TRANSISTOR REPLACEMENT

If it is necessary to replace audio output transistors, then follow these procedures to prevent reoccurrence of transistor failure.

- 1. Carefully remove transistor and mica insulator and clean all the silicone grease off the mica and the mounting area on the chassis. If the mica is damaged, then it must be replaced.
- 2. Remove the defective transistor and clean out the transistor mounting hole.
- 3. Put new silicone grease on the transistor mounting area of the chassis and on both side of the mica insulator. Mount the new transistor, being careful to tighten each transistor mounting screw evenly.

  Driving one screw tightly and then the other is likely-to-cause metal filings which may damage the mica or prevent necessary heat dissipation on chassis.
- 4. Before applying power to the new transistor, with an ohm meter check to see that there is no short between the transistor case and chassis.
- 5. As transistor VS2SB558-O/-1 and VS2SD428-O/-1 are almost similar in the shape. So pay attention to the mark of transistor when replacing the power transistor.

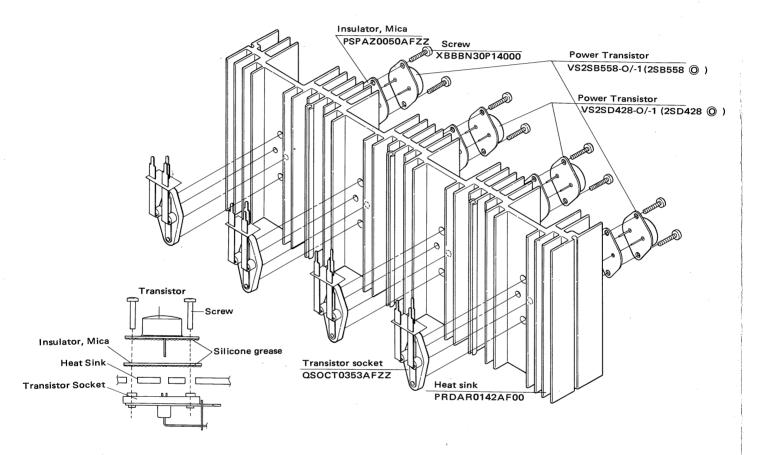
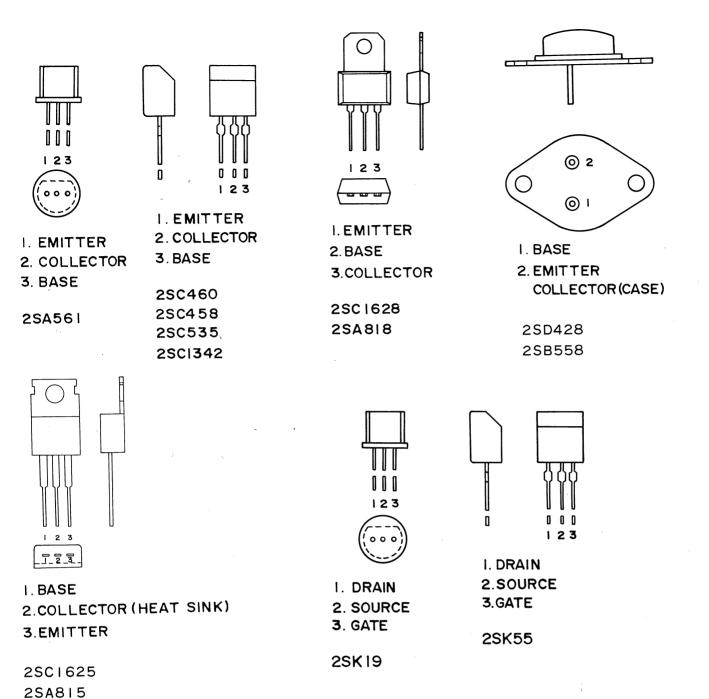


Figure 42 POWER TRANSISTOR REPLACEMENT



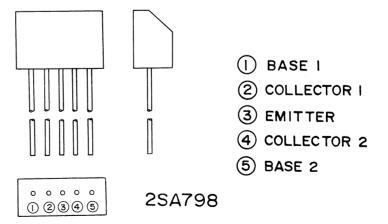
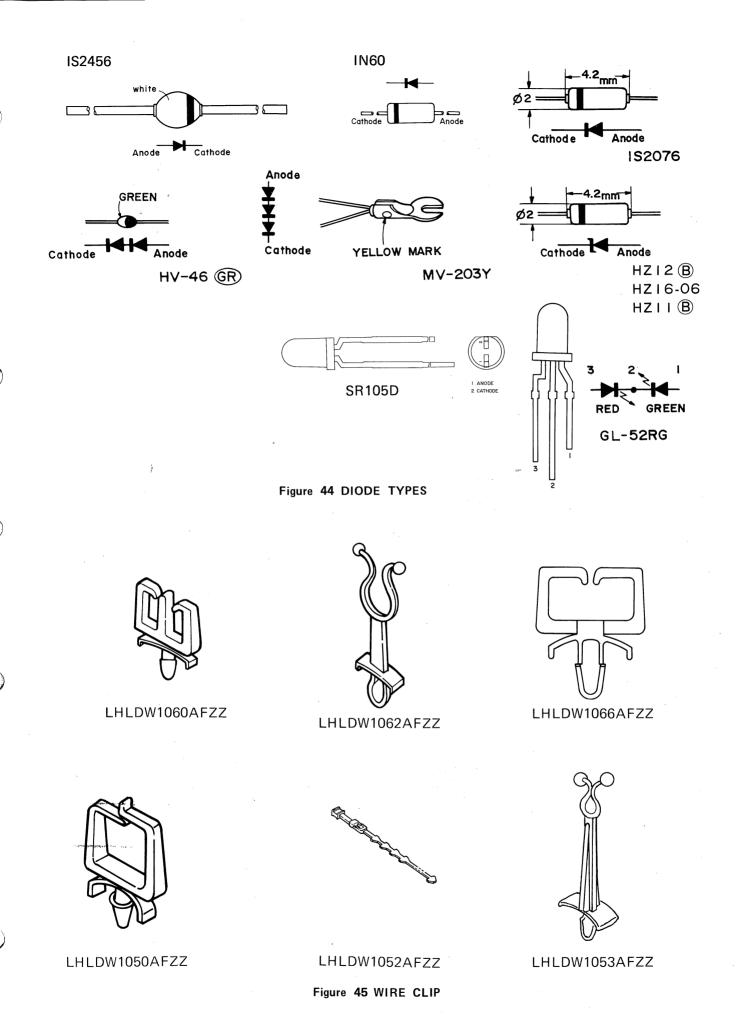
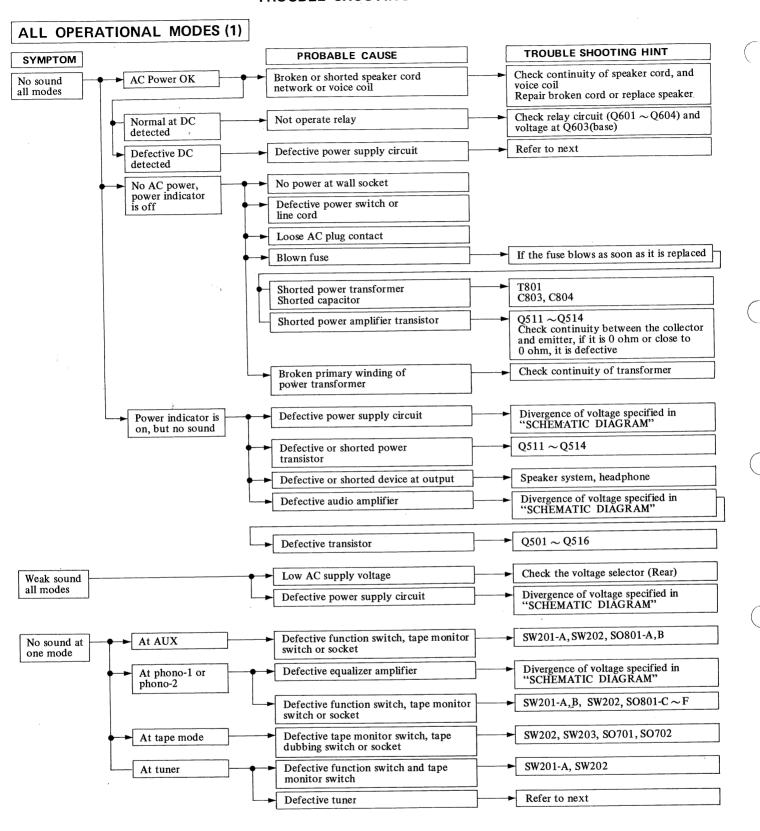
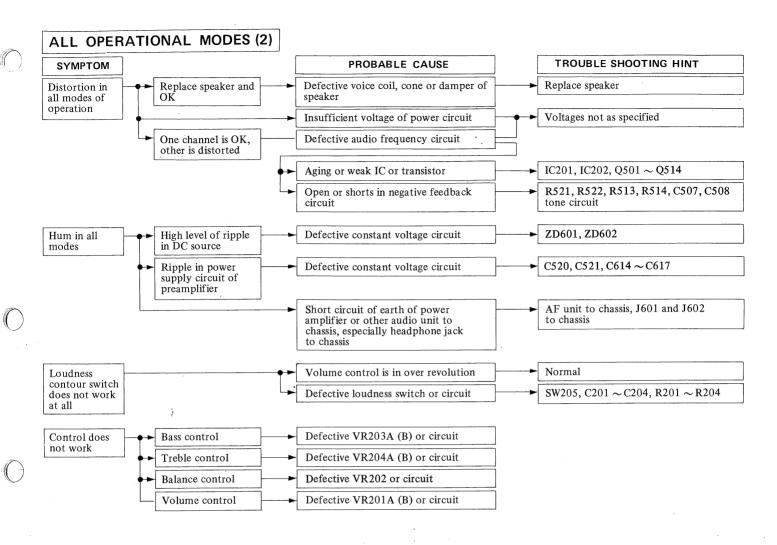


