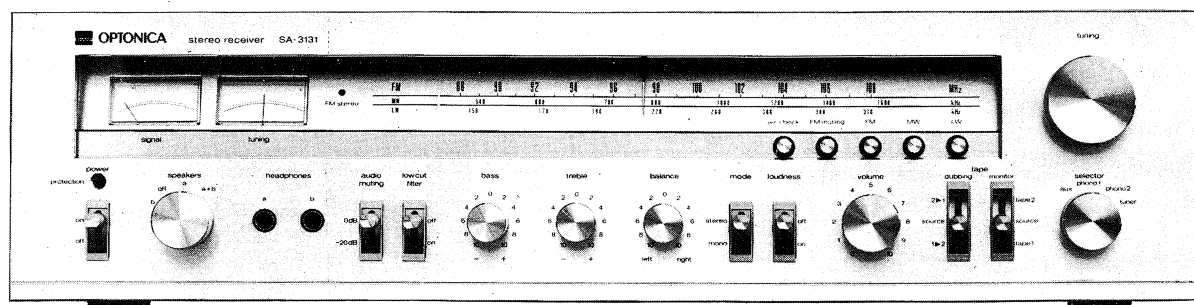




# OPTONICA

# SERVICE MANUAL

SA-3131H



Stereo Receiver

## MODEL SA-3131H

In the interests of user-safety the set should be restored to its original condition and only parts identical to those specified be used.

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# SHARP CORPORATION OSAKA, JAPAN

## SPECIFICATIONS

### ● GENERAL DESCRIPTION

Power source:	AC 110/220/240V, 50/60Hz
Circuit	
Tuner:	Superheterodyne system, LW/MW/FM 3-bands tuner, with P.L.L. stereo demodulation circuit, FM muting circuit, air check calibration circuit.
Main amplifier:	Differential amplifier and all stage direct coupled pure complimentary O.C.L. (Output Capacitor-Less) circuitry.
Tone amplifier:	"NF" type tone control circuit.
Equalizer:	Two-stage direct coupled equalizer circuit
Semiconductors:	6-IC (Integrated circuit) 42-transistor (7-FET) 40-diode (4-Zener diode) 2-LED
Dimensions:	Width . . . . . 550 mm Height . . . . . 142 mm Depth . . . . . 390 mm
Weight:	16 kg

### ● FM SECTION

Tuning range:	87.6 ~ 108 MHz
Intermediate frequency:	10.7 MHz
Sensitivity:	1.4 $\mu$ V (at S/N 26 dB, 40 kHz deviation, antenna terminal voltage)
Distortion (40 kHz deviation)	
Mono:	0.5%
Stereo:	0.8%
Image rejection ratio:	71 dB
I.F. rejection ratio:	76 dB
Spurious frequency rejection ratio:	80 dB
AM suppression ratio:	45 dB (modulated by 30% AM and 75 kHz deviation FM)
Selectivity:	64 dB (IHF)
Capture ratio:	2 dB
Stereo separation:	34 dB (1 kHz)
Antenna input:	75 ohms unbalanced 240 ohms balanced

### ● AM SECTION

Tuning range:	MW 520 ~ 1620 kHz LW 150 ~ 370 kHz
---------------	---------------------------------------

Intermediate frequency:	MW/LW 455 kHz
Quieting Sensitivity:	MW 400 $\mu$ V/m (at 1000 kHz) LW 400 $\mu$ V/m (at 220 kHz)
Image rejection ratio:	MW 34 dB (at 1400 kHz) LW 30 dB (at 340 kHz)
I.F. rejection ratio:	MW 49 dB (at 600 kHz) LW 40 dB (at 340 kHz)
Distortion:	LW/MW 1.6%
Antenna:	Built-in ferrite bar antenna and external antenna terminal

### ● MAIN (POWER) AMPLIFIER

Continuous power output:	2 x 65W/4-ohms, both channels driven at 1 kHz, 0.1% distortion 2 x 40W/8-ohms, both channels driven at 1 kHz, 0.1% distortion
Total harmonic distortion:	0.05% at 40W (AUX IN)
Intermodulation distortion:	0.1% at 40W (AUX IN)
Damping factor:	More than 20 (at 1 kHz, 4-ohms)
Power bandwidth:	10 Hz ~ 20 kHz

### ● PRE-AMPLIFIER

Input sensitivity and input impedance	
PHONO 1:	2.5 mV/50K ohms
PHONO 2:	2.5 mV/50K ohms
AUX:	150 mV/50K ohms
TAPE playback	
1 and 2:	150 mV/50K ohms
Output level and loaded impedance	
REC 1 and 2:	150 mV/50K ohms
REC 1 and 2 (DIN socket):	30 mV/80K ohms
Phono overload:	220 mV (R.M.S. 1 kHz, 0.1% T.H.D.)
"RIAA" curve deviation (Phono):	$\pm 0.5$ dB
Frequency response:	10 Hz ~ 50 kHz $\pm 1.5$ dB (AUX., TAPE playback)
Tone control	
Bass:	$\pm 10$ dB at 100 Hz
Treble:	$\pm 10$ dB at 10 kHz
Low cut filter:	30 Hz, 6 dB/oct
Audio muting:	- 20 dB

## FEATURES

- 1) The power supply circuits for right channel and left channel are independent from each other, and either of them includes two dual-capacitors, each of 6800 $\mu$ F x 2 (thus amounting to 27200 $\mu$ F = 6800 $\mu$ F x 4 in total).
- 2) Being composed of FET's (Field Effect Transistors) as a whole, the equalizer circuit further improves signal-to-noise ratio.
- 3) With a built-in protection circuit, the loudspeaker remains always safe even if the amplifier circuit gets in trouble and reversely the amplifier is protected against a possible short-circuit of the loudspeaker cord.
- 4) Power source/circuit protection indicator making use of 2-color LED element, which will light up in red if there is something abnormal in the internal circuitry. In a normal condition, it is lit green.
- 5) Because of the circuit being ITL (Input Transformerless), OTL (Output Transformerless), OCL (Output Capacitorless) and pure-complementary system, low-distortion characteristic is more assured.
- 6) Dual gate MOS FET and 4-gang variable capacitor adopted at the FM front-end circuit more improve overall characteristics.
- 7) The PLL (Phase Locked Loop) demodulator circuit assures a stabilized characteristic.

## PREPARATION FOR USE

### AC VOLTAGE SELECTION (Refer to Figure 1)

Check the preset voltage selector before inserting the mains plug to an mains outlet. If the voltage is different from your local voltage, change it in the following manner:

1. Disconnect the AC cord plug from the wall outlet in order to prevent an electric shock.
2. Loosen a screw and slide the cover as illustrated in Fig. 1.
3. Put a fuse in the fuse holder which has an indication of your local voltage.

In case the local voltage is 110V, two pieces of fuses should be used.

4. Replace the cover in its original position.

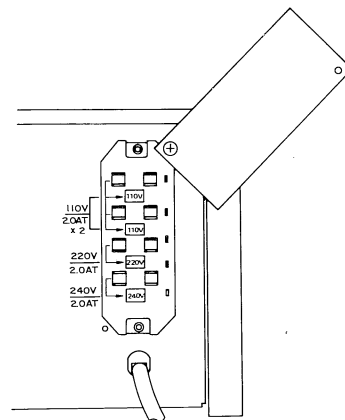


Figure 1

## DISASSEMBLY

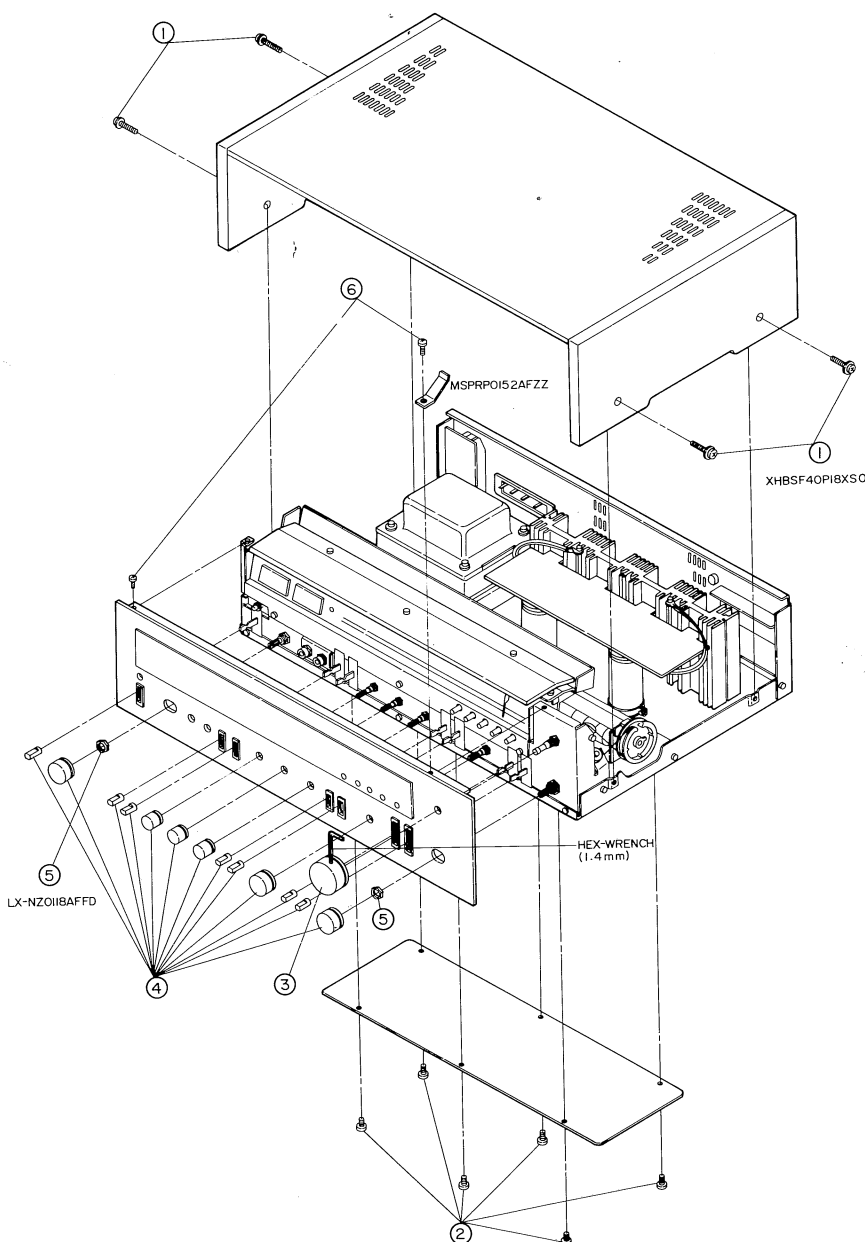


Figure 2 DISASSEMBLY

Prior to removing the chassis, be sure to draw the power supply plug from a wall outlet. Then, proceed with the removal work in the following order after disconnecting all of the connection cords at the rear of the set.

- 1) To remove the cabinet:  
Remove 4 screws ① retaining the cabinet (2 screws each for the right and left sides), then the cabinet can be detached.
- 2) To remove the bottom board:  
Turn over the set and remove 6 screws ② retaining the bottom board, then the bottom board can be detached.
- 3) To remove the front panel:  
(1) Use a hexagonal wrench (1.4 mm) to loosen the screw retaining the tuning knob ③ at the front panel, and pull out the tuning knob.  
(2) Pull out the remaining knobs ④ (13 knobs).  
(3) Remove the nuts ⑤ retaining the speaker switch shaft and selector switch shaft.  
(4) Finally remove 2 screws ⑥ retaining the front panel, then the front panel can be detached.

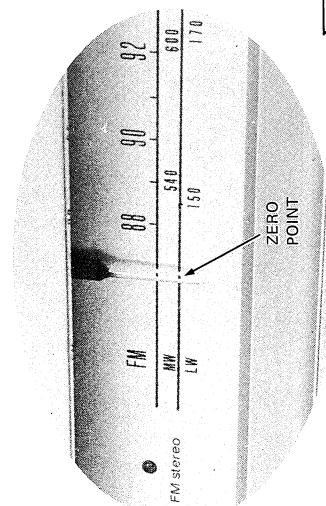
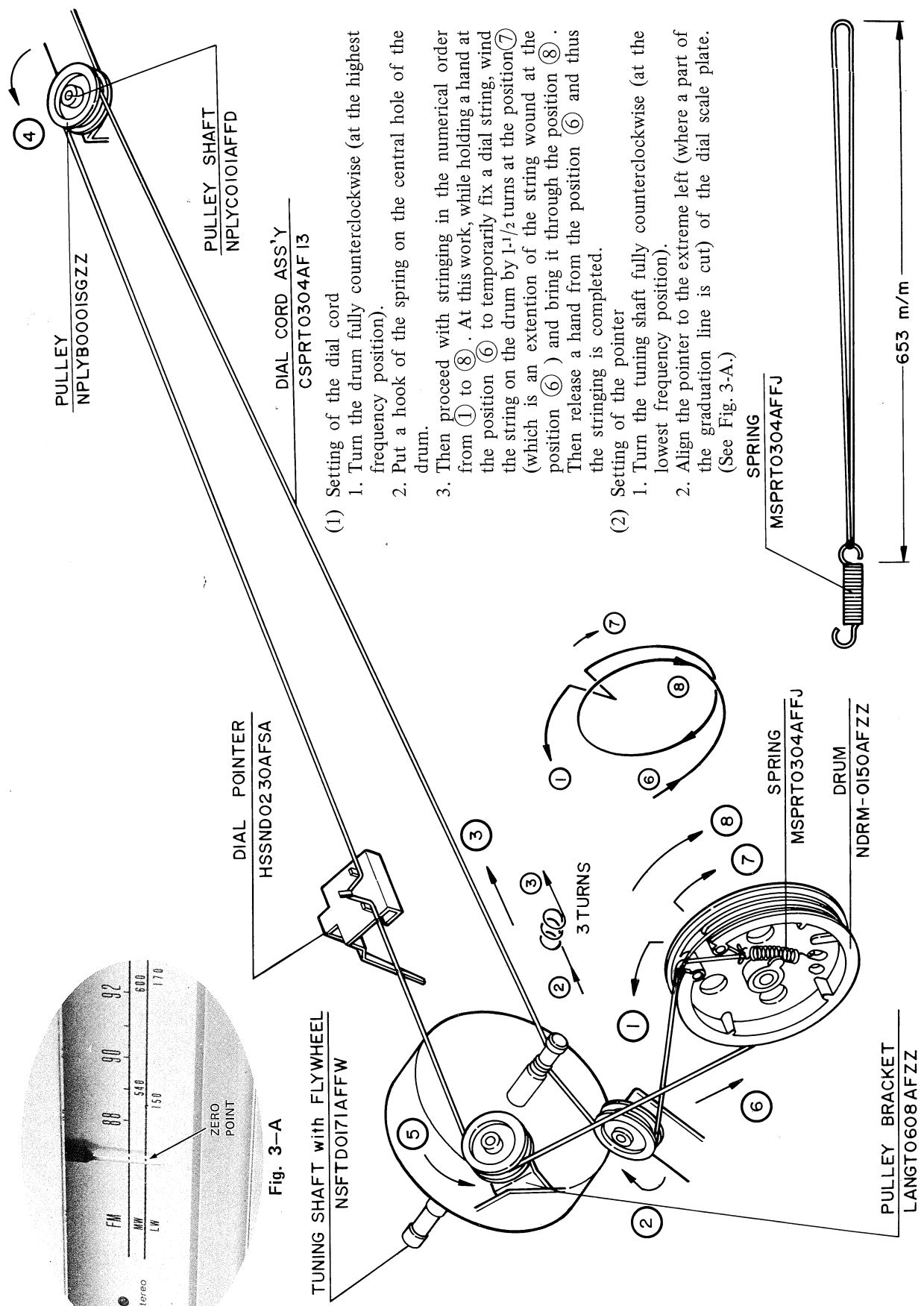


Fig. 3-A



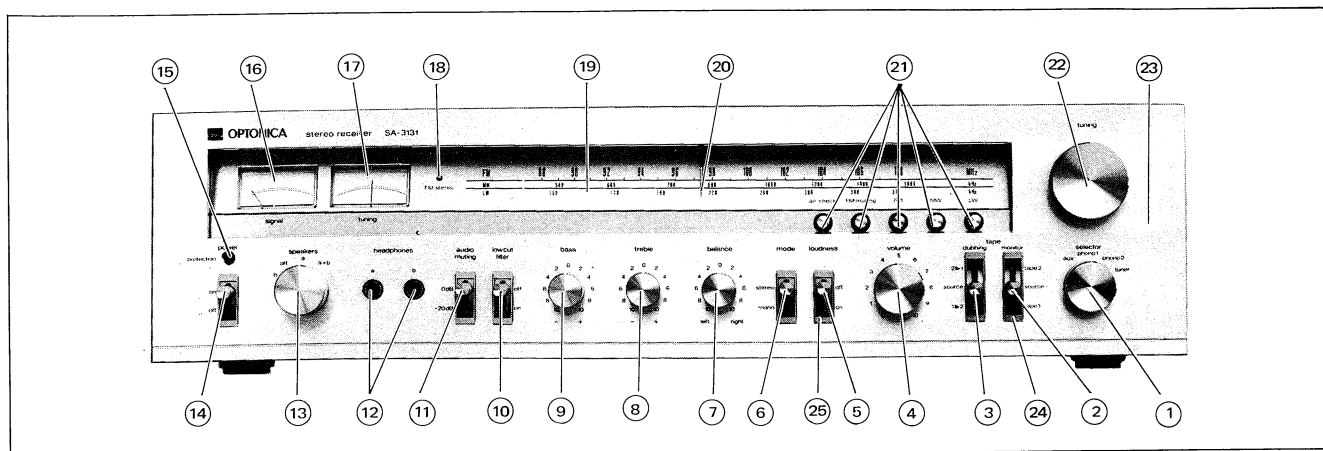
- (1) Setting of the dial cord
  1. Turn the drum fully counterclockwise (at the highest frequency position).
  2. Put a hook of the spring on the central hole of the drum.
  3. Then proceed with stringing in the numerical order from ① to ⑧. At this work, while holding a hand at the position ⑥ to temporarily fix a dial string, wind the string on the drum by 1-1/2 turns at the position ⑦ (which is an extension of the string wound at the position ⑥) and bring it through the position ⑧. Then release a hand from the position ⑥ and thus the stringing is completed.
- (2) Setting of the pointer
  1. Turn the tuning shaft fully counterclockwise (at the lowest frequency position).
  2. Align the pointer to the extreme left (where a part of the graduation line is cut) of the dial scale plate. (See Fig. 3-A.)

Figure 3 DIAL CORD STRINGING

①  
②  
③  
④  
⑤  
⑥  
⑦  
⑧  
⑨  
⑩  
⑪  
⑫  
⑬  
⑭

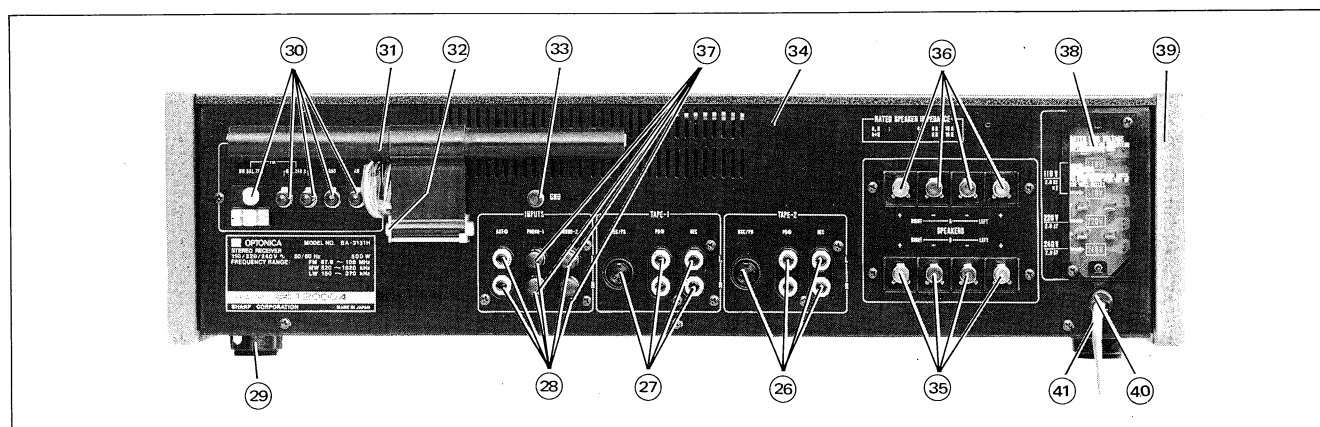
②6  
②7  
②8  
②9  
③0  
③1  
③2  
\* Sh  
For





- |  |  |
|--|--|
| ① Function selector knob (JKNBN0333AFSA)     | ⑮ Power source/circuit protection indicator, LED (VHPGL-52RG/1F) |
| ② Tape monitor switch knob (JKNBP0070AFSA)   | ⑯ Signal strength meter, ME801 (RMTRL0135AFSA)                   |
| ③ Tape dubbing switch knob (JKNBP0070AFSA)   | ⑰ FM tuning (center) meter, ME802 (RMTRL0134AFSA)                |
| ④ Volume control knob (JKNBN0333AFSA)        | ⑱ FM stereo indicator, LED (VHPSR105D // -1)                     |
| ⑤ Loudness switch knob (JKNBP0070AFSA)       | ⑲ Dial (HDALM0170AFSA)   |
| ⑥ Mode selector knob (JKNBN0334AFSA)         | ⑳ Dial pointer (HSSND0230AFSA)                                   |
| ⑦ Balance control knob (JKNBN0334AFSA)       | ㉑ LW/MW/FM/FM muting/Air check knob (JKNBM0248AFSA)              |
| ⑧ Treble control knob (JKNBN0334AFSA)        | ㉒ Tuning control knob (JKNBB0059AFSA)                            |
| ⑨ Bass control knob (JKNBN0334AFSA)          | ㉓ Front panel (HPNLC3273AFSA)                                    |
| ⑩ Low cut filter switch knob (JKNBP0070AFSA) | ㉔ Guide (Large), lever switch (GCOVA1070AFSC)                    |
| ⑪ Audio muting switch knob (JKNBP0070AFSA)   | ㉕ Guide (Small), lever switch (GCOVA1071AFSC)                    |
| ⑫ Headphone jacks (a, b) (QJAKJ0057AFZZ)     |  |
| ⑬ Speakers selector knob (JKNBN0333AFSA)     |  |
| ⑭ Power switch knob (JKNBP0070AFSA)          |  |

Figure 4 FRONT PARTS LAYOUT

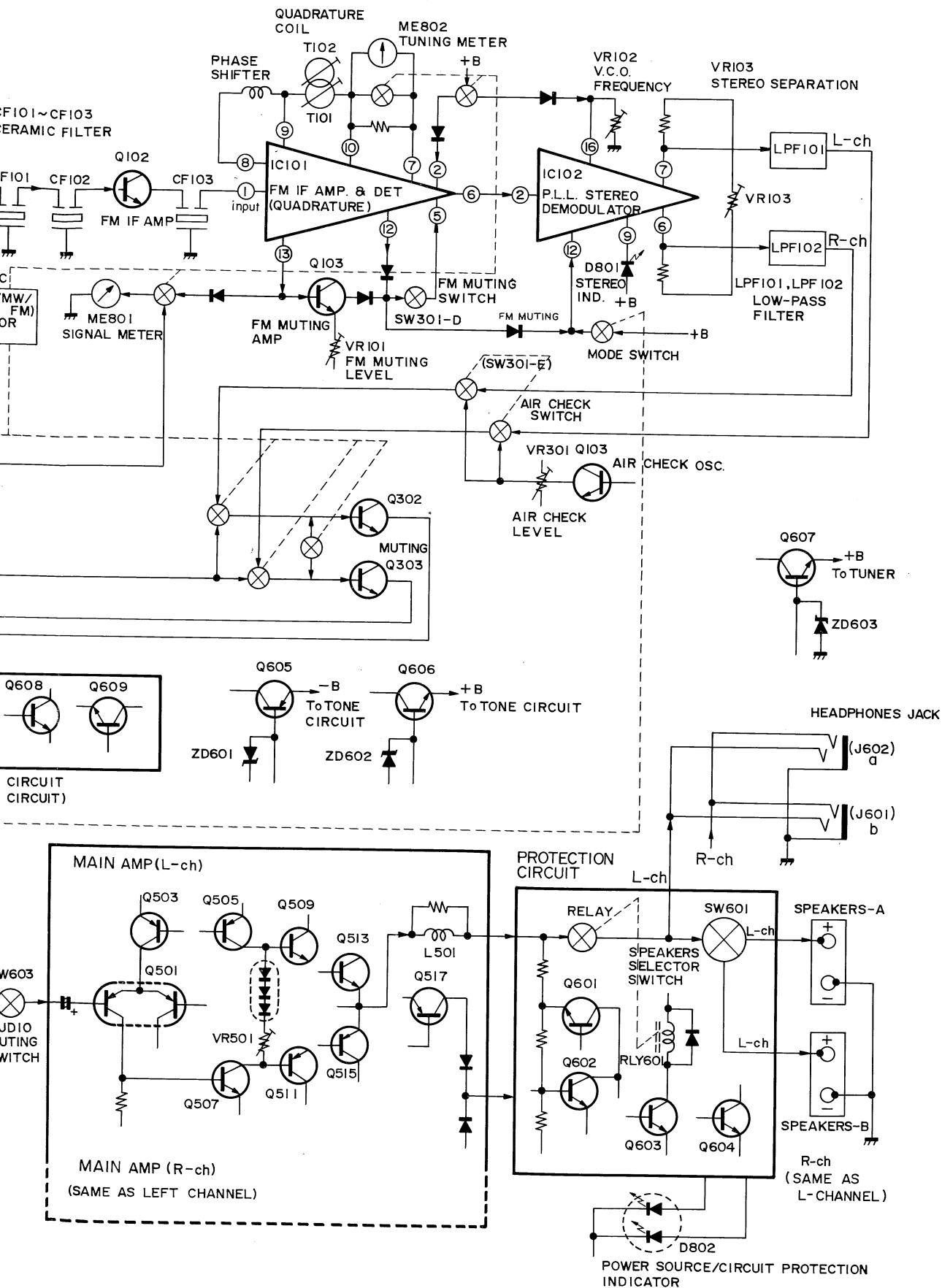


- |   |   |
|---|---|
| ②⑥ Tape-2 (REC/PB) sockets and DIN (REC/PB) (QSOCZ2450AFZZ) | ③③ Grounding (Earth) terminal (QTANN0150AFZZ) |
| ②⑦ Tape-1 (REC/PB) sockets and DIN (REC/PB) (QSOCZ2450AFZZ) | ③④ Rear panel (LANGQ0505AFSA)                 |
| ②⑧ Aux./Phono1/Phono2 input sockets (QSOCJ2660AFZZ)         | ③⑤ Speaker terminals-B (QTANN0454AFZZ)        |
| ②⑨ Leg (GLEGP0002SG00)                                      | ③⑥ Speaker terminals-A (QTANN0454AFZZ)        |
| ③① Antenna terminals (QTANN0453AFZZ)                        | *③⑦ Short plug (QPLGS0102AGZZ)                |
| ③② LW/MW bar antenna (RCILA0403AFZZ)                        | ③⑧ Fuse cover (PCOV1158AFZZ)                  |
| ③③ Bracket of bar antenna (LANGQ0423AFZZ)                   | ③⑨ Cabinet (GCAB-5090AFSA)                    |
|   | ④① Bushing, power supply cord                 |
|   | ④② Power supply cord                          |

\* Short plug

For noise prevention, be sure to insert a furnished short plug into the socket PHONO when not in use.