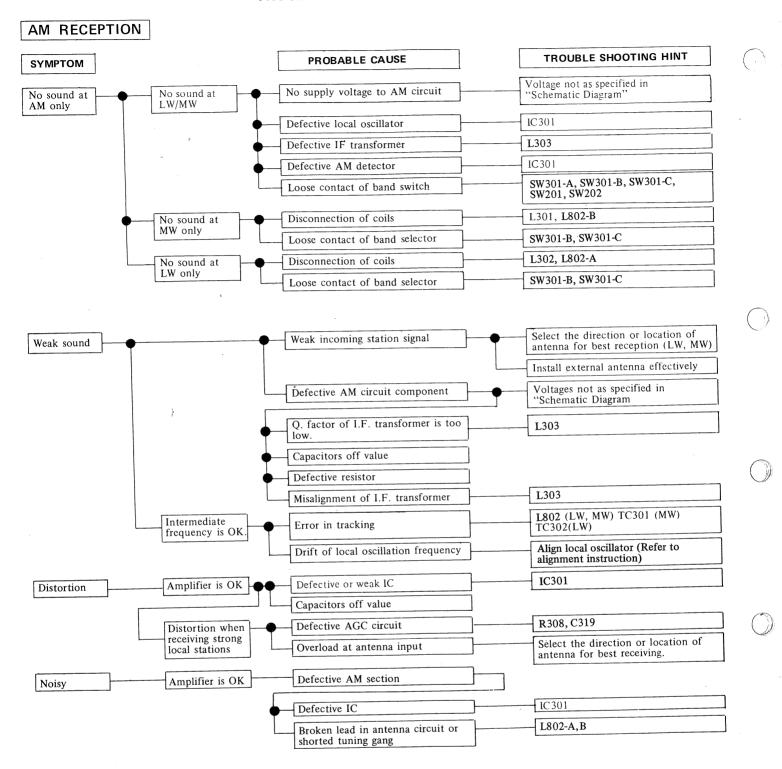
Figure 43 TRANSISTOR TYPES

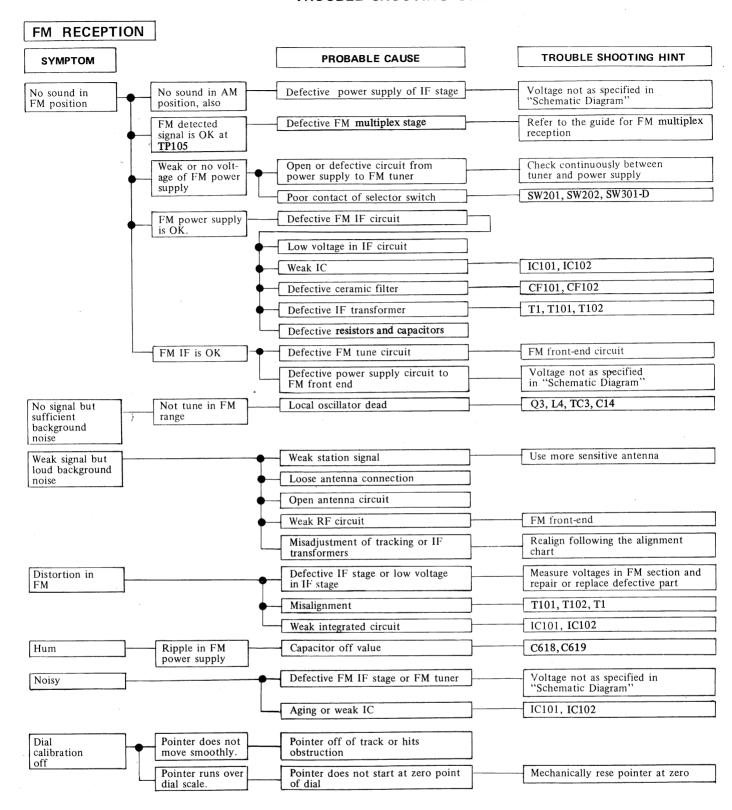
2SD235



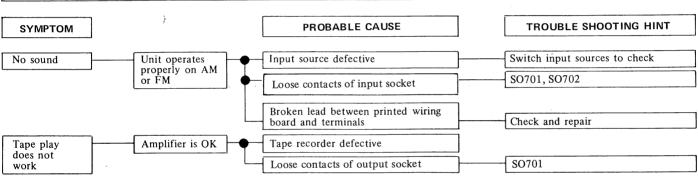


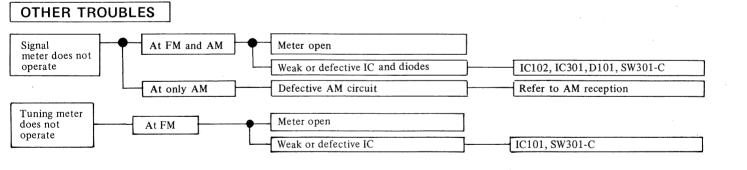






#### FM MULTIPLEX RECEPTION TROUBLE SHOOTING HINT PROBABLE CAUSE **SYMPTOM** SW301-C and E, SW201, SW202, SW204, SW602, SW603, SW601 Components in one channel physically No stereo Stereo light opetouching parts for other channel in tone circuit, main amp. or multiplex circuit rates normally. separation IC102 Aging or weak IC Stereo light does not light when receiving stereo Aging or weak semi-fixed resistor VR103 signal. Defective resistors and capacitors Distortion Weak or Defective IC IC102 Poor separation Stereo light does Defective IC IC102 not operate. Stereo light ope-Drift of VCO frequency Realign following the alignment chart rates normally Multiplex ampli-fier checks OK Stereo light Defective indicator lamp D801 does not Defective power circuit to stereo operate R139 light USING WITH EXTERNAL INPUTS OR OUTPUTS (TAPE, ETC.)





### REPLACEMENT PARTS LIST

### "HOW TO ORDER REPLACEMENT PARTS"

To have your order filled promptly and correctly, please furnish the following informations.

- 1. MODEL NUMBER 2. REF. NO.
- 3. PART NO.
- 4. DESCRIPTION

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE	
	INTEGRAT	TED CIRCUITS		D109	VHD1N60///-1	FM AGC (1N60)	AC	
				D110	VHD1N60///-1	FM AGC (1N60)	AC	
IC101	RH-IX1005AFZZ	FM IF Amplifier and Detector	AT	D111	VHD1S2076//-1	Voltage Detector (1S2076)	AB	
		(Quadrature) (HA1137W)		D301	VHD1S2076//-1	Overload (1S2076)	AB	
IC102	RH-IX1053AFZZ	P.L.L. Multiplex Stereo	AP	D302	VHD1S2076//-1	Overload (1S2076)	AB	
		Demodulator (HA1196)		D401,	VHD1S2076//-1	Speed-up	AB	
IC201,	RH-IX1006AFZZ	Tone Amplifier (TA7136P)	AH	D402 J	VIID152070//-1		110	
IC202				D501,	VHVHV46-G//-1	Varistor, Bias Stabilizer	AD	1
IC301	RH-IX1004AFZZ	AM RF/IF Amplifier and Detector (HA1138)	AS	D502		(HV-46 GR)		
IC401,		Equalizer Amplifier		D503, D504	VHVMV203Y//-1	Varistor, Bias Circuit (Idle Current) (MV-203 (Y))	AD	
IC401, IC402	RH-IX1006AFZZ	(TA7136P)	AH	D505,		, ,,		
10402 )		(111/1301)		D506	VHD1S2076//-1	Voltage Detector (1S2076)	AB	
	TRAN	NSISTORS		D507,				
		•		D508,	VHD1S2456//1D	Power Rectifier (1S2456)	AG	ĺ
Q101	VS2SC460-B/-1	FM IF Amplifier	AE	D509,	.,	,		
	}	(2SC460 B))		D510				
Q103	VS2SC458-C/-1	FM Muting Amplifier	AE	D601	VHD1S2076//-1	Voltage Detector, Protection	AB	
1		(2SC458 ©)				Circuit (1S2076)		
Q302	VS2SC458-D/-1	Muting (2SC458 D)	AE	D602	VHD1S2076//-1	Rectifier (1S2076)	AB	
Q303	VS2SC458-D/-1	Muting (2SC458 (D))	AE	D603	VHD1S2076//-1	Surge Current Provention	AB	
Q501,}	VS2SA798-G/-1	Dual Transistor, Differential Amplifier (2SA798 G)	AF	D001	WIIDGD 105D // 1	(1S2076)	1	
Q502 J Q503, J		Constant Current Circuit		D801	VHPSR105D//-1	Light Emitting Diode, Stereo Indicator (SR105D)	AD	
Q503,{ Q504	VS2SA818-Y/-1	$(2SA818 (\widehat{Y}))$	AH	D802	VHPGL-52RG/1F	Light Emitting Diode, Power	AH	
Q505,		Audio Amplifier, Class "A"		D002	VIII GE-32RG/11	Source/Circuit Protection	AII	
Q506	VS2SC1628-Y-1	(2SC1628 (Y))	AH			Indicator (GL-52RG)		
Q507,	V02001625 O 1		ATT	D803	VHD1S2076//-1	Noise Prevention (1S2076)	AB	
Q508	VS2SC1625-O-1	Drive Amplifier (2SC1625 (0))	AH	ZD601	VHEHZ16-06/1F	Zener Diode, Voltage		
Q509,	VS2SA815-O/-1	Drive Amplifier (2SA815 (0))	AH			Regulator (16.1 $\sim$ 17.1V)		١.
Q510 \	V525A015-O/-1	Drive Amplifier (25A513 (b))	All			(HZ16-06)		
Q511,	VS2SD428-O/-1	Power Amplifier (2SD428 (0))	AP	ZD602	VHEHZ16-06/1F	Zener Diode, Voltage		
Q512	,	• • • • • • • •				Regulator (16.1 $\sim$ 17.1V)		
Q513, Q514	VS2SB558-O/-1	Power Amplifier (2SB558 🔘 )	AR	ZD603	VHEHZ12-BBK-1	(HZ16-06)	AD	
Q514 ) Q515,		Voltage Detector, Protection		ZD003	VHEHZ12-DDK-1	Zener Diode, Voltage Regulator (12.7 ~ 13.5V)	AD	
Q516	VS2SA561-Y/-1	Circuit (2SA561 Y)	AF			(HZ12 (B))		
Q601	VS2SC458-D/-1	Protection Circuit, Voltage	AE	ZD801	VHEHZ11B///-1	Zener Diode, Noise Prevention	AD	
-	•	Detector (2SC458 D)				$(10.1 \sim 11.2 \text{V}) \text{ (HZ11 (B))}$		
Q602	VS2SC458-D/-1	Protection Circuit, Voltage	AE			,		ŀ
	\$ 	Detector (2SC458 (D))				COILS		
Q603	VS2SC458-D/-1	Protection Circuit, Switching	AE	L101	VP-LH100M0000	$10\mu\text{H}$ , +B Choke	AB	
0604	1/00000450 D/ 1	(2SC458 (D))		L102	VP-LH1R0M0000	1µH, Phase Compensation	AB	
Q604	VS2SC458-D/-1	Protection Circuit, Switching	AE	L104	RCILZ0052AFZZ	18µH, Phase Shifter	AB	
Q609	VS2SD235-Y/-1	(2SC458 (D)) Voltage Regulator, Ripple	AG	L105 L106	VP-LH100M0000 VP-LH100M0000	10μH, +B Choke 10μH, +B Choke	AB AB	
Q009	V3Z3DZ33-1/-1	Filter (2SD235 $(Y)$ )	AG	L301	RCILB0395AFZZ	MW Oscillator	AD	
		1 Htor (25D255 👽 )		L302	RCILB0411AFZZ	LW Oscillator	AD	
	D	IODES		L303	RCILI0209AFZZ	AM IF with Ceramic Filter	AH	
				L304	VP-LH1R0M0000	1μH, Choke	AB	
D101	VHD1N60///-1	Signal Meter, FM (1N60)	AC	L305	VP-LH1R0M0000	1μH, Choke	AB	
D103	VHD1S2076//-1	FM Muting (1S2076)	AB	L501,	RCILZ0050AFZZ	.8µH, Oscillation Prevention	AC	
D104	VHD1S2076//-1	FM Muting (1S2076)	AB	L502		• ,		
D105	VHD1S2076//-1	FM Muting (1S2076)	AB	L603	VP-LH100M0000	10μH, Choke	AB	-
D106	VHD1S2076//-1	V.C.O. Stop (1S2076)	AB	L801	RCILA0231AFZZ	Balun (Antenna Matching)	AC	