Figure 5 REAR PARTS LAYOUT



6 BLOCK DIAGRAM

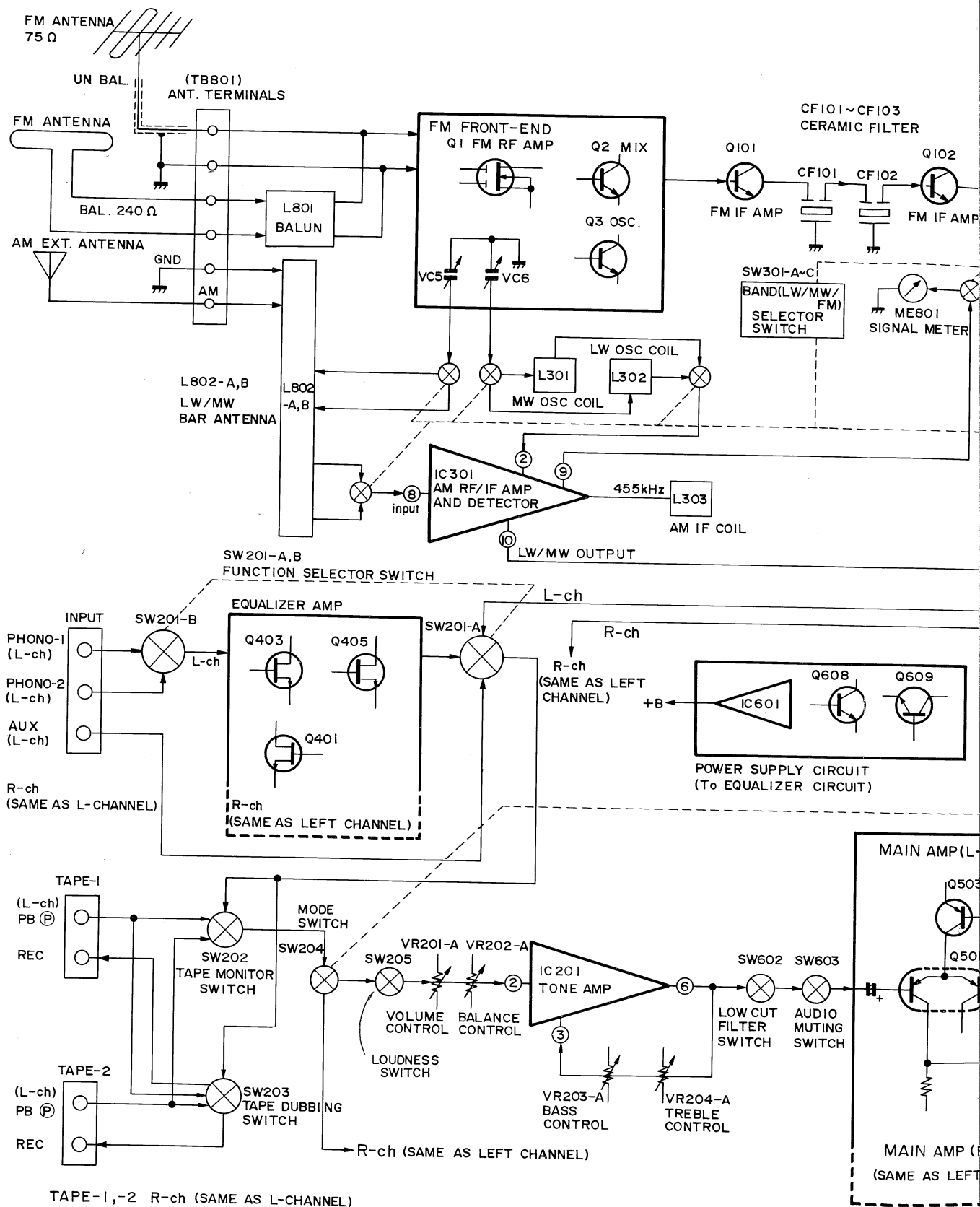


Figure 6 BLOCK DIAGRAM

## CIRCUIT DESCRIPTION

### AM SECTION

#### (1) Block Diagram of IC301

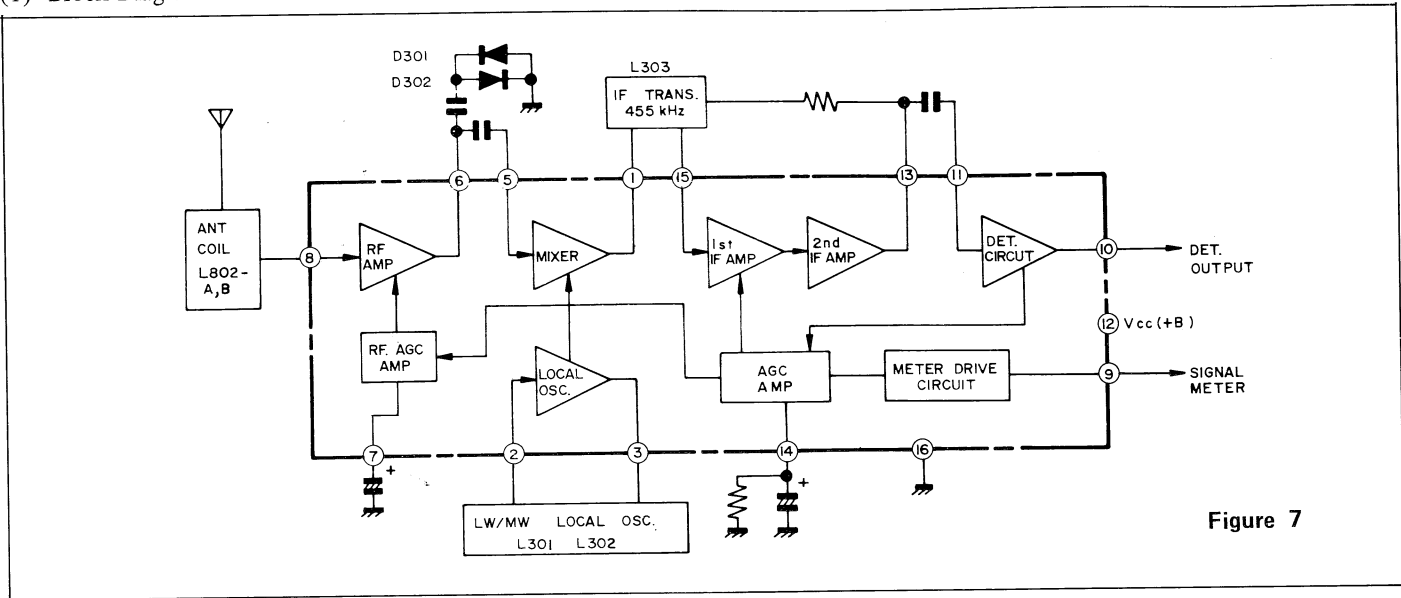


Figure 7

#### (2) Circuit Description

The block diagram of IC301 is indicated as above. AM broadcast signal caught by the antenna coil L802 enter the pin (8) of IC301 and is amplified by RF amplifier to be supplied to the mixer via the overload diodes D301 and D302. Intermediate frequency selection element making use of the ceramic filter L303 is employed as the load for the mixer. AM signal, after being amplified by 1st IF amplifier and 2nd IF amplifier, is detected by the detector circuit. Besides, this IC circuit IC301 incorporates signal meter drive circuit to facilitate the tuning and the output at the pin (9) of IC301 is connected to the signal meter (ME801).

### FM RF SECTION

FM antenna input circuit has two input terminals (75 ohms and 240 ohms) thanks to impedance converter (balun), coil L801. The 75 ohms input terminal is used when FM antenna is connected to the unit by using a coaxial cable. The 240 ohms input terminal is used when FM antenna is connected to the unit by using a balanced feeder. Fig. 8 shows FM Front-End circuit. RF amplifying section consists of 1 dual gate MOS-FET and 2 transistors.

Transistor Q1 is dual gate MOS FET and its function is nearly the same as of vacuum tube. Due to the adoption of MOS FET, crossmodulation characteristic and spurious characteristic are remarkably improved compared with conventional transistor type.

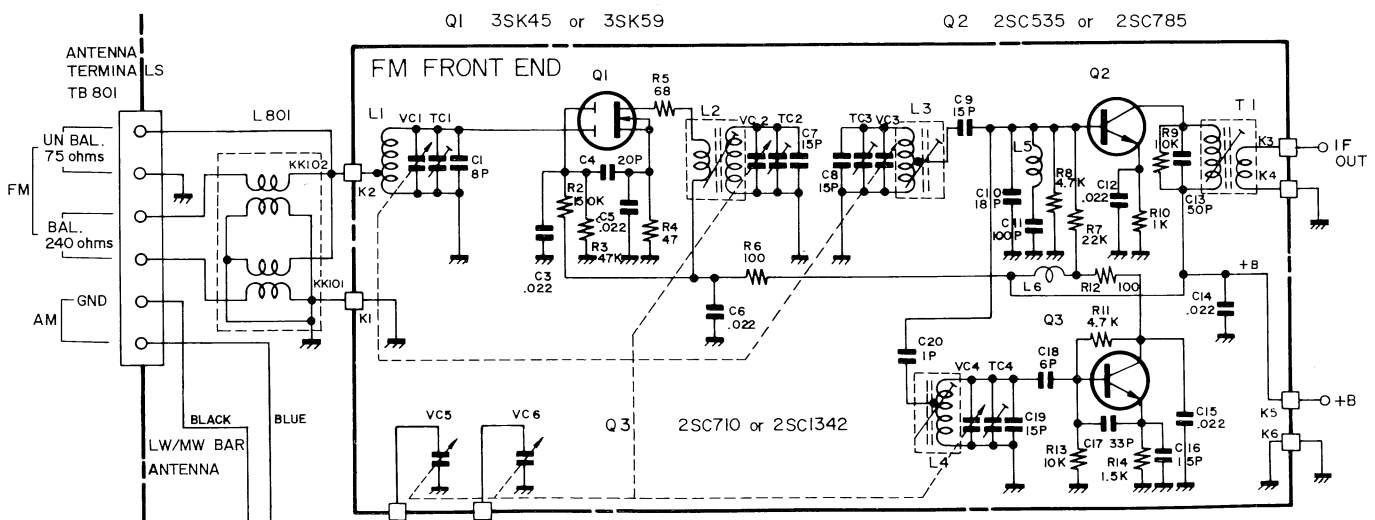


Figure 8 FM FRONT-END CIRCUIT

Dual gate MOS-FET Q1 is FM high frequency amplifier. Transistor Q2 works as frequency mixer, in which high frequency signal coming from the MOS-FET Q1 and local oscillation frequency coming from the transistor Q3 are mixed to produce 10.7 MHz IF signal which will enter IF tuning transformer T1. The transistor Q3 is for the local oscillation and it applies oscillation voltage to the base of transistor Q2 via capacitor C20 (1pF). Therefore, coil L1 is for antenna tuning, coils L2 and L3 are for FM RF amplification and tuning and coil L4 is for local oscillation.

## FM IF SECTION

FM IF section consists of 1 IC (integrated circuit), 2 transistors and 3 ceramic filters. Transistors Q101 and Q102 are FM IF amplification transistor, which is to amplify IF signal which has been converted into 10.7 MHz signal at FM front end section. This 10.7 MHz IF signal is given a higher selectivity since it runs through the concentrated selective elements, that is, ceramic filters CF101, CF102 and CF103. These filters function to amplify IF (intermediate frequency) signals giving no distortion and to assure a necessary selectivity. The IF signal is further supplied to the terminal ① of IC 101, in which the gain of this signal is increased by about 66 dB by the three-stage differential amplifier thus being subjected to an appropriate limiter function.

## FM DETECTION SECTIONS (Quadrature Detector Circuit)

### (1) FM Detector Circuit

This unit employs "Quadrature Detector" based on newly developed IC (Integrated Circuit), which is substituted for ratio detector and Foster-Seeley's detector that have been so far used. The basic structure of quadrature detector circuit is as shown in Fig. 9.

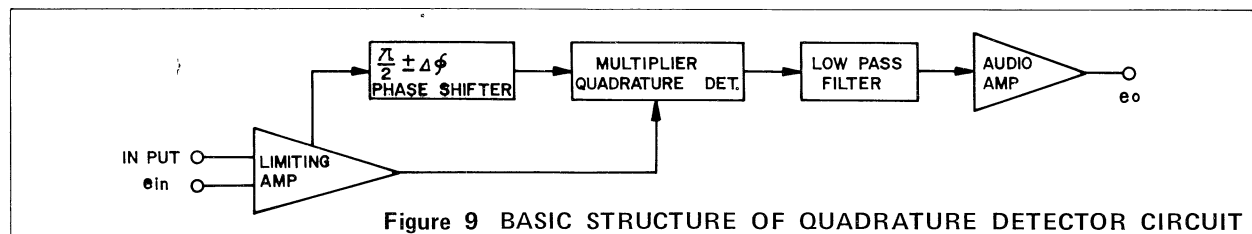


Figure 9 BASIC STRUCTURE OF QUADRATURE DETECTOR CIRCUIT

With this detection system, the multiplier (quadrature detector) circuit receives two types of input signals, one is the signal which has been amplified by the limiting amplifier and another which has passed through the phase shift circuit. (about  $\pi/2$ ). Thus, the quadrature detector circuit produces demodulation signal.

The term "quadrature" is resulted from that the phase difference between these two signal is  $\pi/2$ . The multiplier consists of doubly balance circuit as shown in the following circuit drawing. Phase characteristic of the phase shift circuit is as shown in Fig. 11.

This circuit is featured by:

- (1) Good linearity and low distortion.
- (2) Operates on small signal and less higher harmonics.
- (3) Wide-band detection of as much as 1.2 MHz.

Therefore, this circuit assures low distortion even with the overmodulation of more than 100% thereby reproducing high quality sound.

Actually saying, the detecting circuit SA-3131H uses L104 as phase-shift coil. T101 and T102 are 10.7MHz tuning quadrature coil.

Detection output appears at the terminal ⑥ of IC101 and it is supplied to the terminal ② of P.L.L. multiplex integrated circuit IC102.

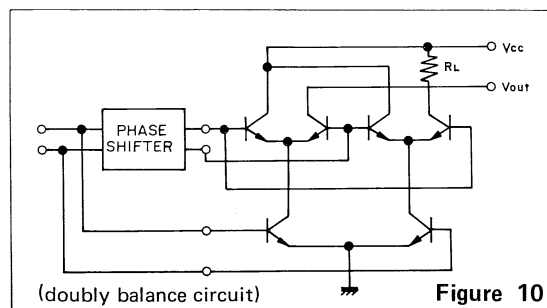


Figure 10

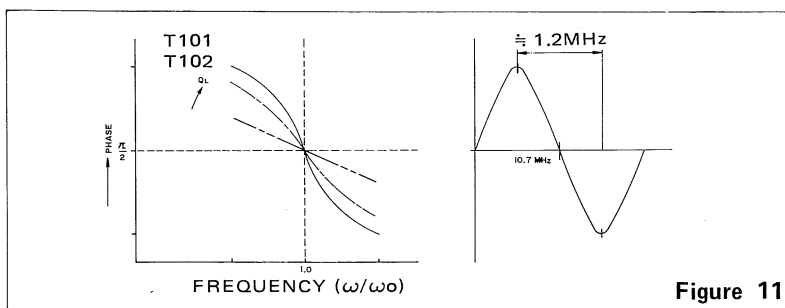


Figure 11

## FM STEREO DEMODULATOR SECTION

### 1) Features of P.L.L. stereo demodulator circuit.

This set incorporates a stereo demodulator circuit that comprises IC's with the PLL (Phase Locked Loop) system applied. The PLL (Phase Locked Loop) FM demodulator circuit is provided with such characteristics as mentioned below.

In order to demodulate stereo composite signals, it is necessary to take a 19kHz pilot signal out of the stereo composite signals and to make it a 38kHz signal.

Most of the conventional methods to obtain such a 38kHz signal are frequency doubling ones which utilize a nonlinearity of the elements. Compared with the conventional type, the recently developed IC-ed demodulator provides more sufficient separation effects. However, since it also requires 2 or 3 coils like the conventional one, if even one of them is dislocated from the initially adjusted point due to a secular change the separation effects will be deteriorated. Moreover there is such a contradiction that the more the efficiencies of the coils are increased enough to withstand the outer pulse signals like automobil ignition noises, the more the coils suffer secular changes.

To eliminate such disadvantages as above, PLL (Phase Locked Loop) system is employed in the method to make a 38kHz signal using a 19kHz pilot signal.

The PLL system stereo demodulator gives such three merits as:

1. Since the phases of a pilot signal and a 38kHz signal are automatically made the same with each other, the deterioration of separation effect is strongly minimized.
2. Since only one of variable resistor, being newly employed, plays the role of 2 to 3 pieces of conventional coils, troubles of the parts due to secular changes are decreased. In addition, even if this variable resistor is slightly dislocated, the separation effect will never be deteriorated because of the merit as mentioned in 1 by which the automatic phase adjustment is assured.
3. Compared with the conventional one, the PLL system demodulator shows a more noise withstanding characteristic since it has such performances as the selection of frequencies and the continuity of oscillation frequencies (short-time memory), thus assuring a stable stereo demodulation.

### 2) FM stereo demodulator circuit of SA-3131H.

IC102 is an integrated circuit for P.L.L. stereo demodulation and its block diagram is as shown in Fig. 12. V.C.O. free-running frequency is to be adjusted to 76 kHz by adjusting semi-fixed resistor VR102 (10K ohm). TP107 is the test point for frequency observation. (See the paragraph "Adjustment" described later.) During LW/MW reception, +B voltage is supplied to the terminal (16) of IC102 through diode D106 and resistor R138 so that oscillation frequency of V.C.O. will be stopped. Semi-fixed resistor VR103 (220K ohm) aims at the adjustment of stereo separation and with this resistor it is possible to minimize crosstalk to the opposite channel. +B voltage is supplied to the terminal (12) to force stereo signals to become monaural ones.