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
L802- A, B	RCILA0403AFZZ	LW/MW Bar Antenna	AS	C217, C218	VCEALU1AC336Y	33μF, 10V, +50 –10%, LR (Orange)	AC
TRANSFORMERS			C223, C224	VCEALU1HC105A	$1\mu$ F, 50V, +75 –10%, LR (Orange)	AC	
T101	RCILD0053AFZZ	Quadrature (10.7MHz)	AE	C229, C230	VCEAAU1CW107Y	$100\mu\text{F}, 16\text{V}, +50 -10\%$	AC
T101	RCILD0055AFZZ	Quadrature (10.7MHz)  Quadrature (10.7MHz)	AE	C309	VCEAAU1CW476Y	$47\mu\text{F}$ , $16\text{V} + 50 - 10\%$	AB
T801,	RTRNP0478AFZZ	Power with Connecting		C310	VCEAAU1AW227Y	$220\mu\text{F}, 10\text{V}, +50 -10\%$	AC
CNS801	KIKNPU4/8AFZZ	Socket		C315	VCEALU1HW224M	.22μF, 50V, ±20%, LL (Yellow)	AB
	FIL	TERS.		C318	VCEAAU1CW476Y	$47\mu\text{F}$ , 16V, +50 –10%	AB
				C319	VCEAAU1EW475A	$4.7\mu\text{F}, 25\text{V}, +75 - 10\%$	AB AC
CF101, CF102	RFILF0001AGZZ	FM IF, Ceramic	AF	C321 C329	VCEAAU1CW107Y VCEAAU1HW105A	$100\mu\text{F}, 16\text{V}, +50 -10\%$ $1\mu\text{F}, 50\text{V}, +75 -10\%$	AB
LPF101, LPF102	RFILL0050AFZZ	Low Pass Filter	AK	C401, C402	VCEALU1EC335A	3.3μF, 25V, +75 –10%, LR (Orange)	AC
LPF1U2	J			C405,)	77 CT 1 1714 CT 100 CT		AC
	CON	TROLS		C406	VCEAAU1CW336Y	$33\mu\text{F}, 16\text{V}, +50 -10\%$	AC .
TC301,	RTO-H2033AGZZ	Trimmer Capacitors	AD	C415, C416	VCEALU1EC335A	$3.3\mu$ F, 25V, +75 $-10\%$ , LR (Orange)	AC
TC302	RTO-HZ033AGZZ	TC301: MW Antenna Trimmer		C417, C418	VCEAAU1CW107Y	$100\mu\text{F}, 16\text{V}, +50 -10\%$	AC
		TC302: LW Antenna Trimmer		C501, C502	VCEALU1EC335A	3.3μF, 25V, +75 –10%, LR (Orange)	AC
TC303, TC304	RTO-H2051AFZZ	Trimmer Capacitors TC303: MW Oscillator	AE	C505, C506	VCEAAU1HW476Y	$47\mu\text{F}$ , 50V, +50 $-10\%$	AC
		Trimmer TC304: LW Oscillator		C507, C508	VCEAAU1CW336Y	$33\mu\text{F}$ , 16V, +50 $-10\%$	AC
VR101	RVR-M0140AFZZ	Trimmer 470(B) ohm, FM Muting	AD	C511, C512	VCEAAU1HW476Y	47μF, 50V, +50 –10%	AC
VR102	RVR-M0078AGZZ	Level Adjust 10K(B) ohm, V.C.O.	AF	C515 C520,	VCEAAU1HW105A RC-EZ1009AFZZ	$1\mu$ F, 50V, +75 –10% 8200 $\mu$ F x 2 (Dual Capacitor),	AB
T/D 102	DVD 1401464E77	Frequency Adjust 220K(B) ohm, Stereo	AD	C521 S	VCEAAU1CW106Y	50V, +50 -10% 10μF, 16V, +50 -10%	AB
VR103	RVR-M0145AFZZ	Separation Adjust	AD	C601	VCEAAU1CW106Y	$10\mu\text{F}, 16\text{V}, +50 - 10\%$	AB
VR201-	)	-	436	C603	VCEAAU1CW337Y	330µF, 16V, +50 –10%	AD
A, B	RVR-B0148AFZZ	100K ohm, Volume Control	AM	C604	VCEAAU1CW337Y	$330\mu\text{F}, 16\text{V}, +50 -10\%$	AD
VR202	RVR-Z0061AFZZ	100K ohm, Balance Control		C605	VCEAAU1CW107Y	$100\mu\text{F}, 16\text{V}, +50 -10\%$	AC
VR203-	RVR-C0066AFZZ	100K ohm, Bass Control	AL	C614	VCEAAU1VW227Y	$220\mu\text{F}, 35\text{V}, +50 -10\%$ $100\mu\text{F}, 35\text{V}, +50 -10\%$	AD AD
A, B	,	•		C615 C616	VCEAAU1VW107Y VCEAAU1VW227Y	$100\mu\text{F}$ , 35 V, +50 $-10\%$	AD
VR204- A, B	RVR-C0066AFZZ	100K ohm, Treble Control	AL	C617	VCEAAU1VW107Y	$100\mu\text{F}, 35\text{V}, +50 -10\%$	AD
VR501,	]	330(B) ohm, Idle Current	AD	C618	VCEAAU1EW227Y	$220\mu\text{F}, 25\text{V}, +50 -10\%$	AC
VR502		Adjust		C619	VCEAAU1CW227Y	$220\mu\text{F}$ , 16V, +50 $-10\%$	AC
	ELECTROLYT	TIC CAPACITORS		C622 C636,	VCEAAU1EW476Y VCEALU1HW105M	$47\mu\text{F}, 25\text{V}, +50 - 10\%$ $1\mu\text{F}, 50\text{V}, \pm 20\%, \text{LL (Yellow)}$	AC AD
				C637		• • •	
C115	VCEAAU1HW105A	$1\mu$ F, 50V, +75 $-10\%$	AB	C805	VCEAAU1EW106Y	$10\mu\text{F}, 25\text{V}, +50 -10\%$ $10\mu\text{F}, 25\text{V}, +50 -10\%$	AB AB
C116	VCEAAU1HW105A	$1\mu$ F, 50V, +75 $-10\%$ 3.3 $\mu$ F, 10V, $\pm$ 20%, Aluminum	AB AD	C806	VCEAAU1EW106Y	$10\mu$ F, 23 V, +30 $-10\%$	AD
C119 C121	VCAAAU1AB335M VCEAAU1CW107Y	$100\mu\text{F}$ , $16\text{V}$ , $\pm 20\%$ , Administration $100\mu\text{F}$ , $16\text{V}$ , $\pm 50 - 10\%$	AC		CAPA	ACITORS	
Ć121	VCAAAU1EB224K	$.22\mu\text{F}, 25\text{V}, \pm 10\%, \text{Aluminum}$	1			e specified capacitors are	
C124	VCAAAU1AB335M	$3.3\mu\text{F}$ , $10\text{V}$ , $\pm 20\%$ , Aluminum			50V, +80 -20%		
C125	VCAAAU1EB155K	1.5µF, 25V, ±10%, Aluminum	AC				
C127	VCEAAU1CW106Y	$10\mu$ F, 16V, +50 $-10\%$	AB	C101	VCKZPU1HF102Z	.001µF	AA
C128	VCEAAU1CW106Y	$10\mu$ F, 16V, +50 $-10\%$	AB	C102	VCKZPU1HF223Z	.022μF	AA AA
C131,) C132	VCEAAU1CW106Y	10μF, 16V, +50 –10%	AB	C103 C104	VCKZPU1HF223Z VCKZPU1HF223Z	.022μF .022μF	AA AA
C133	VCEAAU1AW227Y	220μF, 10V, +50 –10%	AC AB	C107 C108	VCKZPU1HF223Z VCKZPU1HF223Z	.022μF .022μF	AA
C141	VCEAAU1HW105A	$1\mu\text{F}$ , 50V, +75 $-10\%$ 3.3 $\mu\text{F}$ , 25V, +75 $-10\%$ ,		C108	VCKZPU1HF223Z	.022μF .022μF	AA
C205, C206	VCEALU1EC335A	LR (Orange)	AC	C110	VCKZPU1HF223Z	.022μF	AA
C207, C208	VCAAAU1AB224M	.22μF, 10V, ±20%, Aluminum	AC	C111 C112	VCKZPU1ND474M VCKZPU1HF223Z	.47 $\mu$ F, 12V, ±20%, Ceramic .022 $\mu$ F	AD AA
•			1	1			1 1