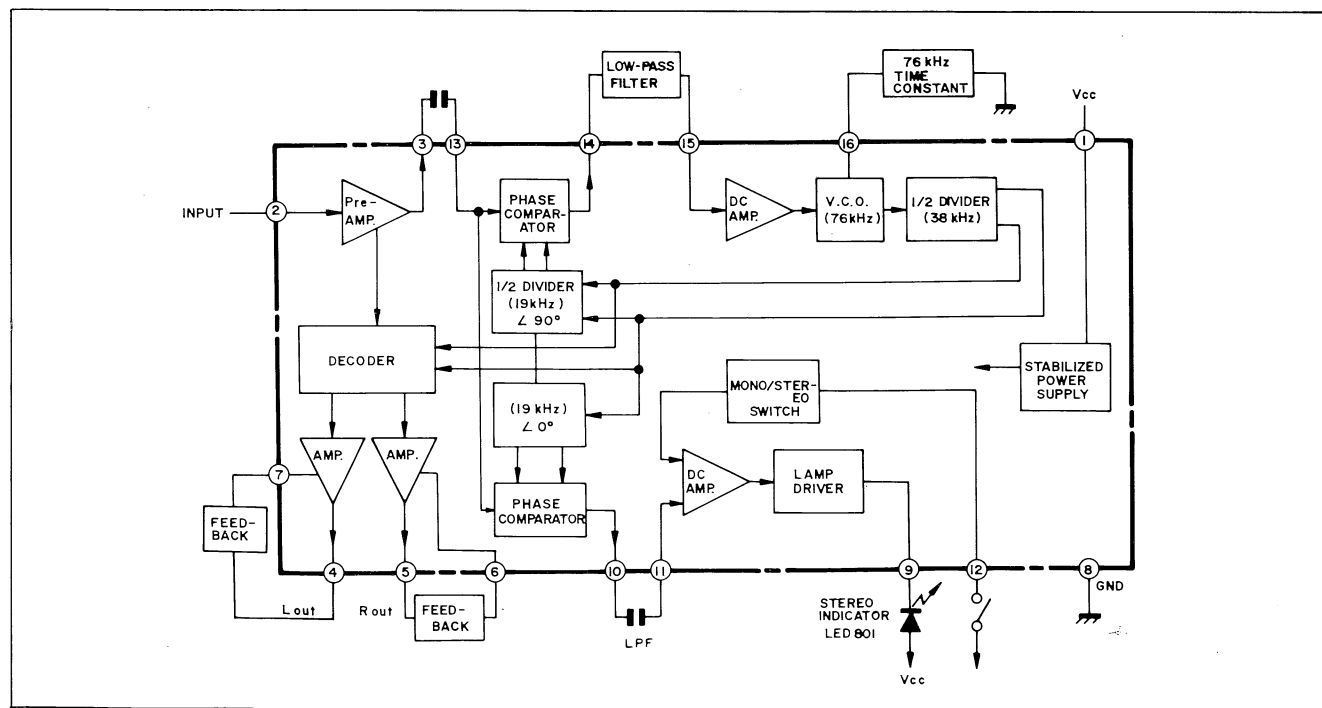


Figure 12

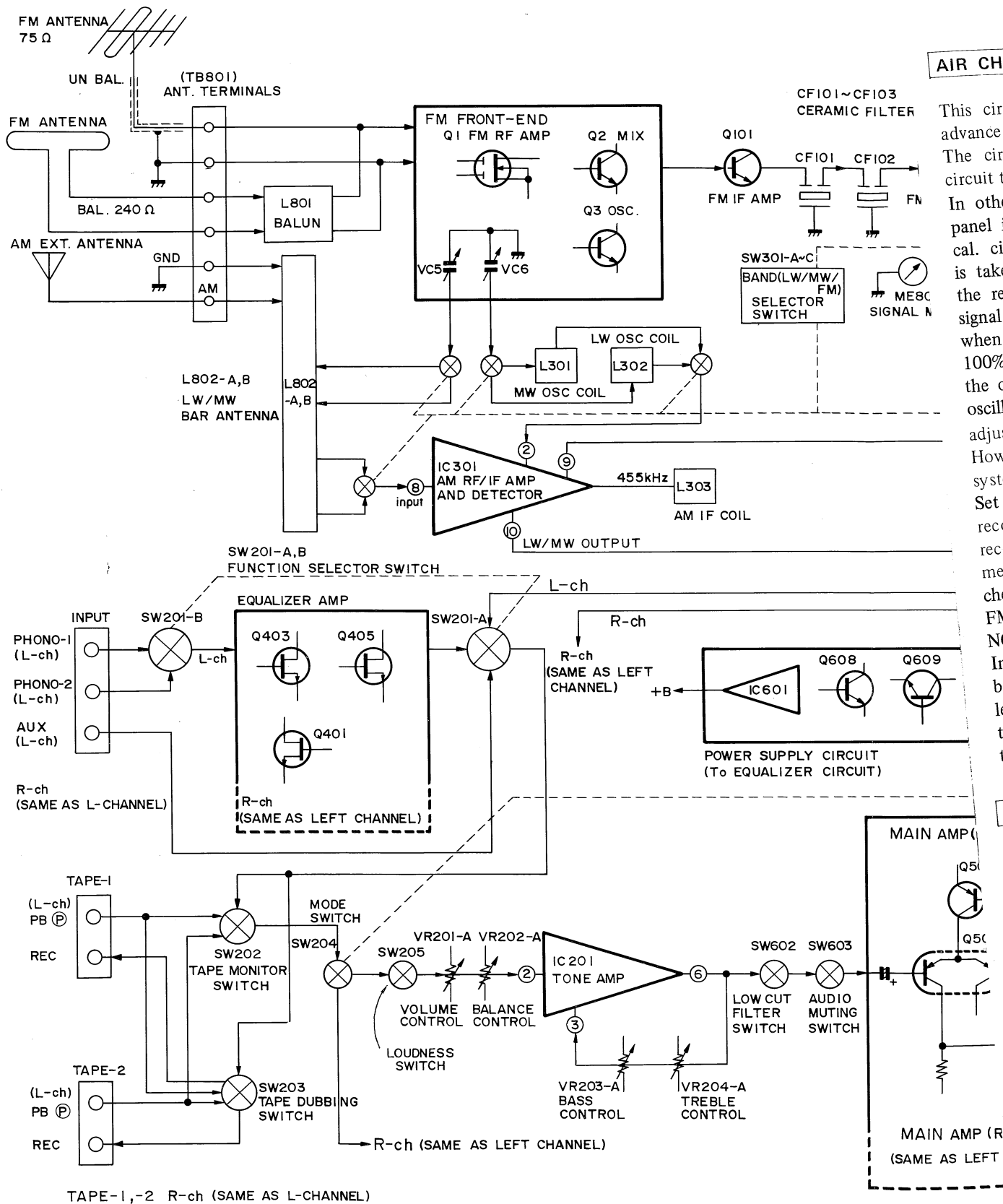


Figure 6 BLOCK DIAGRAM

## TONE AMPLIFIER CIRCUIT

The tone amplifier circuit adopts the integrated circuit (IC) which is of high gain, differential 1-stage and directly-coupled 3-stage type, thus generation of distortion being limited. The power supply is of 2-power (positive and negative) system, in which the voltage at the input and output terminals is designated to be 0V. The coupling capacitor used for input and output signals is of the low leak type which enables reduction of residual noises. The variable resistor aimed to control bass and treble is able to control the resistance in particular when the set is kept in "mechanical center" condition so that beat characteristic at the tone flat mode can be minimized.

Signal coming from the function selector switch is once supplied to the tape monitor switch, mode switch, loudness switch, volume control (VR201-A,B) and balance control (VR202-A,B), and then to the terminal ② of IC201 via the capacitor C205. The signal is amplified in the IC201 to come out of the terminal ⑥ and it is applied to the filter circuit via the capacitor C217.

A part of the output signal of the coupling capacitor C217 is applied to the terminal ③ of IC201 through the tone NF circuit. The tone NF circuit consists of the bass control (VR203-A,B) and the treble control (VR204-A,B) which are to carry out intensification or attenuation respectively of bass and treble ranges. Each of the controls is adjustable every 2 dB.

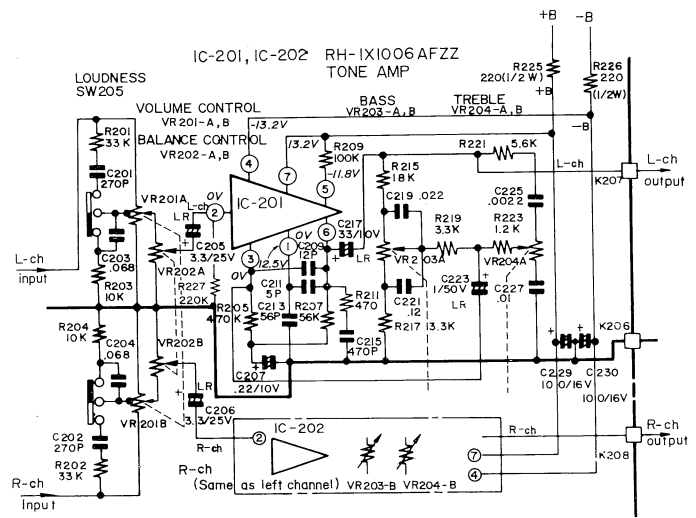


Figure 17

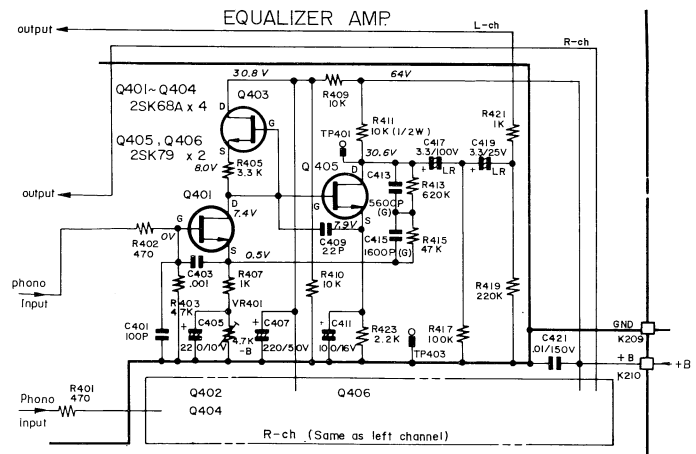
## EQUALIZER AMPLIFIER CIRCUIT

This equalizer circuit is designed to operate on high voltage so that it can obtain higher allowable input level. As a result of the entire adoption of FET (Field Effect Transistor), the circuit also achieves better S/N ratio.

Signal entering the terminal PHONO is, via the resistor R402, applied to FET Q401 to be amplified. To the FET Q401 is connected resistor R405 and FET Q403 as load, and this connection can provide an effect equivalent to that of a special larger resistor so that the amplification factor of FET Q401 is too much assured --- thus the characteristic of FET Q401 is compensated for, say, the distortion characteristic becomes improved. The signal thus amplified in the FET Q401 is applied to FET Q405 to be further amplified. This FET Q405 is of V-FET (Vertical type) which has the same characteristic as the high-voltage withstand triode and it can be said an optional one when used in the equalizer circuit since its output impedance is lower and it is not so much affected by NF element and other loads. Composed of resistors R415 and R413 and capacitors C415 and C413 which are precision parts having too small error. NF element aiming at "RIAA" characteristic is able to restrict "RIAA" deviation to  $\pm 0.5$  dB.

The semi-fixed resistor VR401 (or VR402) is to set the working point of FET Q401 and FET Q403 and with this resistor it is possible to adjust positive and negative clips so that they become symmetrical. In other words, the resistor VR401 (or VR402) is used to adjust so that the drain voltage of FET Q405 (at test point TP401 or TP402) becomes  $+30.6 \pm 0.2$  V when power supply voltage of the equalizer circuit is being +64V.

Resistors R417 and R419 are respectively to prevent capacitors C417 and C419 from discharging and to eliminate noise generation caused at the time of selecting the switches. Capacitors C401, C403 and C409 are for the purpose to prevent interference noises due to SW broadcasts, etc.





## AIR CHECK CALIBRATION CIRCUIT

This circuit is to make appropriate the recording level in advance when recording FM broadcast into the tape recorder. The circuit shown in Fig. 13 hereof is CR type oscillator circuit to be used for the air check calibration. (about 400 Hz). In other words, when the "air check" switch at the front panel is set to "ON" position, (a) and (b) of the air check cal. circuit are connected to each other, oscillator voltage is taken out of (c) and it appears at the output socket at the rear panel being as air check signal level. The air check signal level is set to  $38 \pm 8\%$  of the output voltage obtained when the tuner receives FM broadcast signal (modulation 100% , 75 kHz deviation) and this level voltage appears at the output terminal of the rear panel through the air check oscillator circuit. VR301 is semifixed resistor to be used for adjusting the air check signal level.

How to record FM broadcast using the air check calibration system is described below.

Set the "air check" switch to "ON" position, put the tape recorder in record mode, apply air check signal to the tape recorder and adjust the record level so that the record level meter of tape recorder indicates "0 VU". After that, set the air check switch to "OFF" position and proceed with recording FM broadcast.

### NOTE:

In the case of LW/MW reception, in other words, when the band selector switch is kept to the position LW/MW, air check level signal does not appear at the output terminal located at the rear of the set since the air check calibrator is not functioning at the time.

## FM MUTING CIRCUIT

In SA-3131H, IC101 incorporates muting circuit and this circuit is so designed that if FM input signal to the antenna becomes about 20 dB when the muting switch (SW301-D) is kept at "ON", the muting is released and the signal appears at the output without undergoing muting. The muting release signal is produced by addition of two signals, one is the output signal at the pin (12) of IC101 and another is signal meter signal at the pin (13) which will undergo polarity inversion by the transistor Q103 and these two signals are applied to the pin (5) of IC101 via the muting switch (SW301-D).

Semi-fixed resistor VR101 is adjustable to release the muting when the input signal from the antenna terminal becomes about 20 dB.

Fig. 15 shows the output voltage of two outputs, one is at the pin (12) of IC101 and another, at the collector of transistor Q103, to be added to each other.

This signal (to release the muting) is then supplied to the terminal ⑫ of P.L.L. stereo multiplex demodulator integrated circuit IC102 to make stereo signal be forced to monaural signal.

## LOW-PASS FILTER

LPF101 and LPF102 are low-pass filters to remove carrier signals (19 kHz and 38 kHz) leaking from the stereo multiplex IC102. The characteristic is as shown in the figure 16.

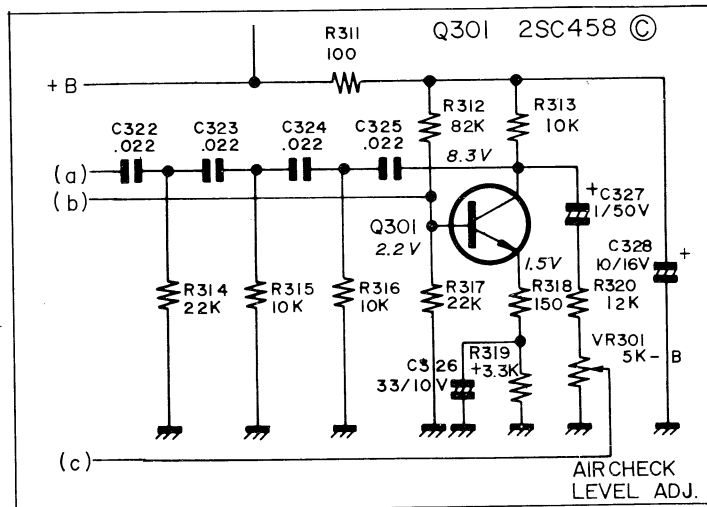


Figure 13 AIR CHECK CAL. CIRCUIT

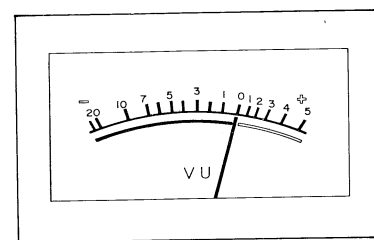


Figure 14 "0 VU"

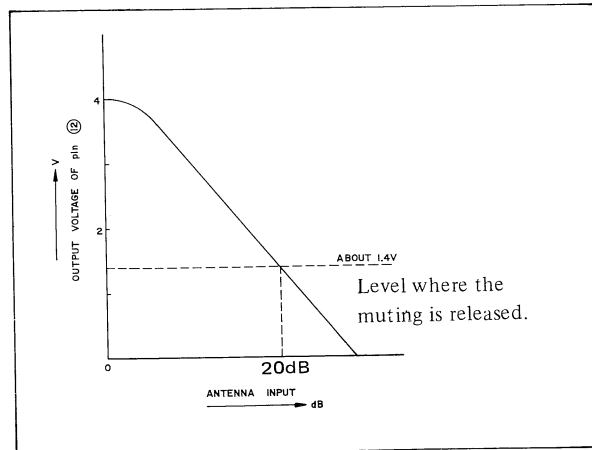


Figure 15

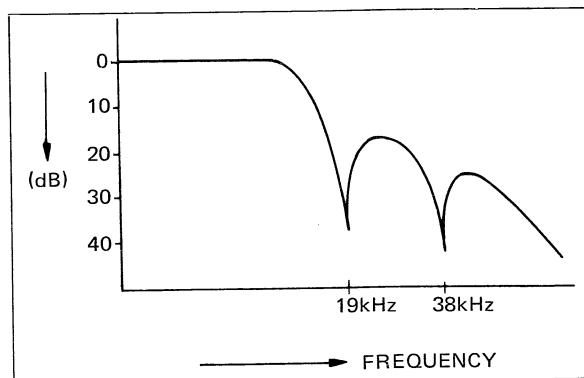


Figure 16

## MAIN AMPLIFIER SECTION

The main amplifier consists of all-stage direct-coupled pure complementary output capacitorless circuit.

This main amplifier is designed to operate on the 2-power (positive and negative) supply system and so the speaker terminal output voltage becomes earth potential (0V) in terms of DC component. Therefore, with this amplifier it is not necessary to use a coupling capacitor for cutting off DC component although it has so far been required when the speaker is connected to the amplifier. Besides, it enables the amplification in a wider range from lower frequency to higher frequency. This is an origin of the term OCL (Output Capacitor-Less).

## FEAUTURE OF PURE COMPLEMENTARY OCL CIRCUIT

Since this circuit is not using output capacitor, the frequency characteristic is kept uniform even at very low frequency band and the output impedance is low in any of frequency bands resulting in that the value of damping factor is made larger so that the braking efficiency of speaker is increased. With this circuit, since a 100 percent NF is assured when the frequency of signal is zero and the value of NF is determined at only one place when the frequency of signal is at low band, the function of circuit is stabilized.

## MAIN AMPLIFIER

The main amplifier is OCL (Output Capacitor-Less) circuit in which the class "A" drive circuit consists of 1-stage differential amplifier circuit.

The signal coming from the filter circuit is amplified by differential amplifier Q501 (or Q502) via resistor R503 (or R504) and capacitor C501 (or C502). The transistor used in this differential amplifier is a PNP type low noise dual transistor (2SA798 ©) the characteristic of which is almost not affected by fluctuations of temperature so that the voltage resulted in the speaker terminal is protected against such fluctuations and it is kept always to minimized.

Signal thus amplified by the differential amplifier is further amplified by the class "A" audio amplifier Q507 (or Q508). Moreover, the signal is amplified for the half cycle at the driver amplifier stage consisting of NPN type transistor Q509 (or Q510) and PNP type transistor Q511 (or Q512). Then, the signal is further amplified for the half cycle at NPN type transistor Q513 (or Q514) and PNP type transistor Q515 (or Q516) to be supplied to the speaker. Transistors Q503 (or Q504) and Q505 (or Q506) are constant-current circuit and its amperage is determined by D503. Transistor Q503 (or Q504) functions to protect the differential amplifier Q501 (or Q502) against fluctuations of temperature and voltage resulting in that the center voltage (speaker terminal voltage) is kept constant. Transistor Q505 (or Q506) is constant-current circuit to supply constant current so that the load applied to the class "A" driver Q507 (or Q508) will be reduced thus the gain being increased. As a result of the gain of Q507 (or Q508) being increased by Q505 (or Q506), plenty of NF is produced and so that distortion is lessened. NF factor of NF circuit is determined by resistors R515 (or R516) and R511 (or R512), and the higher NF factor, the higher is the gain. NF factor at the low frequency band is determined by capacitor C505 and resistor R511.

Transistor Q505 (or Q506) and Diode D503 (or D504) are to cause the bias of class "B" drive stage and to produce idling current of 33 ~ 100 mA so that cross-over distortion due to class "B" operation is eliminated. The idling current is to be adjusted by semi-variable resistor VR501 (or VR502).

Resistor R549 (or R550) and capacitor C511 (or C512) are to keep the power amplifier stabilized when given no load. Coil L501 (or L502) functions to prevent of high-frequency oscillation. Transistor Q517 (or Q518) works as protection circuit.

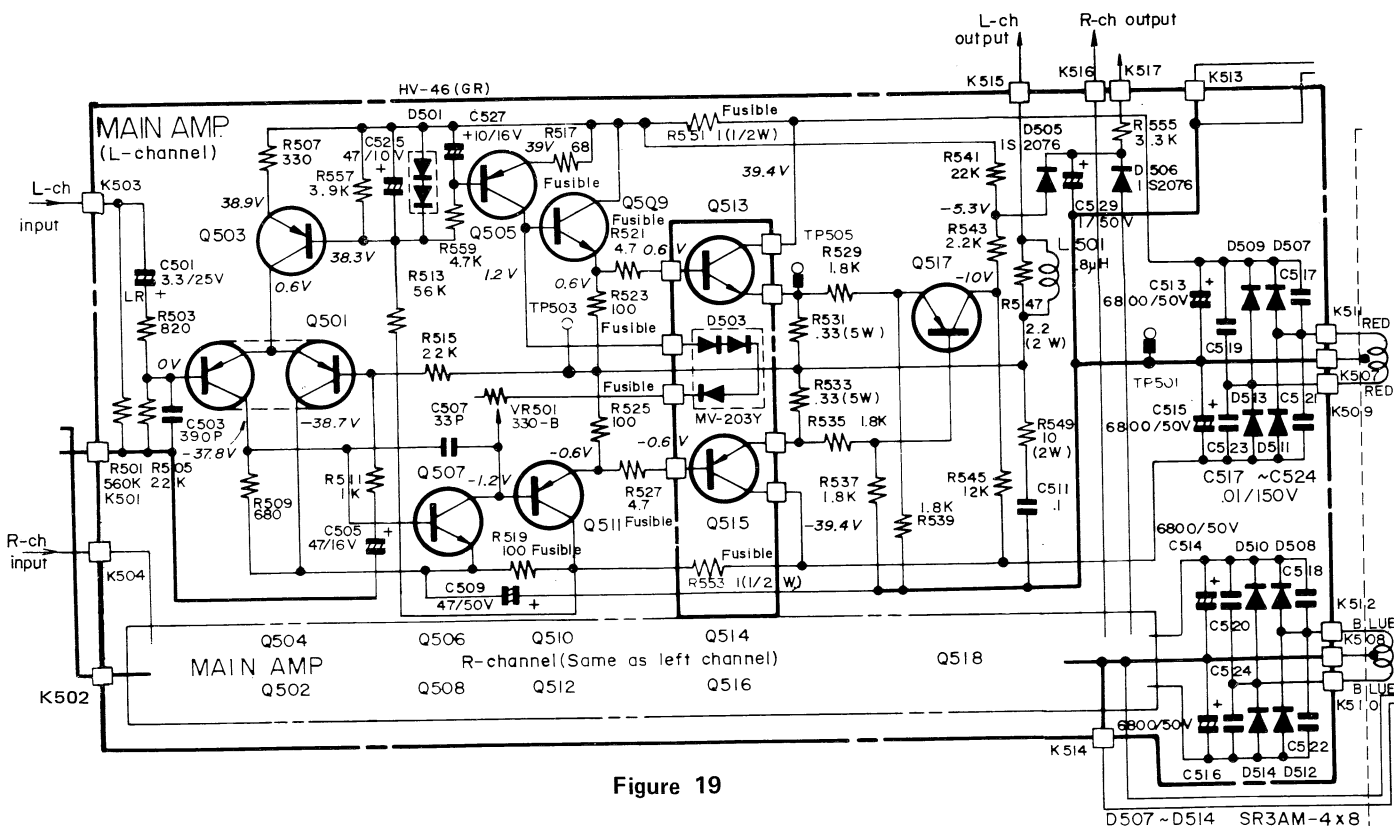


Figure 19

Main amplifier power bandwidth characteristic

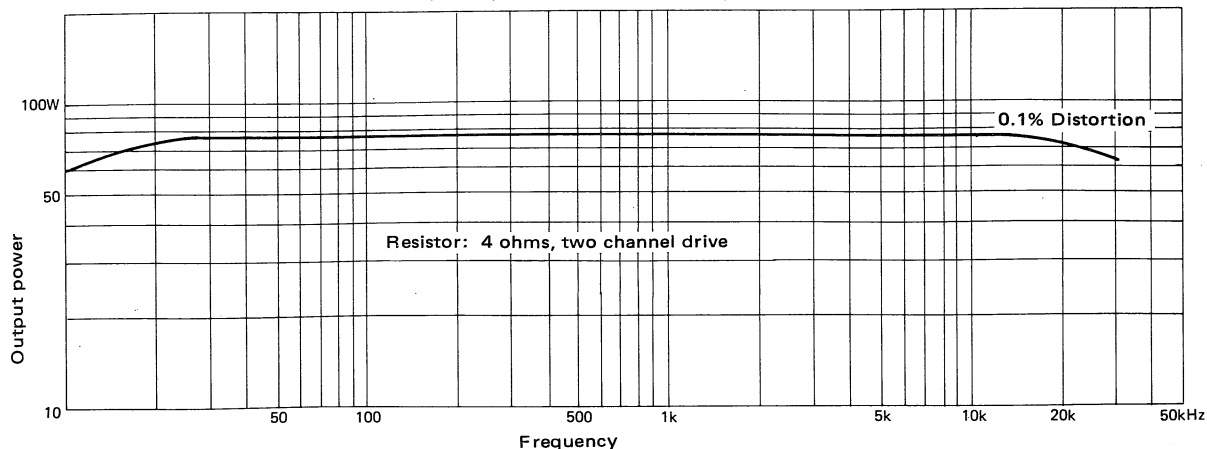


Figure 20

### PROTECTION CIRCUIT (RELAY CIRCUIT)

The protection circuit used in this set is so designed as to function in the following instances:

- (1) It protects the speaker against possible shock noise caused when the power switch is turned on.
- (2) It protects the speaker against possible shock noise caused when the power switch is turned off.
- (3) It functions when DC voltage is generated at the speaker terminal (for instance, when DC voltage gets unbalanced due to a trouble inside the amplifier.)
- (4) It functions when the speaker terminals are shorted and the load impedance is lowered (for instance, when several speakers are connected in parallel to the amplifier.)

Next, we will explain the basic operations of the protection circuit.

The protection circuit is made of two circuits, namely.

Schmitt trigger circuit consisting of transistors Q603 and Q604 and abnormality detection circuit consisting of transistors Q601, Q602, Q517 and Q518.

As to Schmitt trigger circuit, when the base voltage of the transistor Q603 is lower, the transistor Q603 does not function; in other words, the relay does not function since it is given no current so that the speaker circuit is shut off. D802 is 2-color LED (Light Emitting Diode) and it is so designed that it will light up green when the relay is turned on and red when the it is turned off.

Transistors Q601 and Q602 are detection circuits respectively of negative signal and positive signal and each of the two is turned on when given the signal to discharge the potential charged in the capacitor C605, so that the base voltage of the transistor Q603 is decreased and the relay is turned off.

Capacitors C603 and C604 and resistors R606 and R605 are a low-pass filter which prevents mis-operation of the relay due to sound signal. And diode D603 is to absorb the voltage possibly induced when the relay turns on or off.

The above will be further described in detail:

- (1) When the power switch SW801 is set to "on" position, the base voltage of Schmitt trigger transistor Q603 is increased by means of resistors R609 and R608 to have the transistor Q603 be turned on, and thus the relay starts to function. During this process, it is so designed that: since capacitor C605 is being inserted to the base of the transistor Q603, the base voltage of Q603 is kept lower than its emitter voltage until the power supply voltage to the protection circuit will become stabilized and so, during that time, the transistor Q603 is kept off so that the relay does not function since it is given no current. Thus time constant of the relay is determined so that the relay begins to function about 3 to 5 seconds after the power switch is turned on --- in a while the circuits are stabilized to make alive the speakers' connection.

Simultaneously with the above operation, another Schmitt trigger transistor Q604 is turned on and a current runs in the direction which makes the light emitting diode D802 be lit in red.

Distortion factor vs Output characteristic

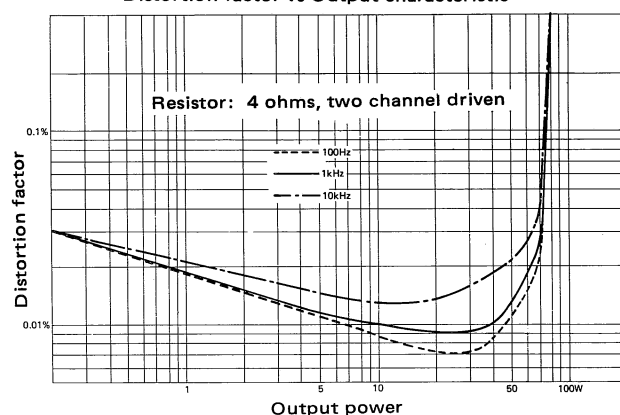


Figure 21

When the power supply voltage is thus stabilized, voltage is charged in the capacitor C605 via resistors R609 and R607 to make the base voltage of the transistor Q603 reach the working point so that the transistor Q603 becomes turned on (at the time, the transistor Q604 is turned off.) A current runs in the relay and the relay begins the operation so that amplifier output will be connected to the speaker terminal. At the time, a current coming from the transistor Q603 runs in the direction which makes the light emitting diode D802 be lit in green.

- (2) The protection circuit is so designed that when the power switch is kept at "on" position, the transistor Q602 is unable to be turned on because a negative voltage coming from the negative rectifier circuit composed of diode D602 and resistor R604 is balanced to a positive voltage coming from the resistor R601. Contrary to the above, when the power switch is set to "off" position, the protection circuit is so designed that: a negative voltage is attenuated faster than a positive one as result of the determination of time constant and so the positive voltage is supplied to the base of transistor Q602 and thus the transistor Q602 is turned on. Then the capacitor C605 begins to discharge so that the base voltage of transistor Q603 is decreased and the transistor Q603 is turned off --- no current runs in the relay and connection of the amplifier output to the speaker terminal is cut off. In short, the protection circuit functions to cut off connection between the amplifier output and the speaker terminal as soon as the power switch is switched off.
- (3) If there appears DC voltage (positive or negative) at the speaker terminal, positive or negative voltage is applied to the transistors Q601 and Q602 through the resistors R605 and R606. As to the positive voltage, it is applied to the base of transistor Q602 via the resistor R603 to have the transistor Q602 be turned on. As to the negative voltage, the emitter voltage of transistor Q601 becomes lower than its base voltage to make the transistor Q601 be turned on. This results in that no current runs in the relay so that connection of the amplifier output to the speaker terminal will be cut off.
- (4) If the speaker terminals are shorted or the load impedance is lowered (for instance, due to connection of the speakers of less than 4 ohms), this can cause a large current to run through the power transistor to be damaged. This trouble can also be avoided by the protection circuit.

If it is supposed that a current of more than the rated value runs in the power transistor, the protection circuit tends to detect abnormal voltage caused at the emitter resistors R531 and R533 (R532 and R534) of the power transistor so that the transistor Q517 (or Q518) is turned on. The voltage thus produced is applied to the base of transistor Q602 via the diode D505 (or D506) and resistor R555 and so the transistor Q602 is turned on. In this way, the protection circuit provides the same effect as said hereinbefore.

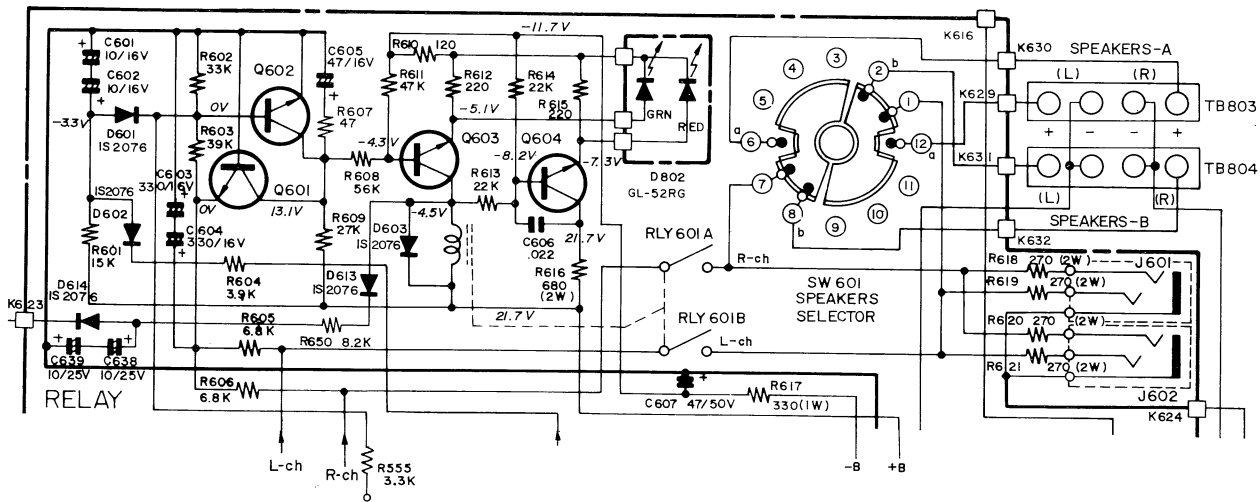


Figure 22

#### POWER SUPPLY CIRCUIT

In the power supply circuit, the secondary of power transformer T801 consists of five windings and 8-power system and this helps to reduce crossmodulation distortion caused due to the power supply circuit impedance as well as dynamic cross-talk between the right and left channels.

As to the power amplifier which requires a larger power, the power supply to it is of 4-power supply system with the right and left windings independent from each other so that mutual interference between the right and left channels is minimized. AC voltage coming from the transformer T801 is rectified by the bridge type full-wave rectifier circuit composed of diodes D507, D509, D511 and D513 (or D508, D510, D512 and D514) and then smoothed by the low impedance dual capacitors C513 and C515 (or C514 and C516) to become DC voltage and it finally is supplied to the power amplifier circuit.

Capacitors C517, C519, C521 and C523 (or C518, C520, C522 and C524) are for the purpose to eliminate switching noises due to diodes D507, D509, D511 and D513 (or D508, D510, D512 and D514) and further to remove noises coming from the power supply primary side.

As to the equalizer amplifier circuit which is liable to greatly affect signal to noise (S/N) characteristic, its power supply is depended upon the voltage regulator circuit formed by transistors Q608 and Q609 and integrated circuit IC601 which achieves a larger loop gain so that noises possibly caused when the function switch is changed over and other noises will be reduced. AC voltage from the power transformer is rectified by the bridge type full-wave rectifier circuit made of diodes D609 to D612 to become DC voltage. This DC voltage thus produced is further smoothed by the capacitors C630 and C631 and resistor R639. Transistors Q609 and Q608 are respectively for voltage regulation and amplification. And integrated circuit IC601 is to carry out error detection. As to DC voltage coming from the resistor R639, its hum and noise components are suppressed by the transistor Q609 and it will be used as power supply to the equalizer amplifier circuit. This output voltage is potential-divided by the resistors R630 and R631 and then applied to the terminal ② of IC601. As to the reference voltage (25V), its noise components are removed by the resistor R634 and capacitor C626 and it is then supplied to the terminal ③ of IC601.

This reference voltage is compared to the said voltage divided by the resistors, R630 and R631 and the resulted difference will be amplified by IC601 to be fed back to the transistor Q609 via the transistor Q608.

If a larger voltage is supposed to be caused, there appears a larger control voltage at the terminal ⑥ of IC601 so that a current more runs in the transistor Q608 --- this results in that the base voltage of transistor Q609 is lowered since there has been more current running in the transistor Q608 and thus the emitter voltage of transistor Q609 becomes lowered. In this way, the output voltage is regulated so that it is lowered and the voltage fluctuation is cancelled and in other words, the power supply circuit can be said a highly regulated one which scarcely causes ripples and noises.

Thus we have explained the case where a larger output voltage is given. The functions contrary to the above will be carried out when a lower output voltage is given. Diode D608 is a speed-up diode which tends to operate when the power switch is turned on.

Power supply voltage to the tone circuit and tuner circuit is depended upon the fact that: AC voltage coming from the power transformer is rectified by the bridge type full-wave rectifier circuit composed of diodes D604 to D607 to become DC voltage and it is further smoothed by the capacitors C612 and C613. DC voltage thus rectified is available in two types, positive one and negative one. As to the tone circuit, the supply voltage is regulated through the ripple filter circuit Q605 (for the negative potential) and the ripple filter circuit Q606 (for the positive potential), while as to the tuner circuit, the supply voltage (positive) is regulated through the ripple filter circuit (transistor Q607).

These regulator circuits all function to effectively suppress fluctuations of the power supply voltage.

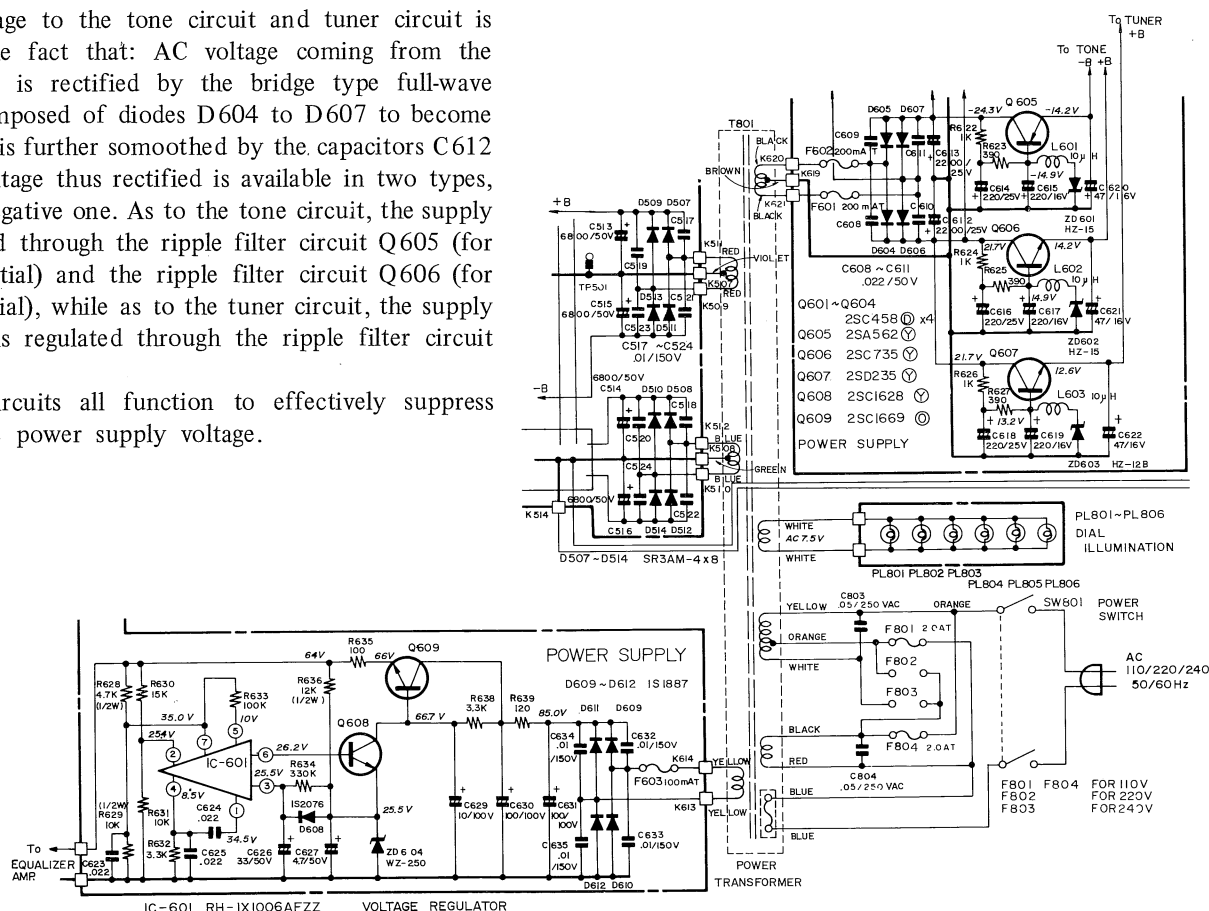


Figure 23 POWER SUPPLY CIRCUIT

## ALIGNMENT INSTRUCTIONS

Alignment is an exacting procedure and should be undertaken only when necessary. If alignment of AM (LW, MW) and FM is required, either section may be done first. The FM stereo section, however, should be done only if the FM monaural section is properly adjusted.

### REQUIRED EQUIPMENT

1. Signal generator with a frequency range of 145 kHz to 1650 kHz; AM (MW, LW)
2. Signal generator with a frequency range of 86.1 MHz to 109.2 MHz; FM
3. Signal generator with a frequency output of 10.7 MHz  $\pm$ 0.5 MHz; FM
4. Vacuum tube voltmeter (AC-VTVM)
5. Sweep signal generator with a sweep range of at least 500 kHz and center frequency of 10.7 MHz with at least a 10.7 MHz marker may be used.
6. Oscilloscope with a wide range amplifier of approximately 100 kHz.
7. Test loops, a coil of any size wire, one turn or more; AM (MW, LW)
8. Vacuum tube voltmeter (DC-VTVM)
9. FM stereo signal generator.
10. Audio signal generator with a frequency range of 20 Hz to 100 kHz.
11. Frequency counter with a frequency range of approximately 100 kHz.

**Notes:** Allow the set at least five minutes to warm up before attempting alignment. During alignment keep the signal generator output at the lowest level that will maintain a usable output from the set.

For the adjustment of stereo separation, the FM stereo generator output is usually 1,000 $\mu$ V. Incorrect grounding to the metal chassis may pick up an unwanted 10.7 MHz signal from the final IF stage, which will cause a regenerative sweep response on the sweep curve and result in misalignment.

Therefore always connect a ground to point.

Ground connection of signal generator	Chassis ground
Generator modulation (AM)	30%, 400 Hz
Generator modulation (FM)	40 kHz, 400 Hz
Generator modulation (FM stereo)	Ch. L. or Ch. R. 40 kHz, 1,000 Hz Mod.

### THE INSTRUCTION OF FM FREQUENCY ADJUSTMENT

In order to comply with FTZ rule: Nr. 358 S757, please fix the low end of dial frequency (87.5 MHz) and high end of dial frequency (107.9 MHz) on FM band, by adjusting oscillation coil (L4) and oscillation trimmer (TC4), respectively, as illustrated in Figure 24.

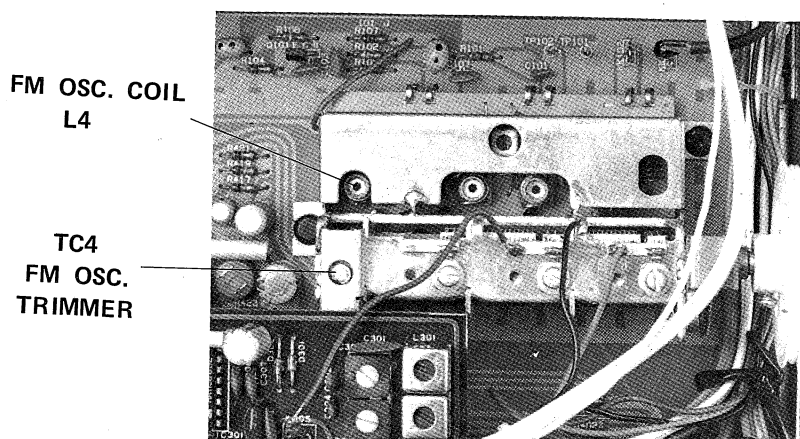


Figure 24 FM FRONT-END

## AF ALIGNMENT

- 1) Set the volume control to the position "minimum" and other switches to the position "normal".
- 2) Turn on the power switch of the set and make sure the voltage in each section is in accordance with the descriptions in Fig. 25.
- 3) Use DC VTVM to make sure that the voltage between K515 and K505 (ground) and that between K516 and K505 (ground) are within the range of  $\pm 30$  mV.
- 4) Only after the above check, it is possible to proceed with the next adjustments.

PROCEDURE NUMBER	ALIGNMENT	METER	OUTPUT INDICATOR	SETTING	ADJUSTMENT	REMARKS
1	Idle Current	DC V.T.V.M.	DC V.T.V.M. is connected between K515(K516) and TP505(TP506)	Volume is minimum position. Other knobs are normal position	VR501 (VR502)	12 mV
2	Equalizer circuit	Same as above.	DC V.T.V.M. is connected between TP401 (TP402) and earth(ground)	Same as above	VR401 (VR402) (Refer to Fig. 27)	30.4 ~ 30.8V

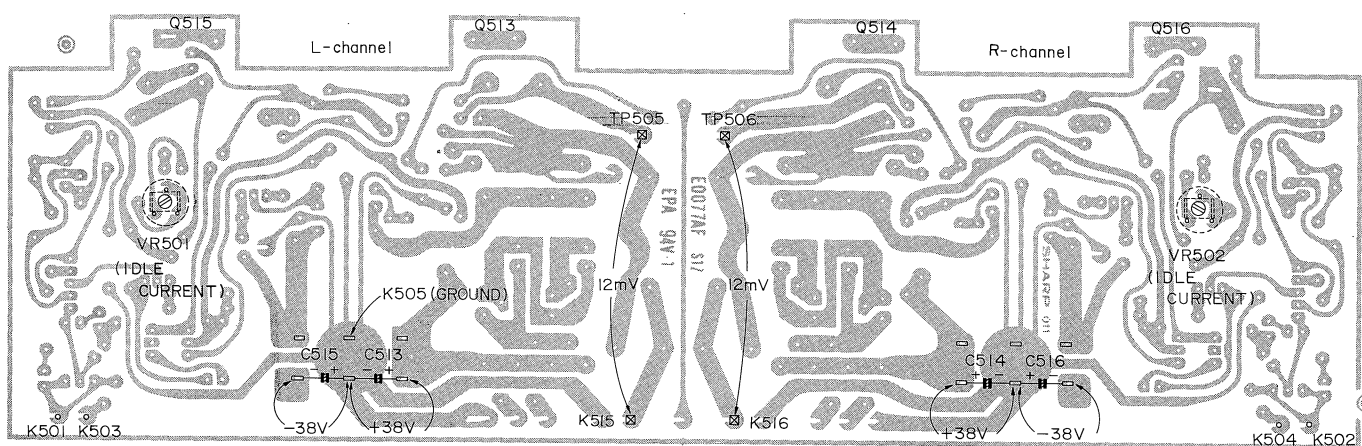
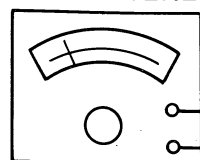


Figure 25 ALIGNMENT POINTS OF POWER AMP. BOARD

## AM IF ALIGNMENT (MW,LW)

PROCEDURE NUMBER	SWEEP GENERATOR		DIAL POINTER SETTING	SELECTOR SETTING	SCOPE CONNECTION	ADJUSTMENT	REMARKS
	CONNECTION	FREQUENCY					
1	Connect AM sweep generator to the test point TP1 (VC5) and variable capacitor case (ground). Keep the input be closed as much as possible.	455 kHz	High end of Dial	Band Selector (MW)	Oscilloscope is connected between TP301 and TP302 (ground)	L303	Maximum response at 455 kHz Repeat 2 or 3 times.