)	REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE	
	C114	VCKZPU1HF223Z	.022μF	AA	C516,)				
	C117	VCKZPU1HF223Z	.022µF	AA	C517,		$.01\mu$ F, 150VAC, +80 $-20\%$ ,		
	C118	VCKZPU1HF223Z	.022μF	AA	C518,	VCKZPU2TE103Z	Ceramic	AB	
	C120	VCCSPU1HL331K	330pF, 50V, ±10%, Ceramic	AB	C519		Columne		
	C122	VCQYKU1HM473K	$.047\mu\text{F}, 50\text{V}, \pm 10\%, \text{Mylar}$	AC	C606	VCKZPU1HF223Z	$.022\mu\mathrm{F}$	AA	
	C126	VCQSMT1HS391J	390pF, 50V, ±5%, Styrol	AB	C801,)	V CREDI OTTII 2232	.022 <b>µ</b> 1	АА	
	C129	VCQYKU1HM122J	$.0012 \mu F$ , 50V, $\pm 5\%$ , Mylar	AB	C802	VCKZPU1HF223Z	$.022 \mu \mathrm{F}$	AA	
	C130	VCQYKU1HM122J	• • • • • • •	AB	C803,		05UE 250MAC +200		İ
	C130	VCKZPU1HF223Z	$.0012\mu$ F, 50V, $\pm$ 5%, Mylar			RC-PZ061CAFZZ	.05μF, 250VAC, ±20%,	AF	
			.022µF	AA	C804 S		Oil		
	C142	VCCSPU1HL220K	22pF, 50V, ±10%, Ceramic	AA		DEO	IOTODO		
	C143	VCCSPU1HL331K	330pF, 50V, ±10%, Ceramic	AB			ISTORS		
	C201, C202	VCCSPU1HL271K	270pF, 50V, ±10%, Ceramic	AB		Unless otherwise speci Carbon Type.	fied resistors are 1/4W, ±5%,		
	C203,	VCQYKU1HM683J	$.068\mu\text{F}, 50\text{V}, \pm 5\%, \text{Mylar}$	AC			1.		
	C204	•			R101	VRD-ST2EE470J	47 ohm	AA	
	C209,	VCCSPU1HL120K	12pF, 50V, ±10%, Ceramic	AA	R102	VRD-ST2EE473J	47K ohm	AA	
	C210		12,7,000, 10,00, 001411110	1111	R103	VRD-ST2EE103J	10K ohm	AA	
	C211,	VCCSPU1HL5R0C	5pF, 50V, ±0.25pF, Ceramic	AA	R104	VRD-ST2EE471J	470 ohm	AA	İ
)	C212	V COSI O I I I I SI NO C	3p1, 30 1, =0.23p1, Colamic	71.71	R105	VRD-ST2EE331J	330 ohm	AA	
	C213,	VCCSPU1HL560K	56pF, 50V, ±10%, Ceramic	AA	R106	VRD-ST2EE470J	47 ohm	AA	
	C214	VCCSi UTILISUUK	30pr, 30 v, ±10%, Ceramic	AA	R107	VRD-ST2EE101J	100 ohm	AA	
	C215,	VCCCDIIIII 471V	470-E 50M +100 Commis	4.5	R116	VRD-ST2EE181J	180 ohm	AA	
	C216	VCCSPU1HL471K	470pF, 50V, ±10%, Ceramic	AB	R117	VRD-ST2EE331J	330 ohm	AA	
	C219,		****		R118	VRD-ST2EE104J	100K ohm	AA	
	C220	VCQYKU1HM223J	.022μF, 50V, ±5%, Mylar	AB	R119	VRD-ST2EE562J	5.6K ohm	AA	
	C221,	}			R120	VRD-ST2EE152J	1.5K ohm	AA	
	C222	VCQYKU1HM124J	.12μF, 50V, ±5%, Mylar	AE	R120	VRD-ST2EE822J	8.2K ohm	AA	
	C225,				R121	VRD-ST2EE8223 VRD-ST2EE121J	120 ohm	AA	
	C226	VCQYKU1HM222J	$.0022\mu$ F, 50V, $\pm$ 5%, Mylar	AB	R123	VRD-ST2EE1213 VRD-ST2EE154J	150K ohm	AA	
\	C227,				R123	VRD-ST2EE333J	33K ohm		
)	C228	VCQYKU1HM103J	.01μF, 50V, ±5%, Mylar	AB				AA	
	C301	VCQSMT1HS331J	220mE 5037 +507 Street	A.D.	R125	VRD-ST2EE333J	33K ohm	AA	
		-	330pF, 50V, ±5%, Styrol	AB	R126	VRD-ST2EE123J	12K ohm	AA	
	C302	VCCUPU1HJ150K	15pF(UJ), 50V, ±10%,	AB	R127	VRD-ST2EE123J	12K ohm	AA	
	G0.0		Ceramic		R128	VRD-ST2EE223J	22K ohm	AA	
	C303	VCQSMT1HS121J	120pF, 50V, ±5%, Styrol	AB	R129	VRD-ST2EE123J	12K ohm	AA	
	C304	VCCCPU1HH470J	47pF(CH), 50V, ±5%, Ceramic	AB	R130	VRD-ST2EE333J	33K ohm	AA	
	C306	VCKZPU1HF103P	$.01\mu$ F, 50V, +100 $-0\%$ ,	AE	R131	VRD-ST2EE333J	33K ohm	AA	
			Ceramic		R132	VRD-ST2EE563J	56K ohm	AA	
	C307	VCKZPU1HF103P	$.01\mu$ F, 50V, +100 $-0\%$ ,	AE	R133	VRD-ST2EE104J	100K ohm	AA	
			Čeramic		R134	VRD-ST2EE225J	2.2 Meg ohm	AA	
1	C308	VCCSPU1HL221K	220pF, 50V, ±10%, Ceramic	AB	R135	VRD-ST2EE223J	22K ohm	AA	
	C311	VCCSPU1HL470K	47pF, 50V, ±10%, Ceramic	AA	R136	VRD-ST2EE102J	1K ohm	AA	
	C312	VCQYKU1HM473K	$.047\mu$ F, 50V, $\pm 10\%$ , Mylar	AC	R137	VRD-ST2EE223J	22K ohm	AA	ļ
	C313	VCKZPU1HF473Z	$.047 \mu \mathrm{F}$	AB	R138	VRD-ST2EE223J	22K ohm	AA	
	C314	VCKZPU1HF473Z	$.047 \mu \mathrm{F}$	AB	R139	VRD-ST2HD561J	560 ohm, 1/2W, ±5%, Carbon	AA	
	C316	VCQYKU1HM223K	$.022\mu\text{F}, 50\text{V}, \pm 10\%, \text{Mylar}$	AB	R140	VRD-ST2EE333J	33K ohm	AA	
	C317	VCQYKU1HM103K	$.01\mu\text{F}$ , 50V, $\pm 10\%$ , Mylar	AB	R141,)			7.22	İ
	C320	VCKZPU1HF473Z	.047µF	AB	R142	VRD-ST2EE682J	6.8K ohm	AA	
	C403, C404	VCCSPU1HL101K	100pF, 50V, ±10%, Ceramic	AA	R143, R144	VRD-ST2EE473J	47K ohm	AA	
	C407, C408	VCCSPU1HL560K	56pF, 50V, ±10%, Ceramic	AA	R145, R146	VRD-ST2EE272J	2.7K ohm	AA	
	C409, C410	VCCSPU1HL5R0C	5pF, 50V, ±0.25pF, Ceramic	AA	R147, R148	VRD-ST2EE392J	3.9K ohm	AA	
	C411, C412	VCQSMU1HS392J	3900pF, 50V, ±5%, Styrol	AC	R149, R150	VRD-ST2EE222J	2.2K ohm	AA	
	C413,	VCQSMU1HS152J	1500pF, 50V, ±5%, Styrol	AB	R151	VRD-ST2EE333J	33K ohm	AA	
	C414 J				R152	VRD-ST2EY101J	100 ohm	AA	
	C503,	VCCSPU1HL391J	390pF, 50V, ±5%, Ceramic	AB	R153	VRD-ST2EE474J	470K ohm	AA	
~\	C504		* , , , ,,		R154	VRD-ST2EE223J	22K ohm	AA	
	C509,	VCCSPU1HL330K	33pF, 50V, ±10%, Ceramic	AA	R156	VRD-ST2EY101J	100 ohm	AA	
	C510		* / ///		R157	VRD-ST2EE184J	180K ohm	AA	
	C513,	VCQYKU1HM104K	$.1 \mu$ F, 50V, $\pm 10\%$ , Mylar	AC	R158	VRD-ST2EE563J	56K ohm	AA	
	C514		, ., ,		R159	VRD-ST2EE473J	47K ohm	AA	
		•		1	R160	VRD-ST2EE223J	22K ohm	AA	1