**SIGNAL or SWEEP GENERATOR**



TP1(VC5)  
GROUND



TP301  
TP302 (GROUND)

**OSCILLOSCOPE**

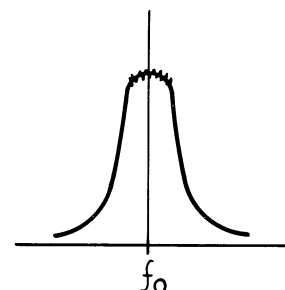
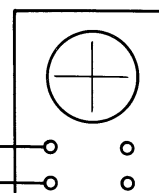


Figure 26 AM IF ALIGNMENT EQUIPMENT CONNECTIONS



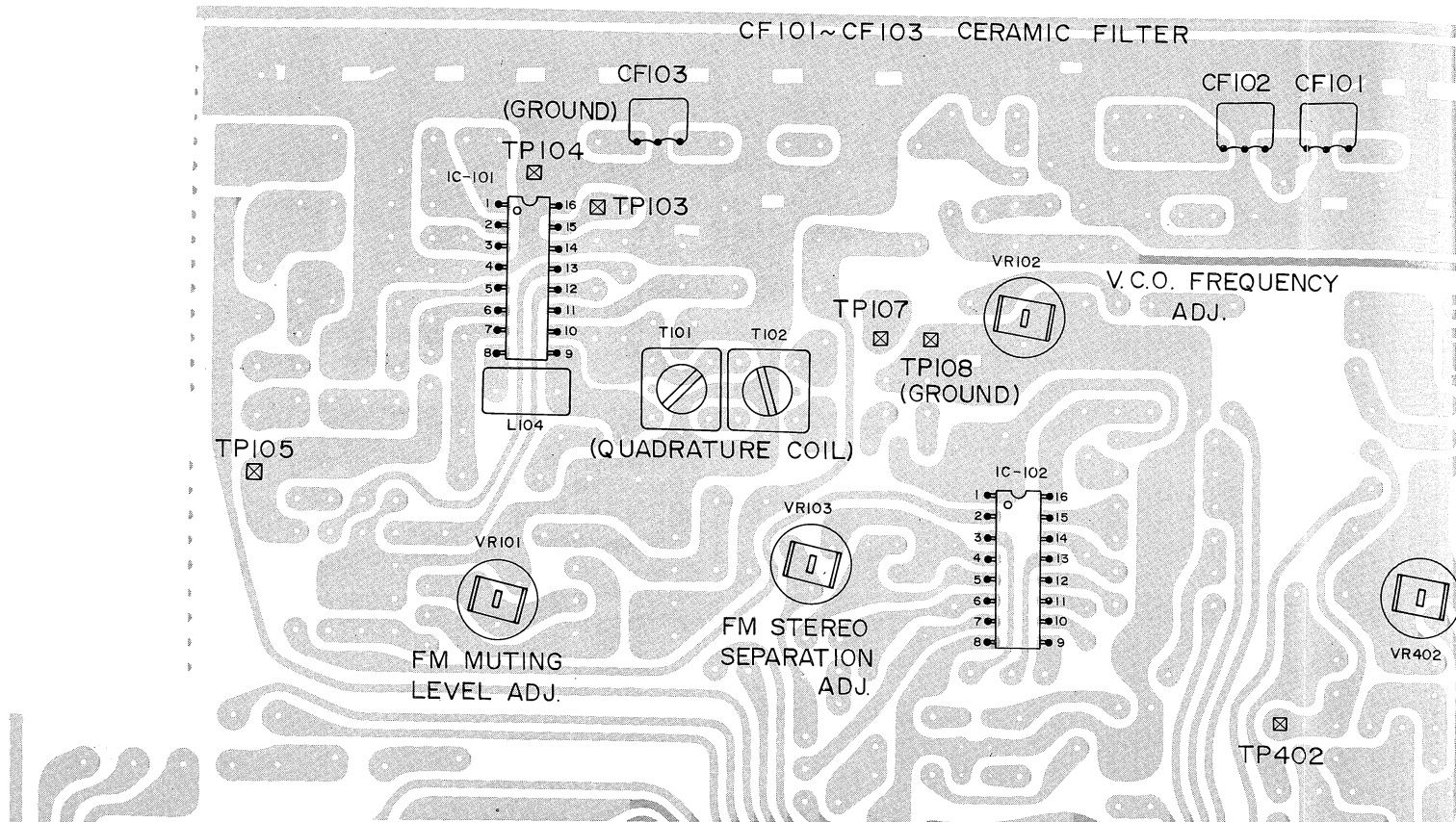


Figure 27 ALIGNMENT POINTS OF FM RF/IF BOARD

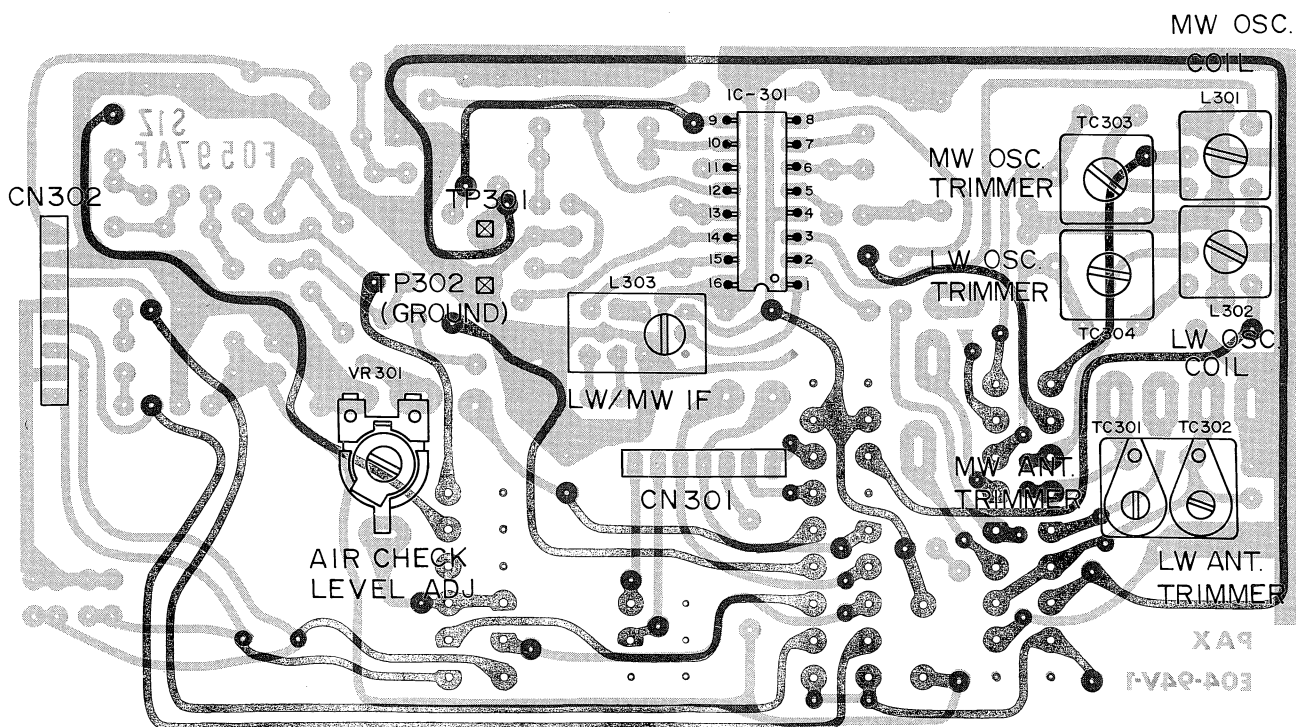


Figure 28 ALIGNMENT POINTS OF AM RF/IF BOARD

Rotate

PROCEDURE  
NUMBER

1

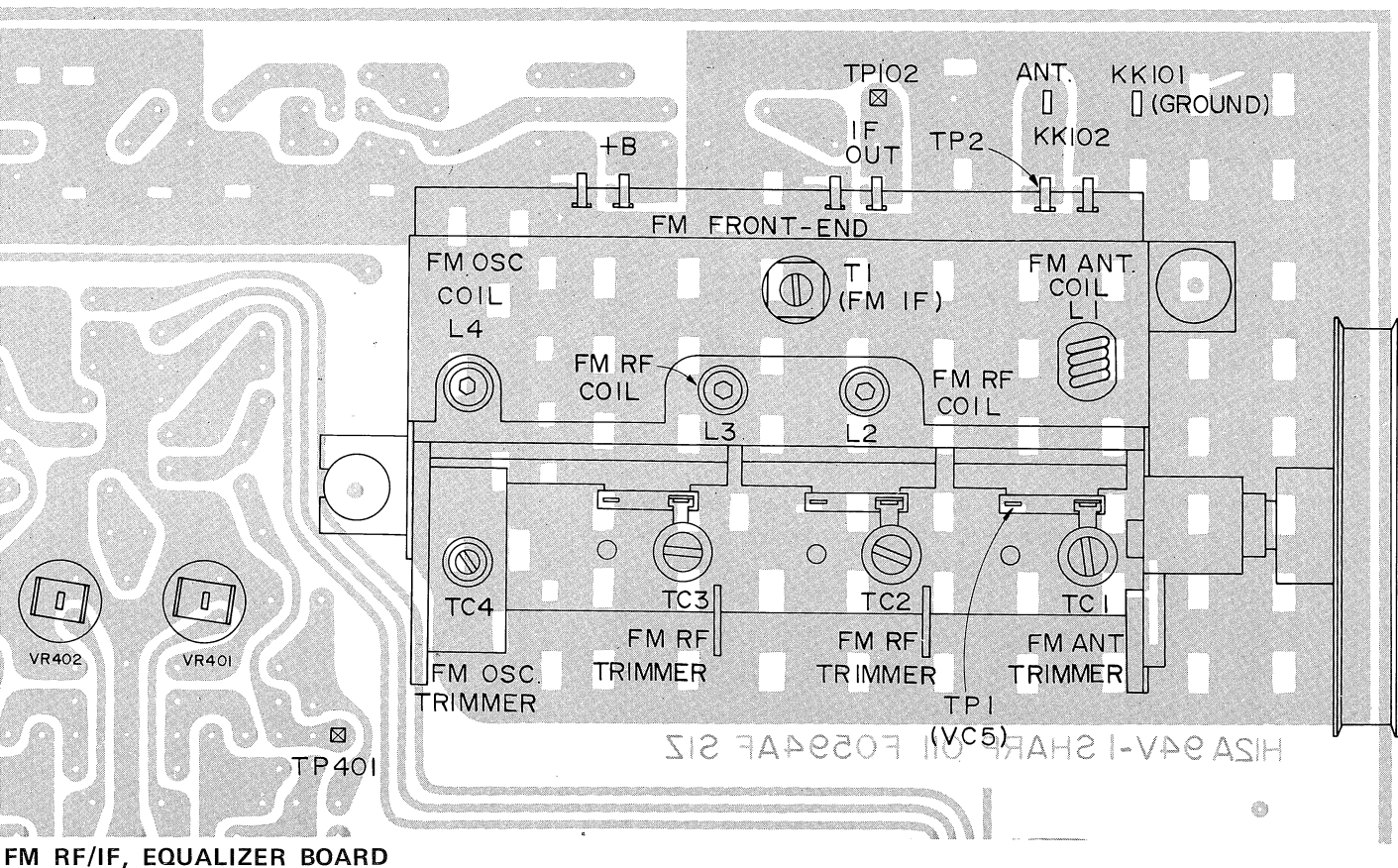
2

3

4

SI  
SV





FM RF/IF, EQUALIZER BOARD

### MW RF ALIGNMENT

Rotate the core of LW oscillation coil L302 fully clockwise.

PROCEDURE NUMBER	TEST STAGE	SIGNAL GENERATOR		DIAL POINTER SETTING	SELECTOR SETTING	SCOPE CONNECTION	ADJUSTMENT	REMARKS
		CONNECTION	FREQUENCY					
1	Band Coverage	Radiated signal as small as possible	515 kHz Modulated	Low end of Dial	Band Selector (MW)	Oscilloscope is connected between TP301 and TP302 (ground)	Oscillator Coil L301	Adjust for maximum output
2		Radiated signal as small as possible	1650 kHz Modulated	High end of Dial	Same as above	Same as above	Oscillator Trimmer TC303	Same as above Repeat steps 1 and 2, 2 or 3 times.
3	Tracking	Radiated signal as small as possible	1400 kHz Modulated	1400 kHz	Same as above	Same as step 1	Antenna Trimmer TC301	Same as step 1
4		Radiated signal as small as possible	600 kHz Modulated	600 kHz	Same as above	Same as step 1	Antenna Coil L802-B	Same as above Repeat steps 3 and 4, 2 or 3 times.

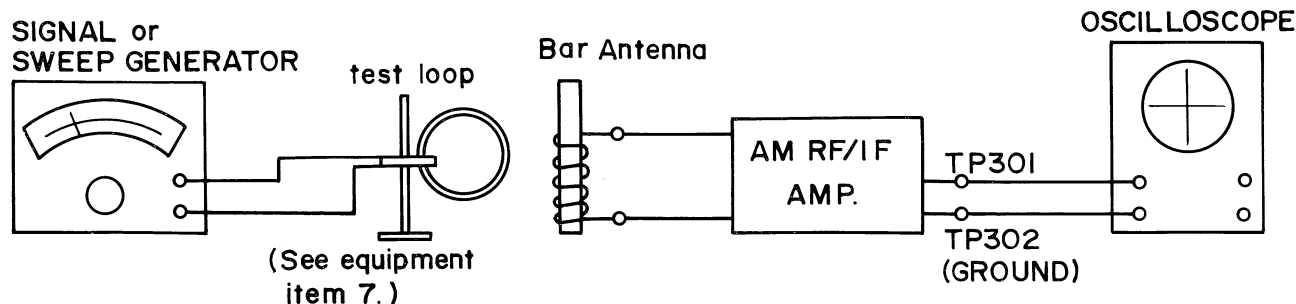


Figure 29 MW/LW RF ALIGNMENT EQUIPMENT CONNECTIONS

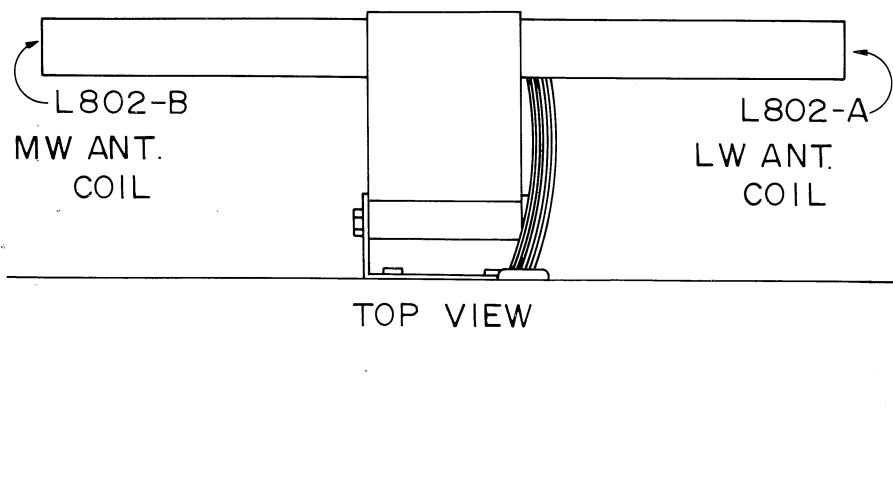


Figure 30 LW/MW BAR ANTENNA

### LW RF ALIGNMENT

PROCEDURE NUMBER	TEST STAGE	SIGNAL GENERATOR		DIAL POINTER SETTING	SELECTOR SETTING	SCOPE CONNECTION	ADJUSTMENT	REMARKS
		CONNECTION	FREQUENCY					
1	Band Coverage	Radiated signal as small as possible	145 kHz Modulated	Low end of Dial	Band Selector (LW)	Oscilloscope is con- nected between TP301 and TP302 (ground)	Oscillator Coil L302.	Adjust for maximum output
2		Radiated signal as small as possible	385 kHz Modulated	High end of Dial	Same as above	Same as above	Oscillator Trimmer TC304	Same as above Repeat steps 1 and 2, 2 or 3 times.
3	Tracking	Radiated signal as small as possible	340 kHz Modulated	340 kHz	Same as above	Same as step 1	Antenna Trimmer TC302	Same as step 1
4		Radiated signal as small as possible	170 kHz Modulated	170 kHz	Same as above	Same as step 1	Antenna Coil L802-A	Same as above Repeat steps 3 and 4, 2 or 3 times.
5		Same as above	145 kHz Modulated	145 kHz	Same as above	Same as step 1	Same as above	Same as step 1

## FM ALIGNMENT

Set the FM Muting switch (SW301-D) at "OFF" position.

PROCEDURE NUMBER	TEST STAGE	SIGNAL GENERATOR		DIAL POINTER SETTING	SELECTOR SETTING	METER CONNECTION	ADJUSTMENT	REMARKS
		CONNECTION	FREQUENCY					
1	IF (NOTE 1 and 2)	Connect FM sweep generator, through 6PF capacitor, to the test point TP2. Connect the ground to the terminal KK101.	10.7MHz $\pm$ 500 kHz as small as possible.	High end of dial	Band Selector(FM), and mono	Connect an oscilloscope to the test points TP103 and TP104 (ground).	T1	Rotate the core of T1 to adjust so that the waveform becomes symmetrical in right and left and attains the maximum in height and width.
2	Detector	Connect FM sweep generator, through 6PF capacitor, to the test point TP102. Connect the ground to the terminal KK101.	Same as above	Same as above.	Band Selector(FM) and mono	Connect an oscilloscope to the test points TP105 and TP104 (ground).	T101, T102	Rotate the core to adjust so that the waveform (Fig.33) becomes symmetrical in the upper and lower with the best linearity.
3	Band Coverage (NOTE 1)	FM Antenna	88MHz as small as possible (Modulated)	Low end of dial.	Band Selector(FM) and mono	Connect VTVM to the test points TP105 and TP104 (ground)	Oscillator coil L4	Adjust for maximum output.
4		FM Antenna	108MHz (Modulated) as small as possible	High end of dial.	Band Selector(FM) and mono	Same as above	Oscillator trimmer TC4.	Same as above 3~4. Repeat 2 or 3 times.
5	Tracking (NOTE 1)	FM Antenna	90MHz (Modulated) as small as possible	90MHz	Band Selector(FM) and mono	Same as step 3	Antenna coil L1 and RF coil L2, L3	Same as step 3
6		FM Antenna	106MHz (Modulated) as small as possible	106MHz	Band Selector(FM) and mono	Same as step 3	Antenna trimmer TC1 and RF trimmer TC2, TC3.	Same as above 5~6. Repeat 2 or 3 times.

### Note 1

As to FM high frequency section (front end section), there is no need to readjust the coil and trimmer since it has been factory-adjusted. It is allowed to readjust them only when there occurs a significant deviation about the preadjustment.

**SIGNAL OR SWEEP GENERATOR**  
10.7MHz ,  $\pm$ 500 kHz

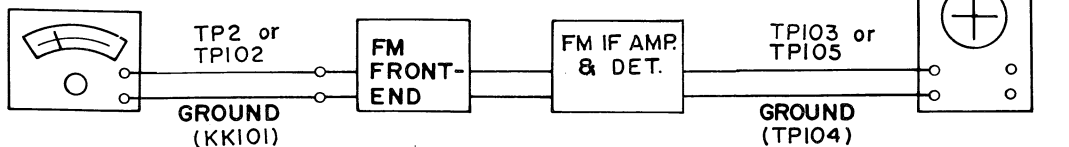


Figure 32 "IF" curve

**SIGNAL OR SWEEP GENERATOR**  
10.7MHz ,  $\pm$ 500 kHz

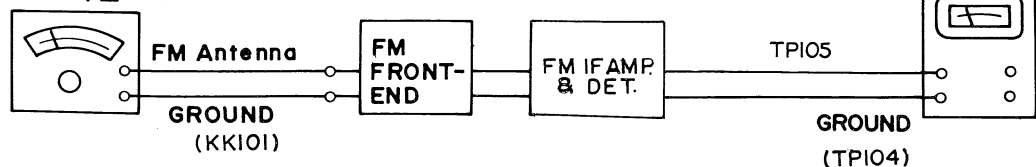


Figure 33 "S" curve

Figure 31 FM ALIGNMENT EQUIPMENT CONNECTIONS

## Note 2

The ceramic filter used for this set is available in 5 types and each of them is given a color indication to differentiate the central frequency from that of the others, as described below. In the actual use, be sure to make 3 ceramic filters of the same type (the same color) as a pair to put them in the set. When other ceramic filters than that given a red color indication (with the central frequency of 10.7 MHz) are used, note that with such filters the marker (10.7 MHz) of FM sweep generator will be deviated; therefore be sure to cut off the marker at the time of the adjustment.

Central Frequency (fo)	Green	10.60 MHz $\pm$ 30 kHz
	Black	10.65 MHz $\pm$ 30 kHz
	Red	10.70 MHz $\pm$ 30 kHz
	White	10.75 MHz $\pm$ 30 kHz
	Yellow	10.80 MHz $\pm$ 30 kHz

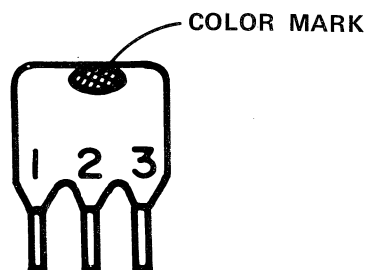


Figure 34

## FM TUNING METER ADJUSTMENT AND DISTORTION FACTOR ADJUSTMENT

- 1) Set the frequency of FM signal oscillator to 98 MHz (75 kHz deviation), fully close the output and connect such signal to the FM antenna terminal of the set through a dummy resistor of 240 ohms.
- 2) Connect a dummy resistor of 4 ohms to the speaker terminal of the set.
- 3) Set the switches and controls of the set to the respective positions shown below and turn on the power switch. [Audio muting—0dB, Low cut filter—off, Bass, Treble and Balance controls—center (zero), Mode—mono, Loudness—off, Volume control—min., Tape (monitor/dubbing)—source, Function selector—tuner, Band selector—FM]
- 4) Keeping the output of FM signal oscillator be fully closed (that is, with no signal given), rotate the core of T101 to have the pointer of the tuning meter indicate the center (around “98 MHz” position.)
- 5) Adjust the output of FM signal oscillator to 60 dB, make the set be tuned to this signal so that the tuning meter indicates its center and under the condition, adjust the core of T102 so that the distortion will be minimized.
- 6) Fully close the output of FM signal oscillator and make sure the pointer of the tuning meter is at the center.
- 7) Repeat the steps 1) to 6) until the best point will be found.

## FM MUTING ADJUSTMENT AND FM STEREO V.C.O., SEPARATION ADJUSTMENT

- 1) Connect FM signal oscillator, through a dummy resistor of 240 ohms, to the FM antenna terminal of the set.
- 2) As to setting of the switches and controls, take the same procedures as in the step 3 “FM TUNING METER ADJUSTMENT AND DISTORTION FACTOR CONTROL”.
- 3) Set the frequency of FM signal oscillator to 98 MHz (40 kHz deviation, 400 Hz) and the output to 20 dB.
- 4) Have the set be tuned in 98 MHz signal, turn on FM muting switch, rotate the semi-fixed resistor VR101 to adjust so that the muting is able to be cleared with the output of FM signal oscillator being 20 dB.
- 5) Set the output of FM signal oscillator to 60 dB (mono signal), place the mode switch of the set to the position “stereo” and let the set be exactly tuned to such signal. (FM muting switch is kept to the position “muting off”.)
- 6) Connect VTVM between the test points TP107 and TP108 (ground) and further connect a frequency counter to output terminal of the said VTVM.  
Make the test points TP105 and TP104 (ground) of the set be connected (shorted). Rotate the semi-fixed resistor VR102 to adjust so that the frequency counter will read 76.00 kHz  $\pm$  200 Hz. (After the adjustment; reset the connection between the test points TP105 and TP104.)
- 7) Connect FM stereo modulator to FM signal oscillator. At the time, the following should be set: modulation frequency; 1kHz (L + R; 20kHz, L—R; 20kHz, pilot (19kHz); 6kHz deviation).
- 8) Set the frequency of FM signal oscillator to 98 MHz and its output to 60 dB, tune the set in such signal so that the tuning meter will indicate the position “center”. Set the modulator so as to cause modulation only in L-channel and consider the output of L-channel as 0 dB. Connect VTVM to the output terminal (R-channel side only) of the set and adjust semi-fixed resistor VR103 so that the separation becomes maximum (the output leaking to the opposite channel is minimized.)

Take the above procedures also for checking the separation of R-channel, then, adjust so that the separations of both channels will be equal to each other.

[ If without the frequency counter, proceed with the alignment as follows. While receiving a FM stereo signal, turn the VR102 until the P.L.L. will be locked (when it is locked, the stereo indicator will be lit). Then, reversely turn the VR102 halfway and fix it.]

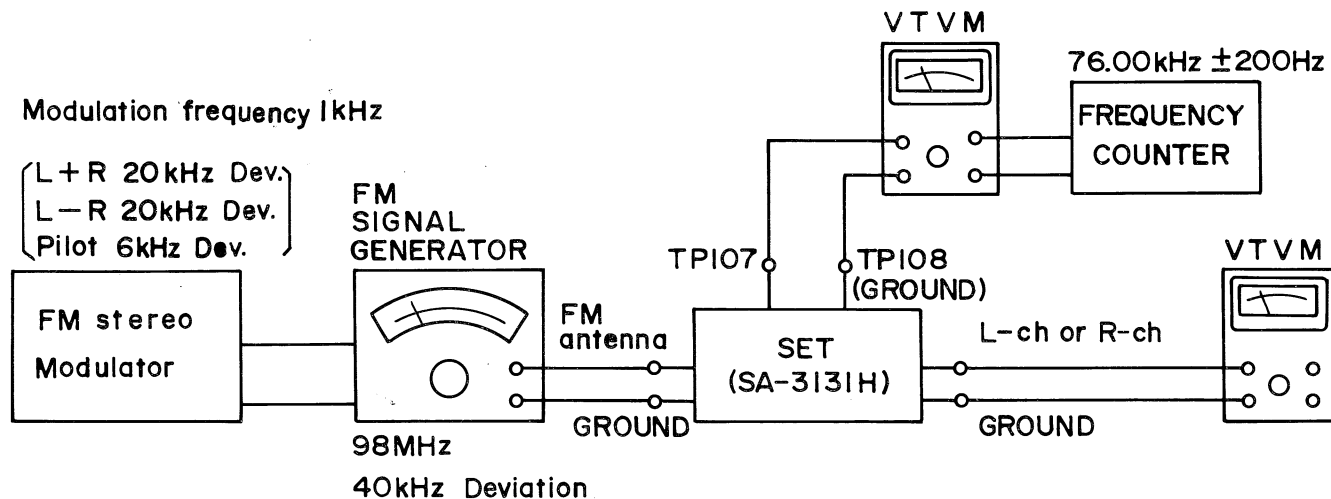


Figure 35 FM STEREO ALIGNMENT EQUIPMENT CONNECTIONS

#### ADJUSTMENT OF AIR CHECK CAL.

Produce 98 MHz, 60 dB FM mono signal (modulation 100%, 400 Hz) by a signal generator to apply it to the antenna of the unit and read the output voltage.

Next, set AIR CHECK switch to "ON" position, then the output voltage will vary. Adjust semi-fixed resistor VR301 so that the output voltage with AIR CHECK switch set to "ON" becomes about 38%, of that with AIR CHECK switch kept at "OFF".

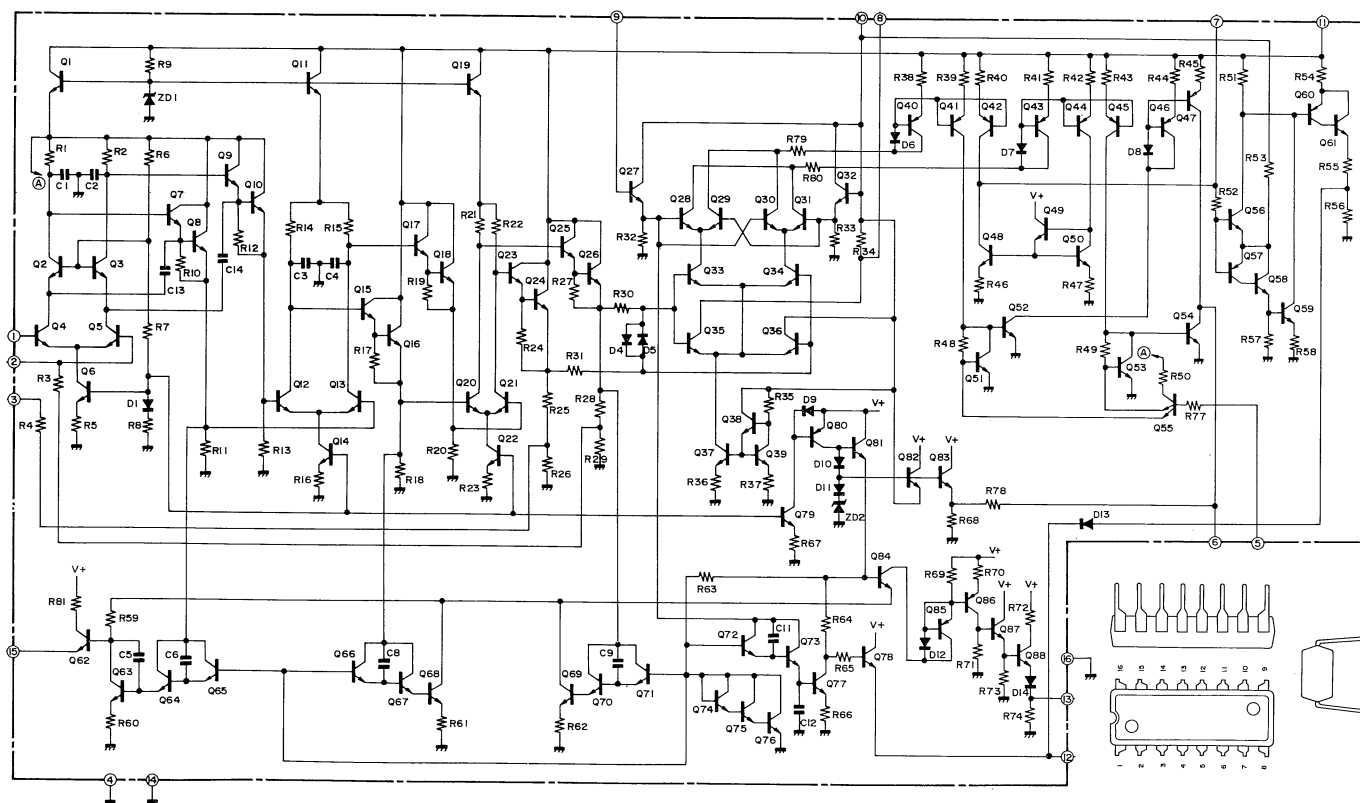
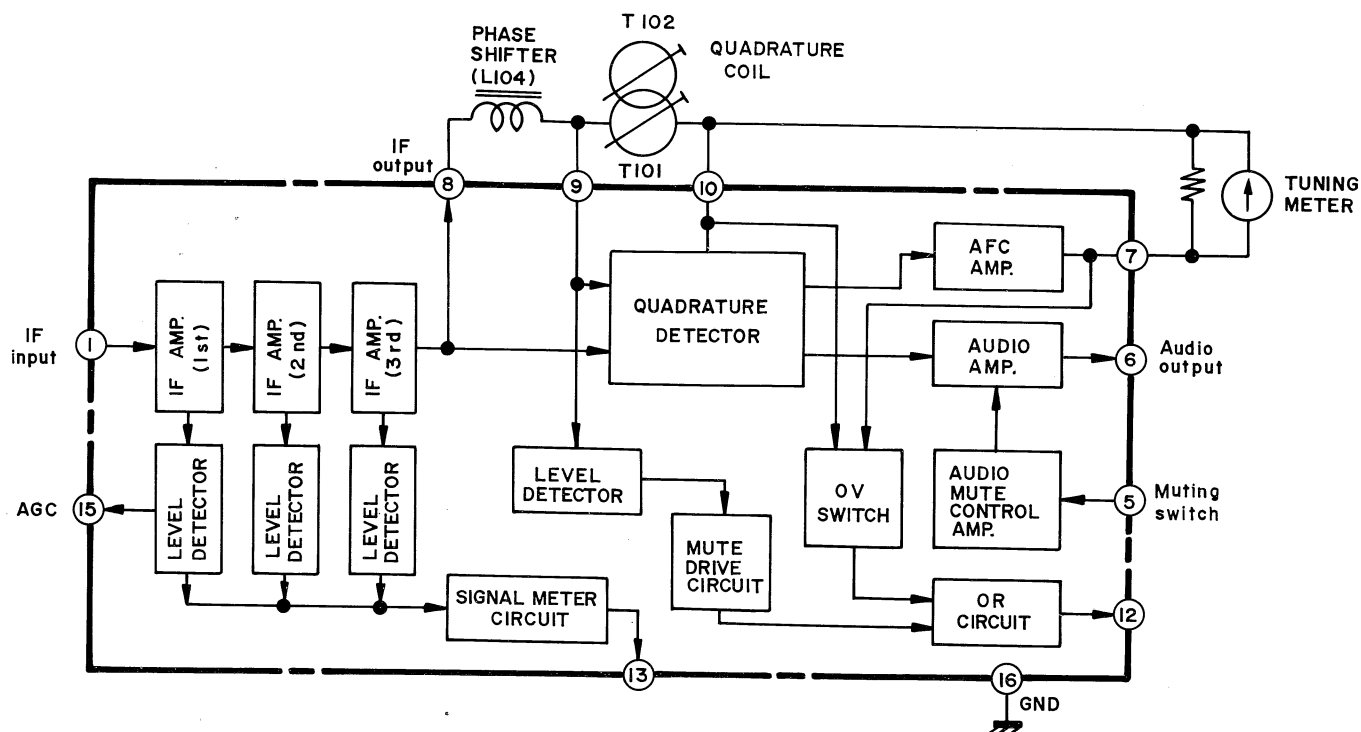


Figure 36 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC101)

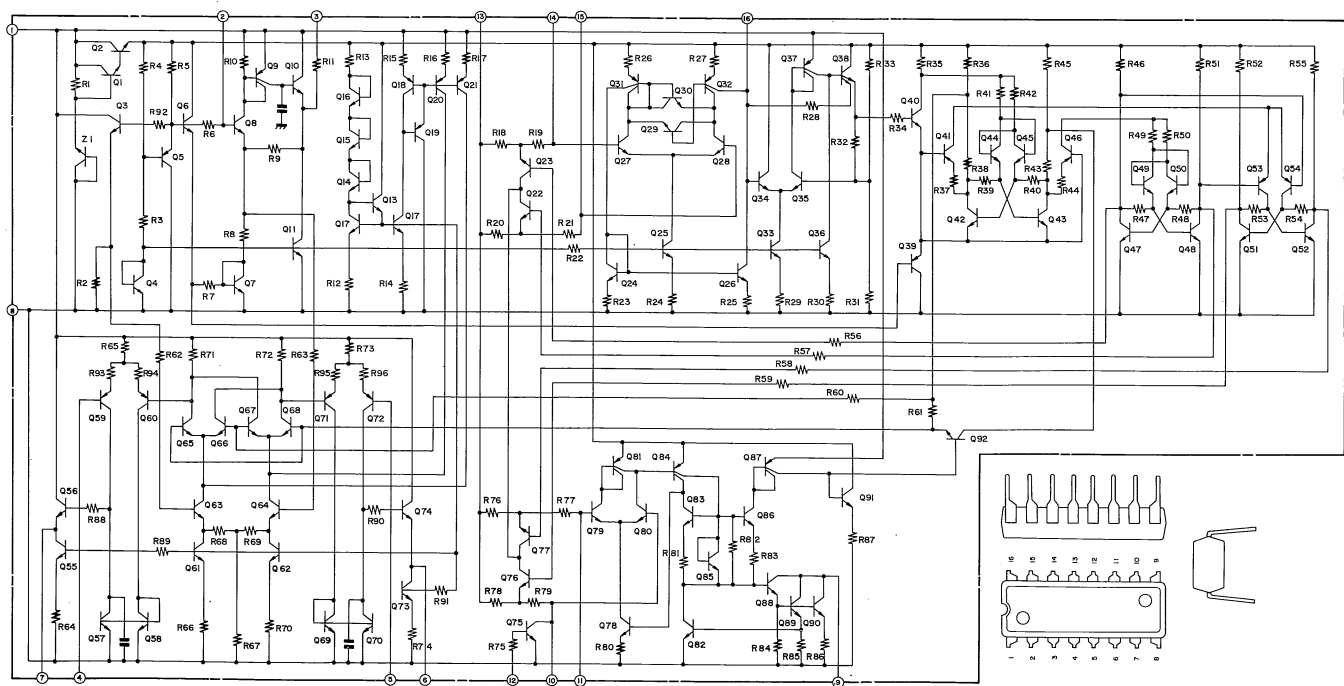
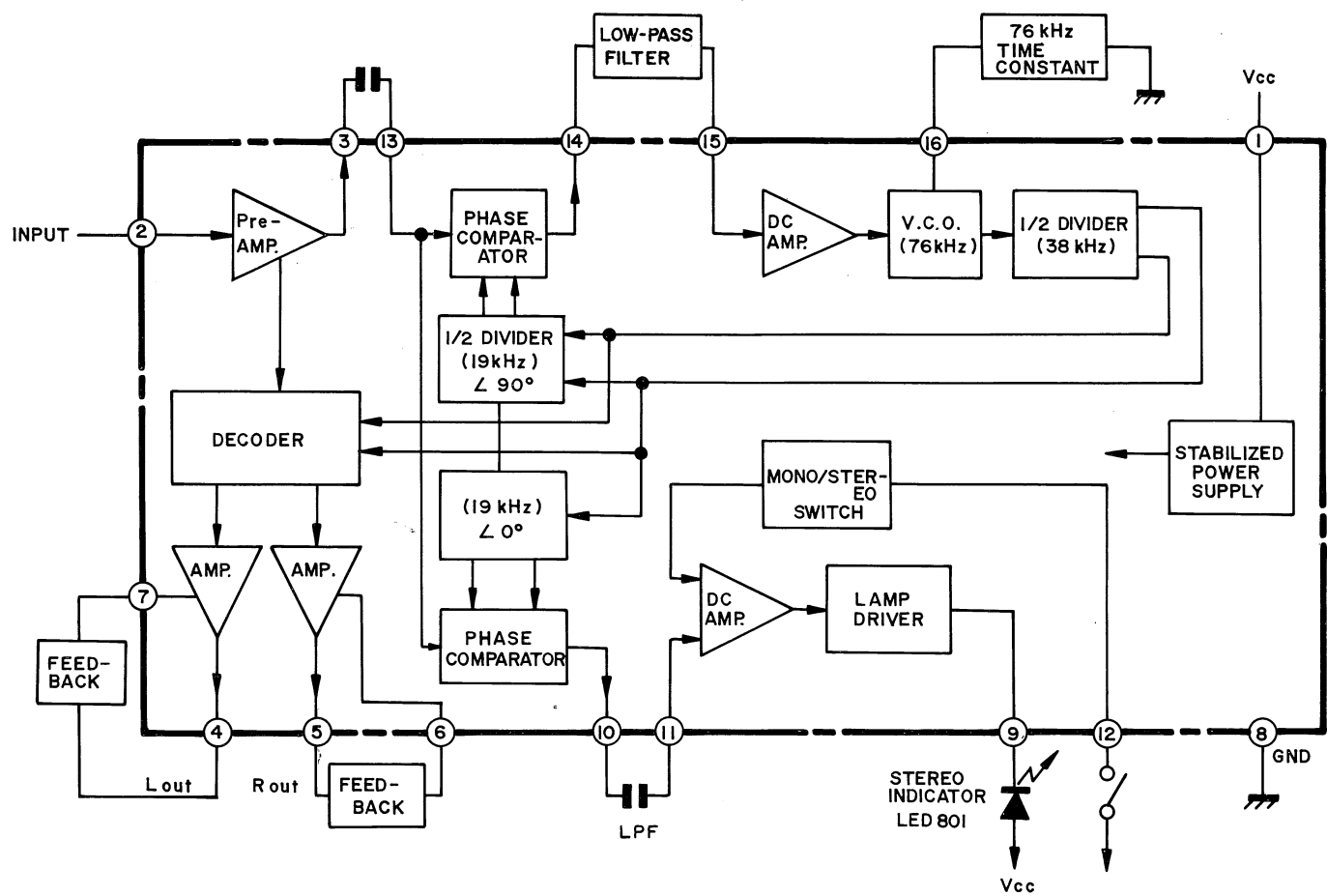


Figure 37 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC102)

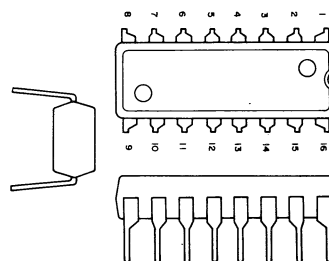
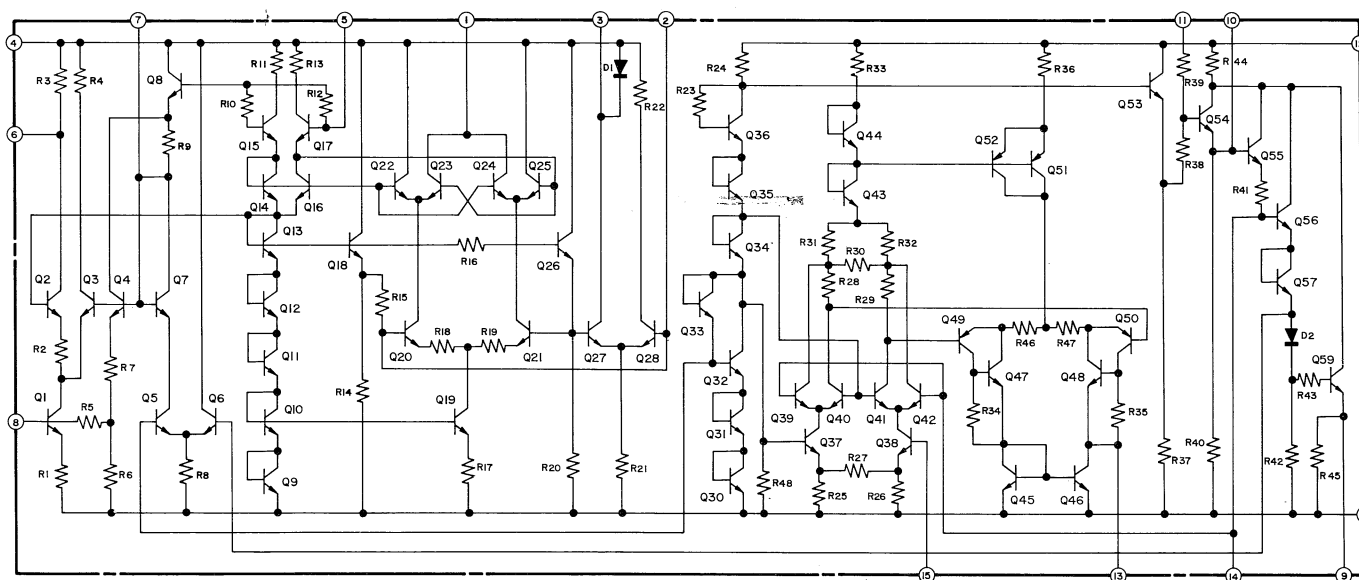
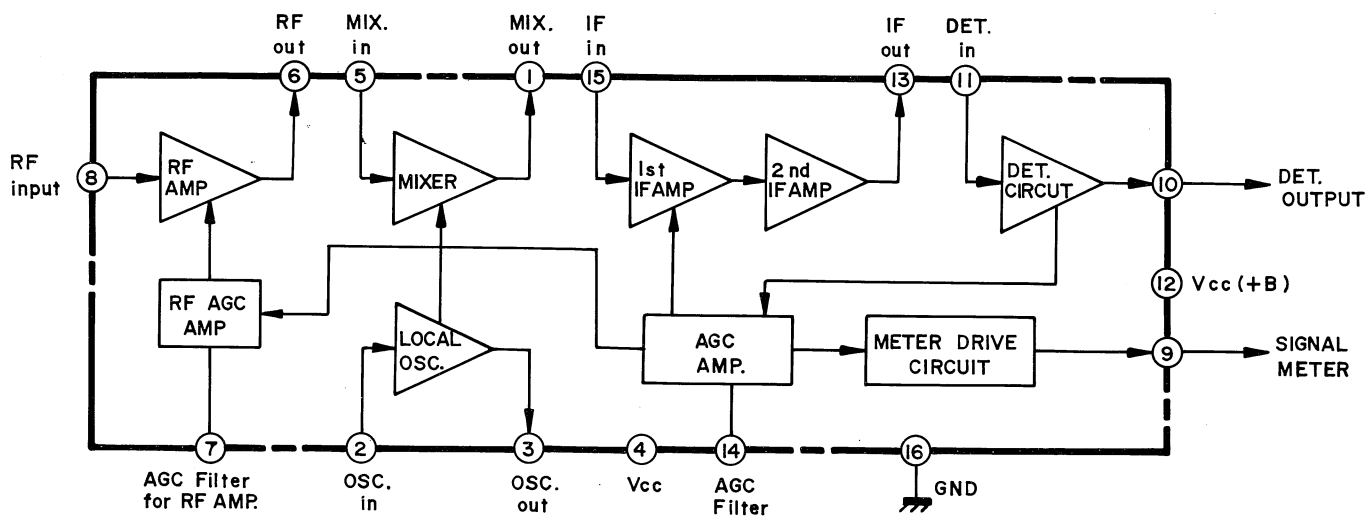


Figure 38 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC301)



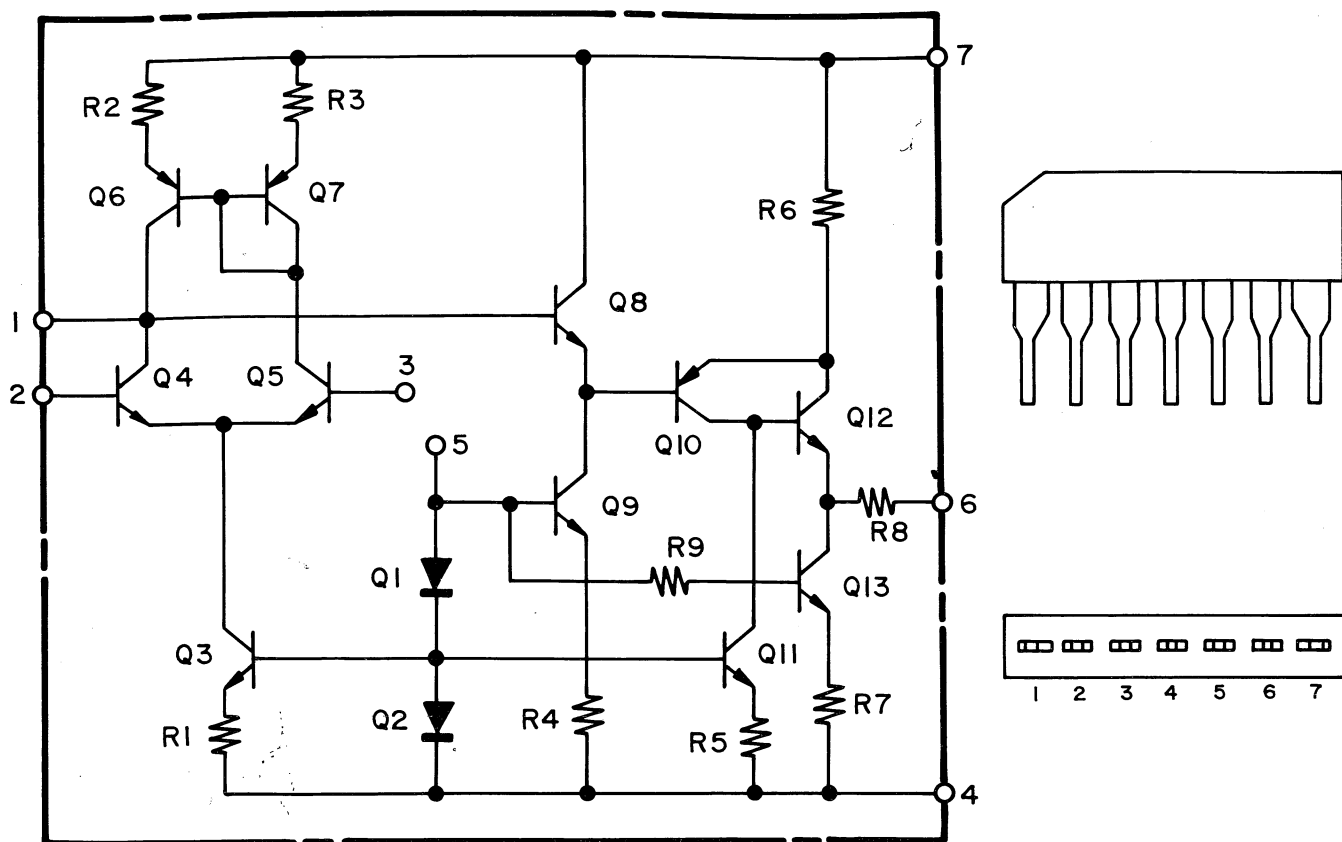
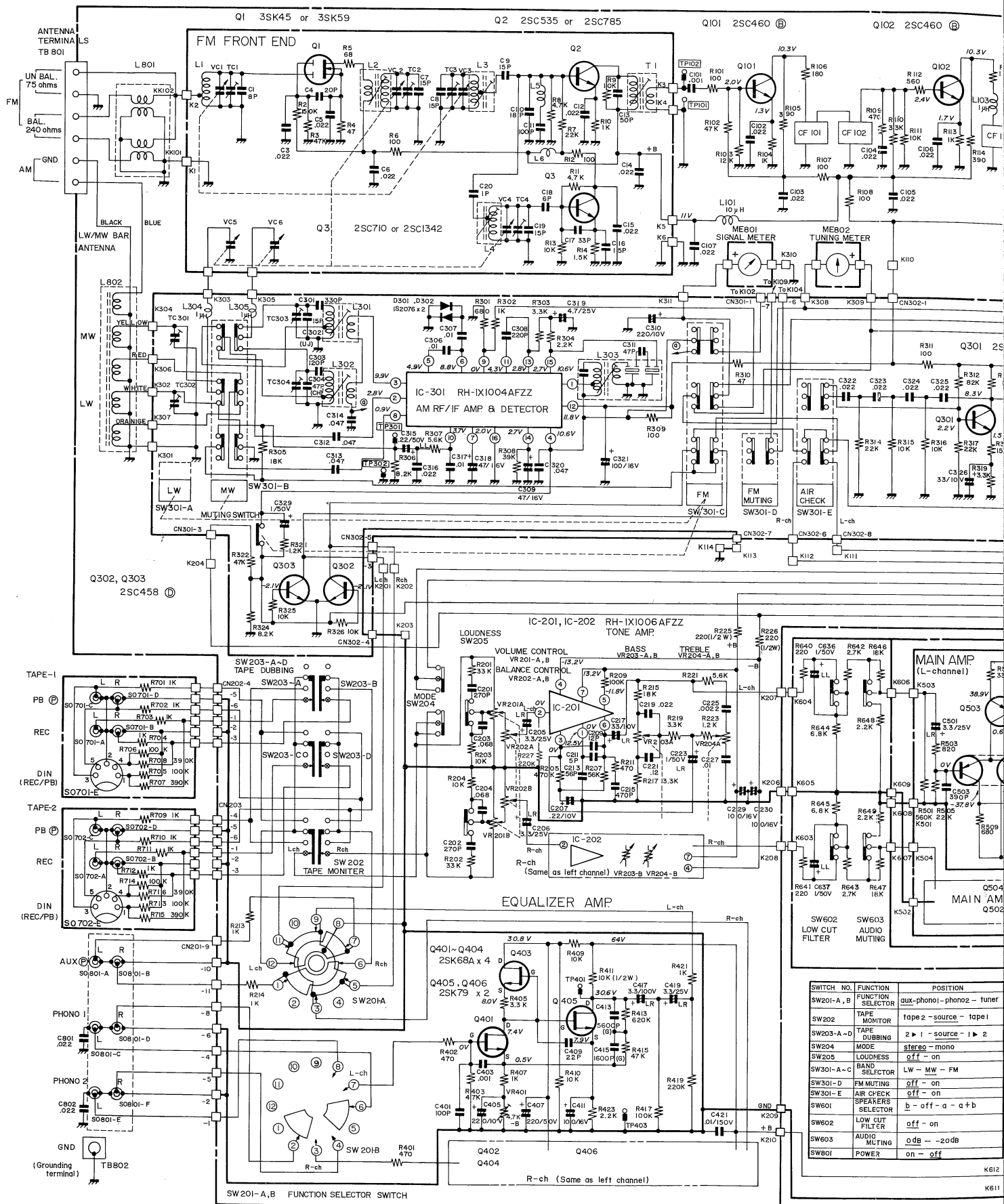