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE	
R201, R202	VRD-ST2EE333J	33K ohm	AA	R501, R502	VRD-ST2EE564J	560K ohm		
R203, R204	VRD-ST2EE103J	10K ohm	AA	R503 R504	VRD-ST2EE821J VRD-ST2EY821J	820 ohm 820 ohm		
R205, R206	VRD-ST2EE474J	470K ohm	AA	R505, R506	VRD-ST2EE273J	27K ohm		
R207, R208	VRD-ST2EE563J	56K ohm	AA	R507, R508	VRD-ST2EE562J	5.6K ohm	AA	
R209, R210	VRD-ST2EE104J	100K ohm	AA	R509, R510 J. R511,	VRD-ST2EE682J	6.8K ohm		
R211, R212	VRD-ST2EE471J	470 ohm	AA	R511, R512 R513,	VRD-ST2EY681J	680 ohm		
R213, R214	VRD-ST2EE102J	1K ohm	AA	R514 R515,	VRD-ST2EE152J	1.5K ohm		
R215, R216	VRD-ST2EE183J	18K ohm	AA	R516 R517,	VRD-ST2EE682J	6.8K ohm		
R217,) R218	VRD-ST2EE332J	3.3K ohm	AA	R518 R519,	VRD-ST2EE223J	22K ohm	AB	(
R219, R220   R221,	VRD-ST2EE332J	3.3K ohm	AA	R520 R521,	VRG-ST2EA680J	68 ohm, 1/4W, ±5%, Fusible 27K ohm	AA	
R222- R222- R223,	VRD-ST2EE562J	5.6K ohm	AA	R522 R523,	VRD-ST2EE273J	100 ohm, 1/4W, ±5%, Fusible		
R224 R225,	VRD-ST2EE122J	1.2K ohm	AA	R524 R525,	VRG-ST2EA101J VRG-ST2EA101J	100 ohm, 1/4W, ±5%, Fusible		
R226 R227,	VRD-ST2HD331J	330 ohm, 1/2W, ±5%, Carbon 220K ohm	AA	R526   R527,	VRG-ST2EA101J	100 ohm, 1/4W, ±5%, Fusible	AB	
R228 R229,	VRD-ST2EE224J	1.8K ohm	AA	R528   R529,	VRG-ST2EA4R7J	4.7 ohm, 1/4W, ±5%, Fusible		,
R230 <sup>)</sup> R301	VRD-ST2EE182J VRD-ST2EE681J	680 ohm	AA	R530   R531,	VRG-ST2EA4R7J	4.7 ohm, 1/4W, ±5%, Fusible	AB	(
R302 R303	VRD-ST2EE102J VRD-ST2EE332J	1K ohm 3.3K ohm	AA AA	R532   R533,	VRW-KT3HDR33K	.33 ohm, 5W, ±10%,	AĎ	
R304 R305	VRD-ST2EE222J VRD-ST2EE153J	2.2K ohm 15K ohm	AA AA	R534   R535,	VRW-KT3HDR33K	Wire Wound .33 ohm, 5W, ±10%, Wire Wound	AD	
R306 R307	VRD-ST2EE103J VRD-ST2EE562J	10K ohm 5.6K ohm	AA AA	R536   R537,	VRD-ST2EE392J	3.9K ohm	)	
R308 R309	VRD-ST2EE393J VRD-ST2EY101J	39K ohm 100 ohm	AA AA	R538   R539,   R540	VRD-ST2EE392J	3.9K ohm		
R310 R321	VRD-ST2EY470J VRD-ST2EE122J	47 ohm 1.2K ohm	AA AA AA	R541, R542	VRD-ST2EE392J	3.9K ohm		(
R322 R324	VRD-ST2EE473J VRD-ST2EE822J	47K ohm 8.2K ohm 10K ohm	AA AA	R543,) R544		3.9K ohm	AA	
R325 R326 R401,	VRD-ST2EE103J VRD-ST2EE103J	10K ohm	AA	R545, R546	VRD-ST2EE223J	22K ohm		
R402 R403,	VRD-ST2EE102J	1K ohm	AA	R547, R548		6.8K ohm		
R404 R405,	VRD-ST2EE473J	47K ohm	AA	R549, R550		10K ohm	] .	
R406 R407,	VRD-ST2EE224J	220K ohm 680K ohm	AA	R551, R552	V KW-KI3DD2K2K	2.2 ohm, 2W, ±10%, Wire Wound	AC	
R408 R409,	VRD-ST2EE684J	1.2K ohm	AA	R553, R554	VKW-KI3DD100K	10 ohm, 2W, ±10%, Wire Wound	AC AA	
R410 } R411,	VRD-ST2EE122J VRD-ST2EE104J	100K ohm	AA	R556,		3.3K ohm 1 ohm, 1/2W, ±5%,		
R412 ( R413,)		56K ohm	AA	R557, R558,	VKG-512HAIRO3	Fusible	AC	
R414 ( R415,	VKD-S12LL3033	3.3K ohm	AA	R561,	VRD-ST2EE821I	820 ohm	)	
R416 R417,	VRD-ST2EE3323	220K ohm	AA	R601	VRD-ST2EE153J VRD-ST2EE333J	15K ohm 33K ohm		"
R418 R419,	) VDD-ST2HD3311	330 ohm, 1/2W, ±5%, Carbor		R602	VRD-ST2EE393J	39K ohm 3.9K ohm		
R420	1 112 512112531	, , , , , , , , , , , , , , , , , , ,	1	1004	γ KD-0 1 2 EE 5 7 2 3	5171x OIIII		