Figure 39 EQUIVALENT CIRCUIT OF INTEGRATED CIRCUIT (IC 201, IC 202 and IC 601)

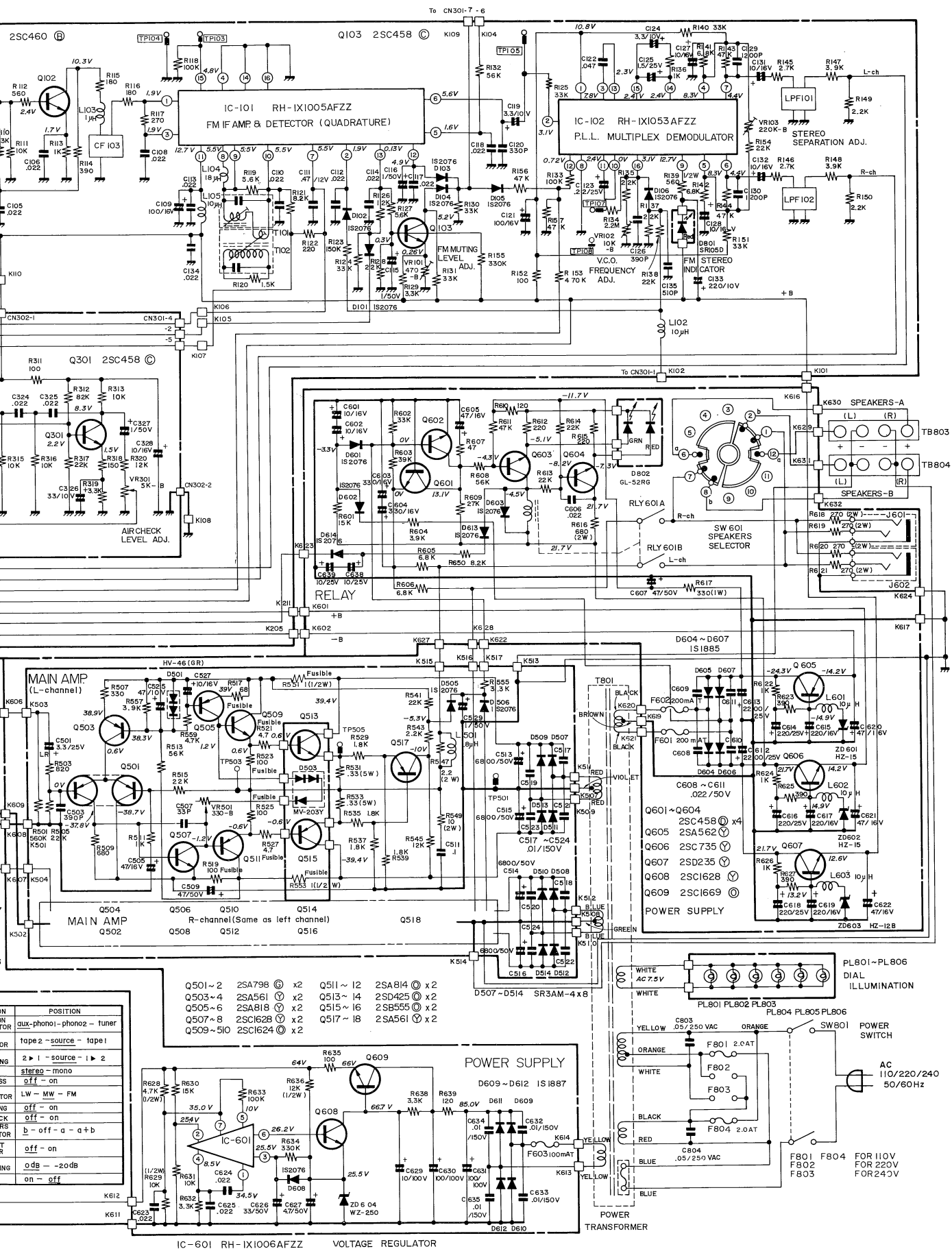
#### NOTES ON SCHEMATIC DIAGRAM

1. Frequency range: FM; 76.5 to 108 MHz  
MW; 520 to 1620 kHz  
LW; 150 to 370 kHz
2. IF: FM 10.7 MHz, MW/LW 455 kHz
3. Resistor: To differentiate the units of resistors, such symbols as K and M are used: the symbol K means  $K\Omega$  and the symbol M means  $M\Omega$  and the resistor without any symbol is  $\Omega$ -type resistor. Besides, the one with "Fusible" is a fuse type.
4. Capacitor: To indicate the unit of capacitor, a symbol P is used; this symbol P means pF and the unit of the capacitor without such symbol is  $\mu F$ . As to electrolytic capacitor, the expression "capacitance/withstand voltage" is used. The symbols LL and LR for the electrolytic capacitor respectively mean low-leak type.
5. SW 201: It is Function selector (aux./phono-1/phono-2/tuner) switch ("aux." position)
6. SW 202: It is Tape monitor (tape 2/source/tape 1) switch ("source" position)
7. SW 203: It is Tape dubbing (2  $\rightarrow$  1/source/1  $\rightarrow$  2) switch ("source" position)
8. SW 204: It is Mode (stereo/mono) switch ("stereo" position)
9. SW 205: It is Loudness (off/on) switch ("off" position)
10. SW 301-A ~ C (interlocked): It is Band selector (LW/MW/FM) switch ("MW" position)  
SW 301-D: It is FM muting switch ("off" position)  
SW 301-E: It is Air check switch ("off" position)
11. SW 601: It is Speakers selector (b/off/a/a+b) switch ("b" position)
12. SW 602: It is Low cut filter (off/on) switch ("off" position)
13. SW 603: It is Audio muting (0 dB/-20 dB) switch ("0dB" position)
14. SW 801: It is Power (on/off) switch ("off" position)
15. The indicated voltage in each section is the one measured by VTVM between such a section and the chassis with no signal being given.



(Specifications or wiring diagrams of this model are subject to change for the improvement without prior notice.)

Figure 40 SCHEMATIC DIAG

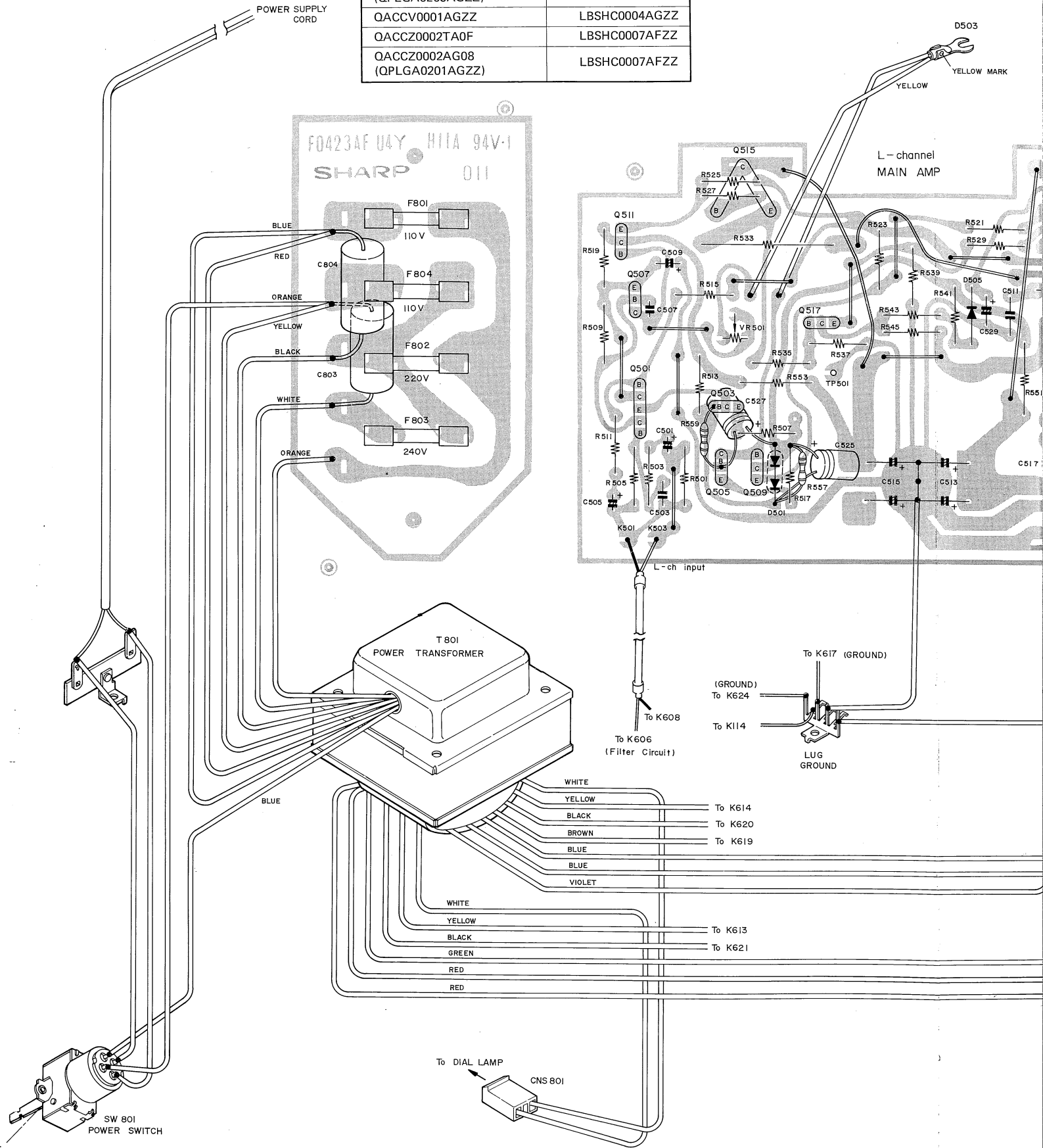


prior notice.)  
 EMATIC DIAGRAM





POWER SUPPLY CORD	BUSHING
QACCN0001AGZZ	LBSHC0004AGZZ
QACCS9001SE00 (QPLGA0205AGZZ)	LBSHC0007AFZZ
QACCV0001AGZZ	LBSHC0004AGZZ
QACCZ0002TA0F	LBSHC0007AFZZ
QACCZ0002AG08 (QPLGA0201AGZZ)	LBSHC0007AFZZ







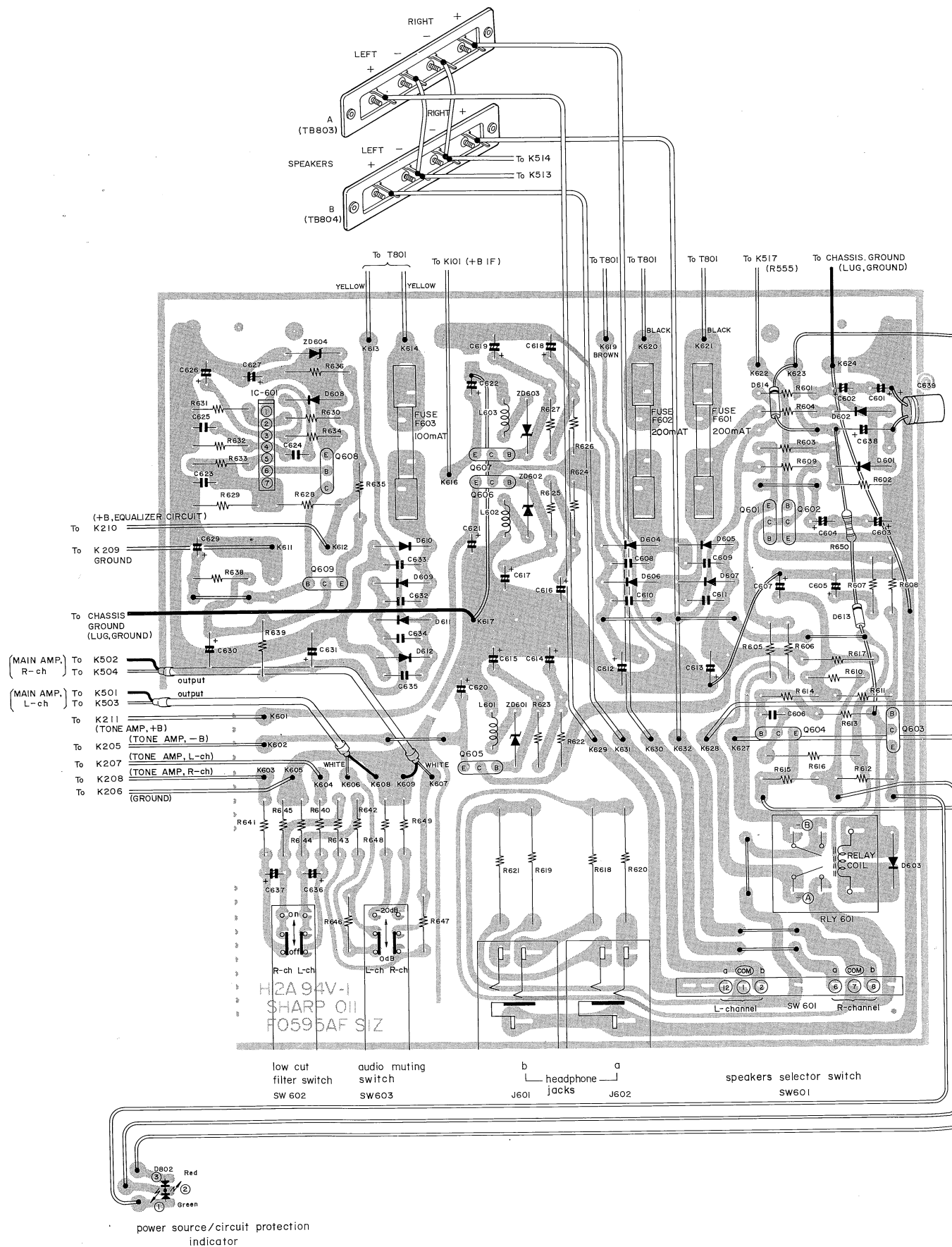


Figure 43 WIRING SIDE OF A





## POWER TRANSISTOR REPLACEMENT

If it is necessary to replace audio output transistors, then follow these procedures to prevent reoccurrence of transistor failure.

1. Carefully remove transistor and mica insulator and clean all the silicone grease off the mica and the mounting area on the chassis. If the mica is damaged, then it must be replaced.
2. Remove the defective transistor and clean out the transistor mounting hole.
3. Put new silicone grease on the transistor mounting area of the chassis and on both side of the mica insulator. Mount the new transistor, being careful to tighten each transistor mounting screw evenly. Driving one screw tightly and then the other is likely to cause metal filings which may damage the mica or prevent necessary heat dissipation on chassis.
4. Before applying power to the new transistor, with an ohm meter check to see that there is no short between the transistor case and chassis.
5. As transistor VS2SB555-O/-1 and VS2SD425-O/-1 are almost similar in the shape. So pay attention to the mark of transistor when replacing the power transistor.

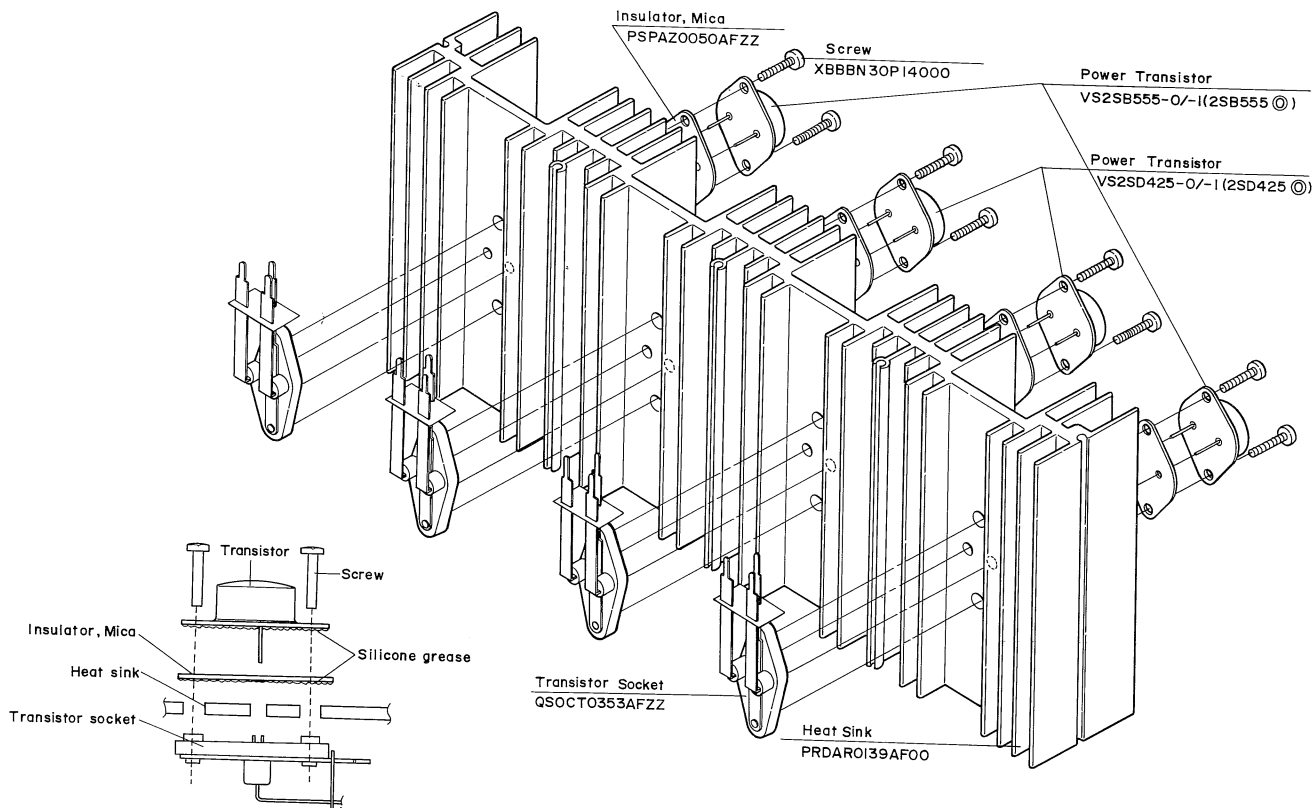
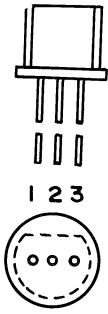
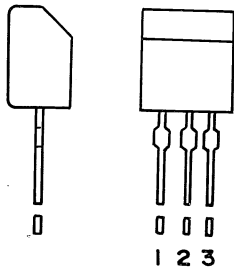


Figure 44 POWER TRANSISTOR REPLACEMENT



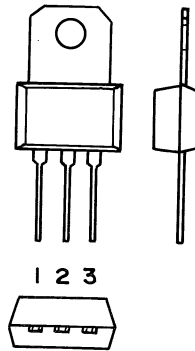
1. EMITTER
2. COLLECTOR
3. BASE

2SA562  
2SC735  
2SA561  
2SC785



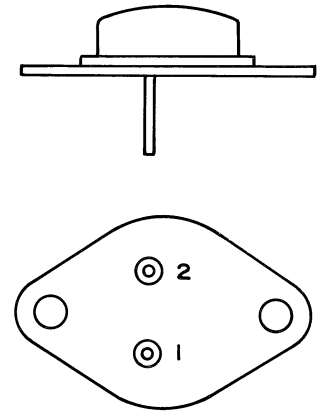
1. EMITTER
2. COLLECTOR
3. BASE

2SC460  
2SC458  
2SC535  
2SC1342



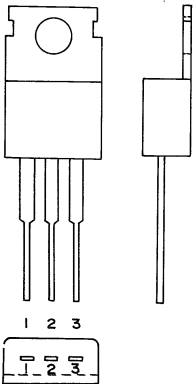
1. EMITTER
2. BASE
3. COLLECTOR

2SC1628  
2SA818



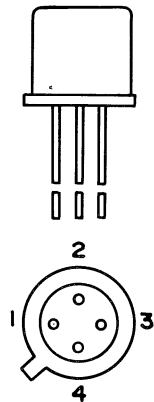
1. BASE
2. EMITTER  
COLLECTOR(CASE)

2SD425  
2SB555



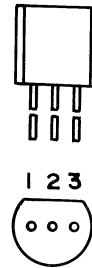
1. BASE
2. COLLECTOR (HEAT SINK)
3. EMITTER

2SC1624  
2SA814  
2SD235  
2SC1669



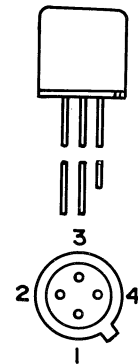
1. DRAIN
2. GATE 2
3. GATE 1
4. SOURCE (CASE)

3SK59



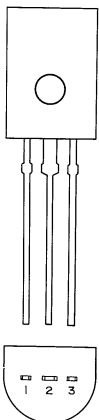
1. DRAIN
2. GATE
3. SOURCE

2SK68A



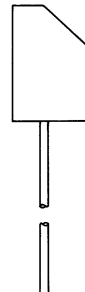
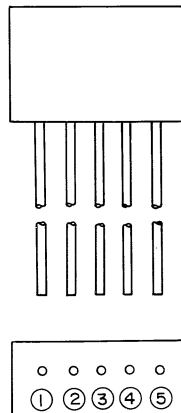
1. DRAIN
2. GATE 2
3. GATE 1
4. SOURCE (CASE)