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
R605	VRD-ST2EE682J	6.8K ohm	1		HSSND0230AFSA	Dial Pointer	AF
R606	VRD-ST2EE682J	6.8K ohm			JKNBB0059AFSA	Knob, Tuning Control	AP
R607	VRD-ST2EE470J	47 ohm	AA		JKNBM0248AFSA	Knob, LW/MW/FM/FM	AF
R608	VRD-ST2EE562J	5.6K ohm				Muting	Air
R609	VRD-ST2EE683J	68K ohm			JKNBN0334AFSA	Knob, Bass, Treble, Balance	AG
R610	VRD-ST2EY121J	120 ohm			JKNBN0333AFSA	Knob, Speakers Selector,	AH
R612	VRD-ST2EY221J	220 ohm				Volume Control, Function	All
R613	VRD-ST2EE223J	22K ohm				Selector	
R614	VRD-ST2EE223J	22K ohm			JKNBP0070AFSA	Knob, Power Switch, Audio	AH
R615	VRD-ST2EY221J	220 ohm				Muting Switch, Low Cut	AII
R616	VRS-PT3DB681K	680 ohm, 2W, ±10%,	AB			Filter Switch, Mode	
		Oxide Film				Selector, Loudness Switch,	
R618,						Tape Dubbing Switch, Tape	
R619,	VRS-PT3DB271K	270 ohm, 2W, ±10%,				Monitor Switch	
R620,	VK3-F13DB2/1K	Oxide Film	AB		LANGQ0423AFZZ	Bracket, LW/MW Bar Antenna	AB
R621					LANGQ0508AFSA	Rear Panel	AT
R622	VRG-ST2EA151J	150 ohm, 1/4W, ±5%, Fusible	AB		LANGQ0504AFZZ	Bracket, Dial Lamp P.W. Board	
R623	VRS-PT3AB561K	560 ohm, 1W, ±10%,	AB		-	(Part of PREFL0061AFZZ)	
		Oxide Film	İ		LANGR0414AFZZ	Bracket, Front Panel	AP
R624	VRG-ST2EA151J	150 ohm, 1/4W, ±5%, Fusible	AB		LANGR0413AFZZ	Bracket, Power Transformer	AH
R625	VRS-PT3AB561K	560 ohm, 1W, ±10%,	AB		LANGT0607AFZZ	Bracket, Dial	AF
		Oxide Film			LANGT0608AFZZ	Bracket, Pulley	AB
R626	VRD-ST2HD182J	1.8K ohm, 1/2W, ±5%, Carbon	AA		LANGT0622AFZZ	Bracket, Heat Sink	
R627	VRD-ST2EE681J	680 ohm	AA		LBSHC0002AGZZ	Bushing, LW/MW Bar Antenna	AB
R639	VRG-ST2EA4R7J	4.7 ohm, 1/4W, ±5%, Fusible	AB			Wire	
R640,	VRD-ST2EE221J	220 ohm	AA		LBSHC0004AGZZ	Bushing, Power Supply Cord	AC
R641	,		7171			(SEMKO, KEMA)	
R642,	VRD-ST2EE272J	2.7K ohm	AA		LBSHC0007AFZZ	Bushing, Power Supply Cord	AB
R643 ∫			7171			(SEV, A-club)	
R644,	VRD-ST2EE682J	6.8K ohm	AA		LCHSM0257AFZZ	Chassis Assembly	AW
R645			71.1		LHLDP3055AFZZ	Holder, Dial Lamp	_
R646,	VRD-ST2EE183J	18K ohm	AA			(Part of PREFL0061AFZZ)	
R647 ∫		_	1111		LHLDW1050AFZZ	Wire Clip	AA
R648,	VRD-ST2EE222J	2.2K ohm	AA		LHLDW1052AFZZ	Wire Clip	AA
R649   R650	VDD CTARVICIT	150 1			LHLDW1053AFZZ	Wire Clip Refer to Figure 45	AB
	VRD-ST2EY151J	150 ohm	AA		LHLDW1060AFZZ	wife Cip	AA
R701,					LHLDW1062AFZZ	Wire Clip	AA
R702,	VRD-ST2EY102J	1K ohm	AA		LHLDW1066AFZZ	Wire Clip	AA
R703, R704					LHLDW9050AFZZ	Wire Holder, AM Antenna	AD
R705,					I DI TIDOGEA I TITT	Wire	
R706	VRD-ST2EY104J	100K ohm	AA		LPLTP0053AFZZ	Acryl, Dial Illumination	
R700)					T 77 T17700 FA	(Part of PREFL0061AFZZ)	
R707,	VRD-ST2EY394J	390K ohm	AA		LX-HZ0053AFFD	Flange Head Screw, P.W.	AA
R709,)					TWANTAGAGGER	Board	
R710,					LX-NZ0006SGFD	Flange Nut, Antenna	AA
R710,	VRD-ST2EY102J	1K ohm	AA		I W M70110 + FFD	Terminals	
R711,					LX-NZ0118AFFD	Nut, Speaker Selector Switch	AA
R712)						Shaft, Function Selector	
R714	VRD-ST2EY104J	100K ohm	AA			Switch Shaft and Headphone	
R715,)					IV MZ0110 APPW	Jacks	
R716	VRD-ST2EY394J	390K ohm	AA		LX-NZ0119AFFW	Hexagon Head Cap Screw,	AD
R801	VRD-SU2EY822J	8.2K ohin				Speaker Selector Switch and	
1001	V RD 502L 10223	8.2K Ollili	AA		I V N70120 A EED	Function Selector Switch	
	MISCEL	LANEOUS			LX-NZ0120AFFD	Flange Nut $(5\phi)$ , Power	AA
		LANEOUS			MCDD D0152 AE77	Transformer	
	CSPRT0304AF16	Dial Cord Assembly			MSPRP0152AFZZ	Plate Spring, Grounding	AA
	GCAB-5090AFSA	Cabinet	BF		MSDRT0304 A EET	(Earth)	
	GCOVA1070AFSC	Guide (Large), Lever Switch	1		MSPRT0304AFFJ	Spring, Dial Cord	AA
	GCOVA1070AFSC	Guide (Large), Lever Switch  Guide (Small), Lever Switch	AD		NDRM-0150AFZZ	Drum	AF
	GFTAU3065AFZZ	Plate, Bottom	AD		NPLYB0001SGZZ NPLYC0101AFFD	Pulley, Dial Cord	AB
	3. 1.1.0000JA1 <u>DL</u>	(Part of LCHSM0257AFZZ)				Shaft, Pulley	AA
	GLEGP0002SG00	Leg	40		NSFTD0171AFFW	Tuning Shaft with Flywheel	AN
	HDALM0173AFSA	Dial	AC		PCUSCO077A FOO	Cover, Fuse, Rear Panel	AF
	HPNLC3276AFSA	Front Panel	AY		PCUSG0077AF00	Cushion, AM P.W. Board	D.4
	THE INDESTRUCTION	1 10111 1 41101	BG		PRDAR0142AF00	Heat Sink, Power Transistor	BA

AF AP AF AG AH

AΗ

AB AT

AP AH AF AB AB

AB AW

AA AB AA AA AA AA

AA AA

ΔD

AA AA AF AB AA

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
	PRDAR0101AFFW PREFL0061AFZZ	Heat Sink, Transistor Q609 Dial Illumination Assembly	AB BA		QPWBF0597AFZZ	Printed Wiring Board, AM RF/IF Circuit	AU
	PSHEF0110AFZZ PSHEF0114AF00	Felt (Long), Lever Switch Felt (Short), Power Switch	AA —		QSOCT0353AFZZ	Socket, Power Transistor TAPE-1 Socket,	AD
	PSLDM3126AFZZ	Shield Plate	AA	SO701-1		REC (SO701-A, B),	
	PSPAS0053AFSA	Spacer, Push Knob	AB	$\left  \begin{array}{c} 30701 \\ A \sim E \end{array} \right $	QSOCZ2450AFZZ	PB (P) (SO701-C, D),	AK
	PSPAS0054AFZZ	Spacer, Headphone Jack	AC	11 10 ,		DIN(SO701-E)	
	PSPAZ0050AFZZ	Insulator, Mica, Power	AB			TAPE-2 Socket,	
		Transistor	122	SO702-1		REC (SO702-A, B),	
	PSPAZ0060AFZZ	Spacer, LED (D801)	AA	$A \sim E$	QSOCZ2450AFZZ	PB(P) (SO702-C, D),	AK
	PZETF0128AFZZ	Insulator, Fuse P.W. Board		, ,		DIN (SO702-E)	
	QACCN0001AGZZ	Power Supply Cord with	AP			Socket, Auxiliary Input	
		Plug (SEMKO)		SO801-1	000	(SO801-A, B), PHONO-1	
	QACCS9001SE00	Power Supply Cord (SEV)	AF	$A \sim F$	QSOCJ2660AFZZ	Input (SO801-C, D),	AG
	QPLGA0205AGZZ	Plug, Power Supply Cord	AH	,		PHONO-2 Input	
		(SEV)				(SO801-E, F)	
	QACCV0001AGZZ	Power Supply Cord with Plug (KEMA)	AN	SW201- A, B	QSW-R0141AFZZ	Switch, Function Selector	AR
	QACCZ0002TA0F	Power Supply Cord with Plug (USA type Plug)	AF	SW202 SW203-)	QSW-B0073AFZZ	Switch, Tape Monitor	AH
	QACCZ0002AG08	Power Supply Cord	AF	$A \sim D$	QSW-B0054AFZZ	Switch, Tape Dubbing	AK
	QPLGA0201AGZZ	Plug, Power Supply Cord	AE	SW204	QSW-B0051AFZZ	Switch, Mode Selector	AH
	QANTW0055AFZZ	FM Indoor Antenna, T-Shape	AH	SW205	QSW-B0051AFZZ	Switch, Loudness	AH
CN201	QCNCM135LAFZZ	Connecting Plug, 11-Pin	AE		(5 ·· 20001111 22	Switch, Band (LW/MW/FM)	
CN202	QCNCM132FAFZZ	Connecting Plug, 6-Pin	AD	SW301-}	QSW-P0143AFZZ	Selector (SW301-A~C),	AS
CN203	QCNCM132FAFZZ	Connecting Plug, 6-Pin	AD	$A \sim D$	<b>Q</b> 2 2 <b>V</b> 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	FM Muting (SW301-D)	
CN301	QCNCM133GAFZZ	Connecting Plug, 7-Pin	AD	SW601	QSW-R0140AFZZ	Switch, Speakers Selector	AN
CN302	QCNCM134HAFZZ	Connecting Plug, 8-Pin	AD	SW602	QSW-B0051AFZZ	Switch, Low Cut Filter	AH
CNP801	QCNCW108CAFZZ	Connecting Plug, 2-Pin		SW603	QSW-B0051AFZZ	Switch, Audio Muting	AH
		(Part of PREFL0061AFZZ)		SW801	QSW-B9059AFZZ	Switch, Power	AQ
CNS201	QCNCW106LAFZZ	Connecting Socket, 11-Pin	AC	TB801	QTANN0453AFZZ	Antenna Terminals, FM	AH
CNS202	QCNCW103FAFZZ	Connecting Socket, 6-Pin	AB			(75 ohms and 240 ohms)	
	QCNCW103FAFZZ	Connecting Socket, 6-Pin	AB			and AM	
CNS301	QCNCW104GAFZZ	Connecting Socket, 7-Pin	AB	TB802	QTANN0150AFZZ	Terminal, Grounding (Earth)	AD
CNS302	QCNCW105HAFZZ	Connecting Socket, 8-Pin	AB	TB803	QTANN0454AFZZ	Speaker Terminals-A	AG
	QFS-C202CAGNI	Fuse, 2.0AT (250V)	AE	TB804	QTANN0454AFZZ	Speaker Terminals-B	AG
7.0.4	QFSHD1001AGZZ	Holder, Fuse	AA	ME801	RMTRL0135AFSA	Meter, Signal (Strength)	AU
J601	QJAKJ0057AFZZ	Jack, Headphone-b	AG	ME802	RMTRL0134AFSA	Meter, Tuning (Center)	AU
J602	QJAKJ0057AFZZ	Jack, Headphone-a	AG	RLY601	RRLYZ0050AFZZ	Relay, DC24V, Protection	AW
	QLUGL0250AFZZ	Terminal Strip, 2-Lug	AC	-A, B	) DTINE0061AE77	Circuit	BC
	QLUGZ011AAFZZ	Lug, Ground (Earth)	AA		RTUNF0061AFZZ	FM Tuner (Front-end)	BC
	QPLGS0102AGZZ QPWBF0603AFZZ	Plug, Short Printed Wiring Board, Main	AD AQ	PL801,		Assembly	
	QPWBF0353AFZZ	Amplifier Circuit Printed Wiring Board, Tape	AD	PL802, PL803,	DI MDDOOG A DZZ	Dial Illumination Lamp	
	QPWBF0423AFZZ	Circuit Printed Wiring Board, Fuse	AE	PL804, PL805,	RLMPP0057AFZZ	(8V, 0.3A) (Part of PREFL0061AFZZ)	
		Circuit	AL.	PL806	VDDCD40B45000		
	QPWBF0593AFZZ	Printed Wiring Board, Dial Lamp Circuit (Part of PREFL0061AFZZ)			XBBSD40P45000 XHBSF40P18XSO XHBSD40P12000	Screw, Bar Antenna Bracket Screw, Cabinet Screw, Leg	AA
	QPWBF0596AFZZ	Printed Wiring Board, FM RF/IF, Equalizer and Tone Circuits	AS		XNESD40-32000 XWHSD91-10140	Nut, Bar Antenna Bracket Washer, Function Selector Switch	AA
	QPWBF0595AFZZ	Printed Wiring Board, Power Supply and Relay Circuits	AM		XWUSE84-08000	Shakeproof Lockwasher Internal Type, Grounding (Earth) Terminal	AA