2SK45



1. SOURCE
2. DRAIN
3. GATE

2SK79



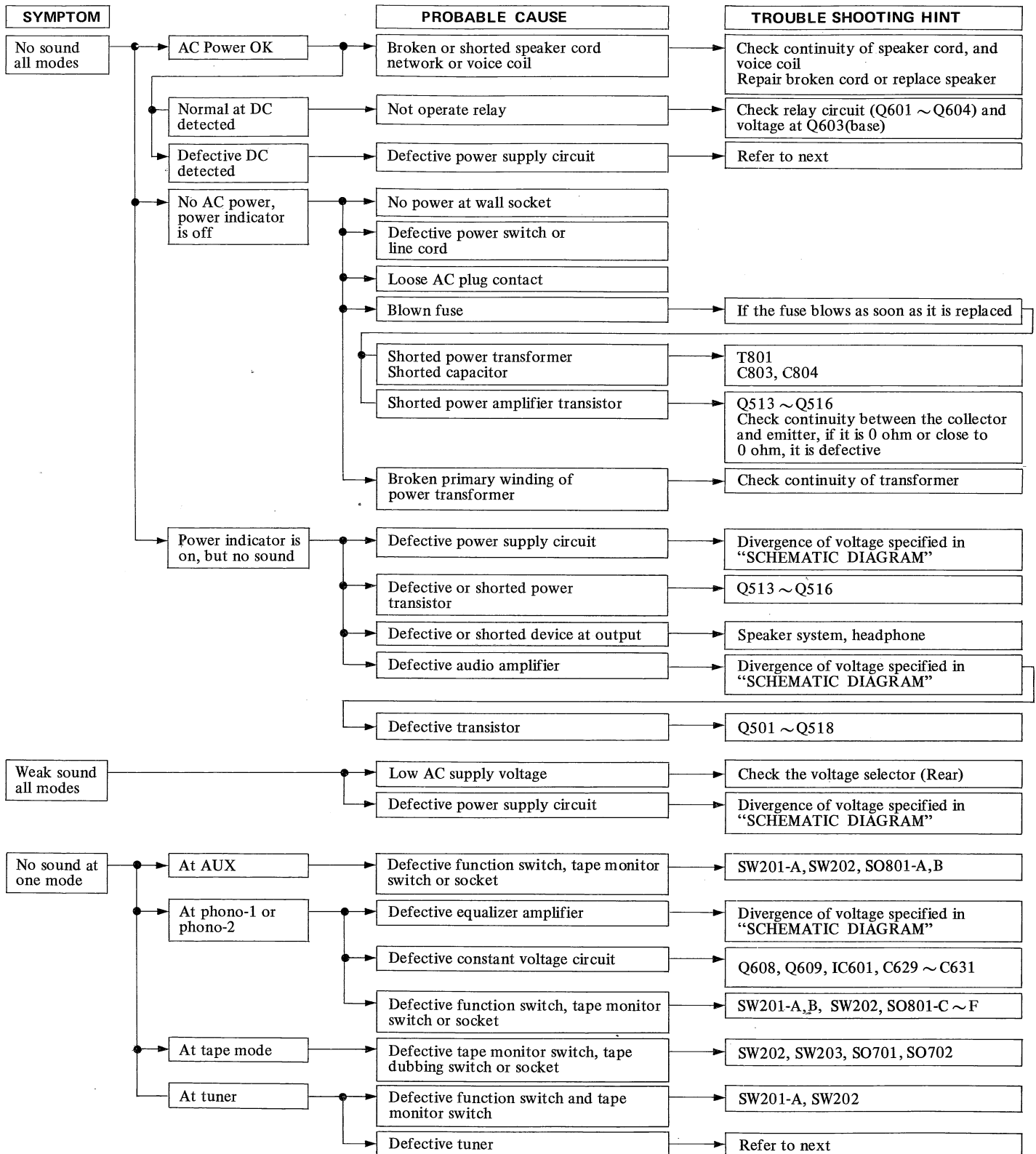
- ① BASE 1
- ② COLLECTOR 1
- ③ EMITTER
- ④ COLLECTOR 2
- ⑤ BASE 2

2SA798

Figure 45 TRANSISTOR TYPES

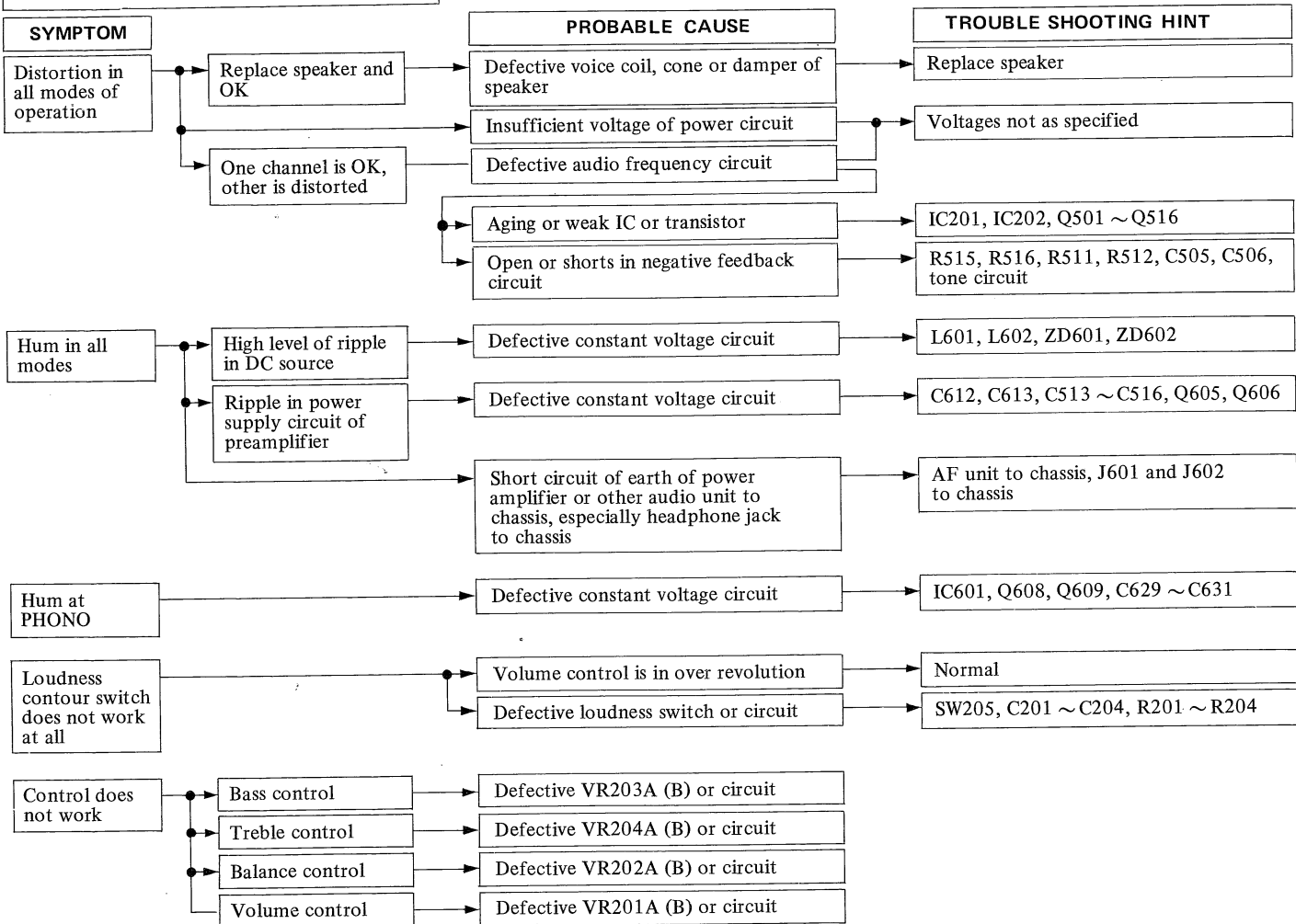
## TROUBLE SHOOTING GUIDE

### ALL OPERATIONAL MODES (1)



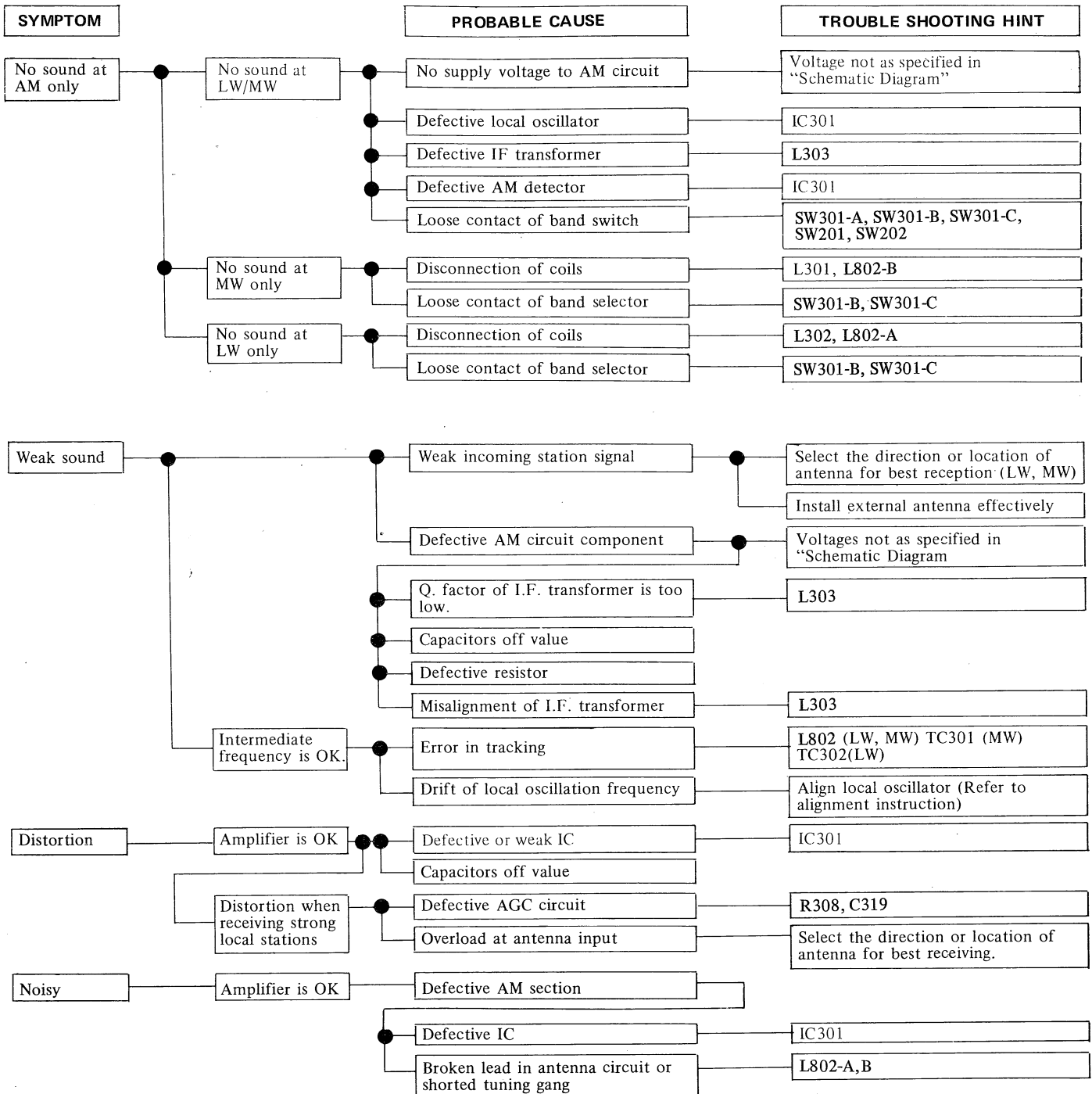
# TROUBLE SHOOTING GUIDE

## ALL OPERATIONAL MODES (2)



# TROUBLE SHOOTING GUIDE

## AM RECEPTION



# TROUBLE SHOOTING GUIDE

## FM RECEPTION

SYMPTOM		PROBABLE CAUSE	TROUBLE SHOOTING HINT
No sound in FM position	No sound in AM position, also	Defective power supply of IF stage	Voltage not as specified in "Schematic Diagram"
	FM detected signal is OK at TP105	Defective FM multiplex stage	Refer to the guide for FM multiplex reception
	Weak or no voltage of FM power supply	Open or defective circuit from power supply to FM tuner	Check continuously between tuner and power supply
		Poor contact of selector switch	SW201, SW202, SW301-D and E
	FM power supply is OK.	Defective FM IF circuit	
		Low voltage in IF circuit	
		Weak IC	IC101, IC102
		Defective ceramic filter	CF101, CF102, CF103
		Defective IF transformer	T1, T101, T102
		Defective resistors and capacitors	
	FM IF is OK	Defective FM tune circuit	FM front-end circuit
		Defective power supply circuit to FM front end	Voltage not as specified in "Schematic Diagram"
No signal but sufficient background noise	Not tune in FM range	Local oscillator dead	Q3, L4, TC4, C18
Weak signal but loud background noise		Weak station signal	Use more sensitive antenna
		Loose antenna connection	
		Open antenna circuit	
		Weak RF circuit	FM front-end
		Misadjustment of tracking or IF transformers	Realign following the alignment chart
Distortion in FM		Defective IF stage or low voltage in IF stage	Measure voltages in FM section and repair or replace defective part
		Misalignment	T101, T102, T1
		Weak integrated circuit	IC101, IC102
Hum	Ripple in FM power supply	Capacitor off value	C612, C619, C622, C618, C109
Noisy		Defective FM IF stage or FM tuner	Voltage not as specified in "Schematic Diagram"
		Aging or weak IC	IC101, IC102
Dial calibration off	Pointer does not move smoothly.	Pointer off of track or hits obstruction	
	Pointer runs over dial scale.	Pointer does not start at zero point of dial	Mechanically rese pointer at zero

## TROUBLE SHOOTING GUIDE

### FM MULTIPLEX RECEPTION

SYMPTOM		PROBABLE CAUSE	TROUBLE SHOOTING HINT
No stereo separation	Stereo light operates normally.	Components in one channel physically touching parts for other channel in tone circuit, main amp. or multiplex circuit	SW301-C and E, SW201, SW202, SW204, SW602, SW603, SW601
	Stereo light does not light when receiving stereo signal.	Aging or weak IC	IC102
		Aging or weak semi-fixed resistor	VR103
		Defective resistors and capacitors	
Distortion		Weak or Defective IC	IC102
Poor separation	Stereo light does not operate.	Defective IC	IC102
	Stereo light operates normally.	Drift of VCO frequency	Realign following the alignment chart VR102
Stereo light does not operate	Multiplex amplifier checks OK	Defective indicator lamp	D801
		Defective power circuit to stereo light	R139

### USING WITH EXTERNAL INPUTS OR OUTPUTS (TAPE, ETC.)

SYMPTOM		PROBABLE CAUSE	TROUBLE SHOOTING HINT
No sound	Unit operates properly on AM or FM	Input source defective	Switch input sources to check
		Loose contacts of input socket	SO701, SO702
		Broken lead between printed wiring board and terminals	Check and repair
Tape play does not work	Amplifier is OK	Tape recorder defective	
		Loose contacts of output socket	SO701

### OTHER TROUBLES

Signal meter does not operate	At FM and AM	Meter open	
		Weak or defective IC and diodes	IC102, IC301, D101, SW301-C
	At only AM	Defective AM circuit	Refer to AM reception
Tuning meter does not operate	At FM	Meter open	
		Weak or defective IC	IC101, SW301-C
Air check circuit does not operate The air check circuit does not function.	At FM	Defective air check/multipath switch	SW301-E
		Defective air check oscillator circuit	Q301, R314, R315, R316, C322, C323, C324, C325



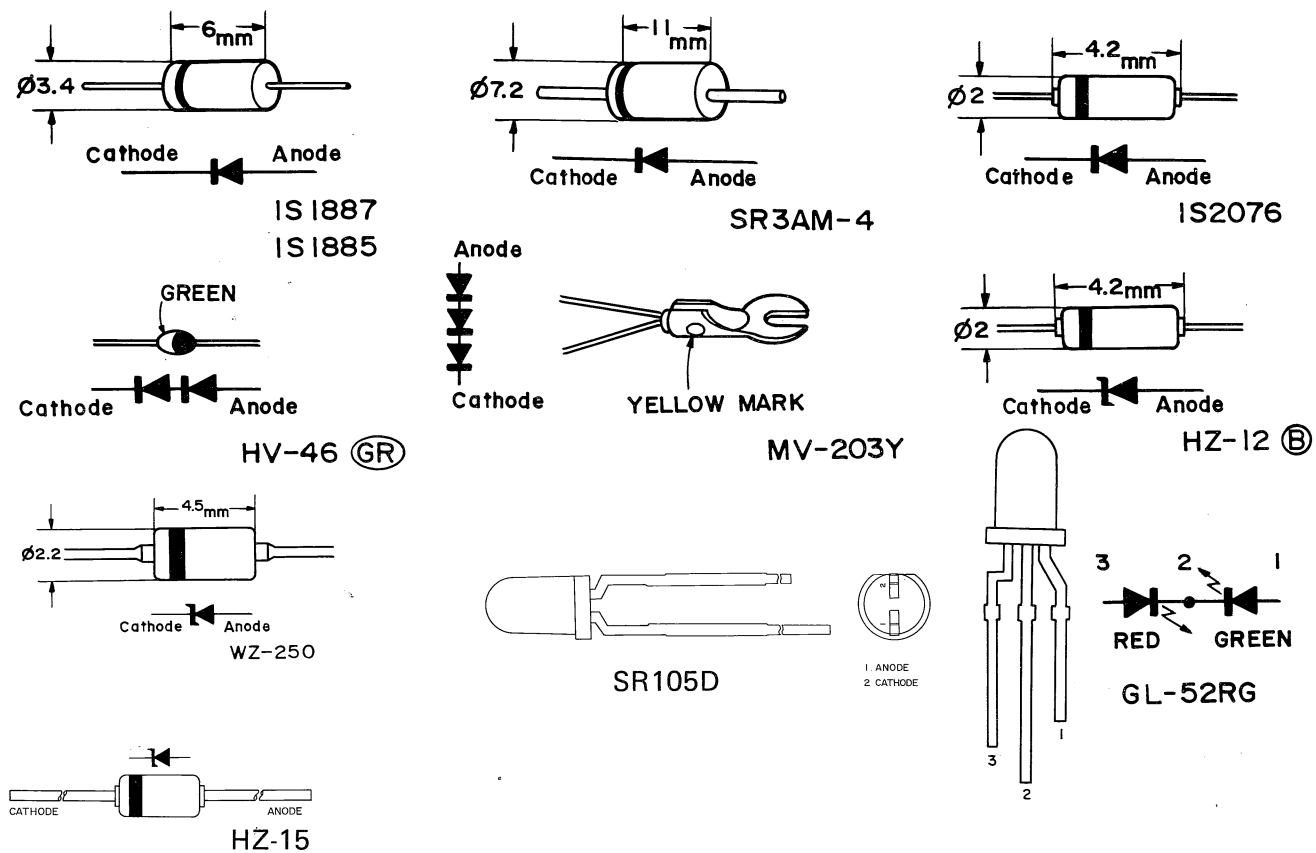


Figure 46 DIODE TYPES

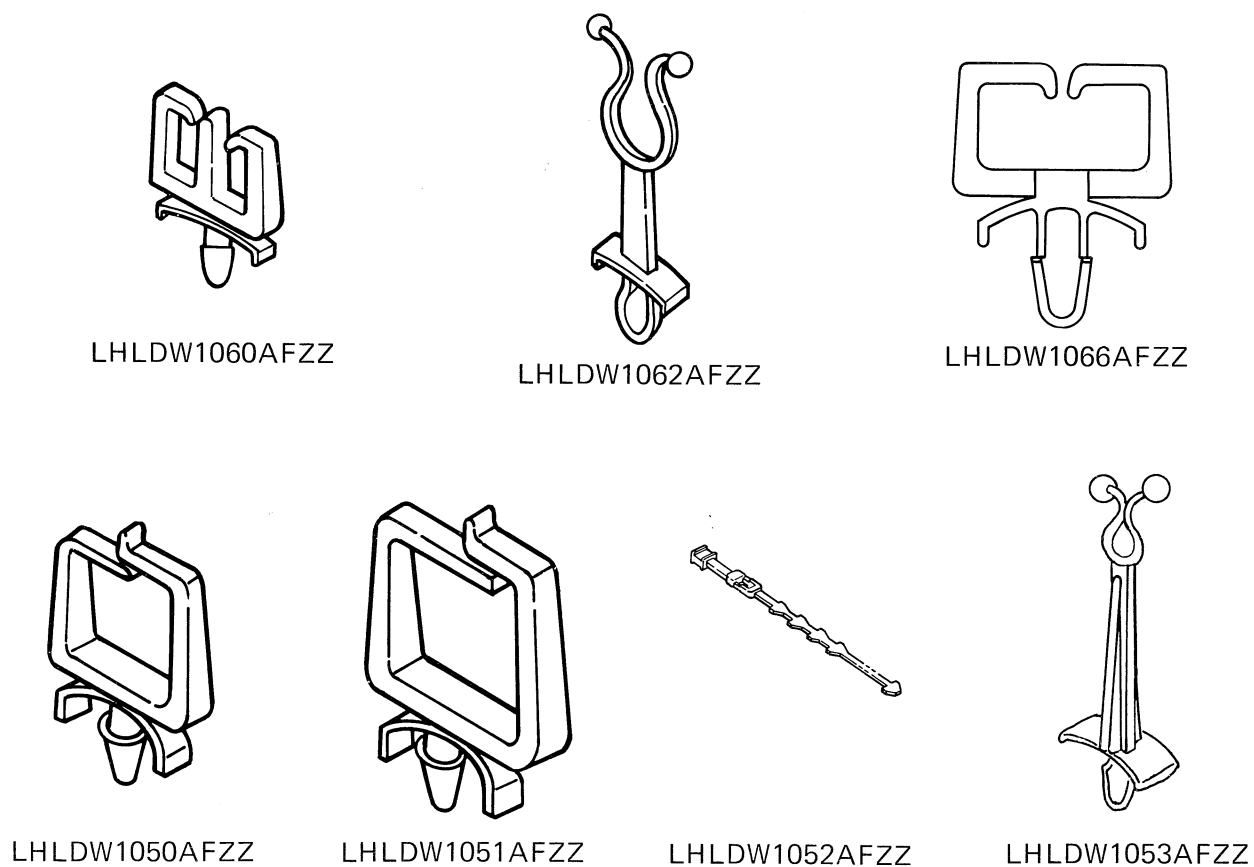


Figure 47 WIRE CLIP

# REPLACEMENT PARTS LIST

## "HOW TO ORDER REPLACEMENT PARTS"

To have your order filled promptly and correctly, please furnish the following informations.

1. MODEL NUMBER
2. REF. NO.
3. PART NO.
4. DESCRIPTION

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
<b>INTEGRATED CIRCUITS</b>				Q604	VS2SC458-D/-1	Protection Circuit, Switching (2SC458 (D))	AE
IC101	RH-IX1005AFZZ	FM IF Amplifier and Detector (Quadrature) (HA1137W)	AT	Q605	VS2SA562-Y/-1	Voltage Regulator, Ripple Filter (2SA562 (Y))	AF
IC102	RH-IX1053AFZZ	P.L.L. Multiplex Stereo Demodulator (HA1196)	AP	Q606	VS2SC735-Y/-1	Voltage Regulator Ripple Filter (2SC735 (Y))	AF
IC201, IC202	RH-IX1006AFZZ	Tone Amplifier (TA7136P)	AH	Q607	VS2SD235-Y/-1	Voltage Regulator, Ripple Filter (2SD235 (Y))	AG
IC301	RH-IX1004AFZZ	AM RF/IF Amplifier and Detector (HA1138)	AS	Q608	VS2SC1628-Y-1	Voltage Regulator, Equalizer Circuit (2SC1628 (Y))	AH
IC601	RH-IX1006AFZZ	Voltage Regulator, Equalizer Circuit (TA7136P)	AH	Q609	VS2SC1669-O-1	Voltage Regulator, Equalizer Circuit (2SC1669 (O))	AL
<b>TRANSISTORS</b>				<b>DIODES</b>			
Q101	VS2SC460-B/-1	FM IF Amplifier (2SC460 (B))	AE	D101	VHD1S2076//-1	Signal Meter (1S2076)	AB
Q102	VS2SC460-B/-1	FM IF Amplifier (2SC460 (B))	AE	D102	VHD1S2076//-1	Voltage Detector (1S2076)	
Q103	VS2SC458-C/-1	FM Muting Amplifier (2SC458 (C))	AE	D103	VHD1S2076//-1	FM Muting (1S2076)	
Q301	VS2SC458-C/-1	Air Check Oscillation (2SC458 (C))	AE	D104	VHD1S2076//-1	FM Muting (1S2076)	
Q302	VS2SC458-D/-1	Muting (2SC458 (D))	AE	D105	VHD1S2076//-1	FM Muting (1S2076)	
Q303	VS2SC458-D/-1	Muting (2SC458 (D))	AE	D106	VHD1S2076//-1	V.C.O. Stop (1S2076)	AD
Q401, Q402	VS2SK68A///1F	FET, Equalizer Amplifier (2SK68A)	AF	D301	VHD1S2076//-1	Overload (1S2076)	
Q403, Q404	VS2SK68A///1F	FET, Equalizer Amplifier (2SK68A)	AF	D302	VHD1S2076//-1	Overload (1S2076)	AD
Q405, Q406	VS2SK79///1F	V-FET, Equalizer Amplifier (2SK79)	AM	D501, D502	VHVHV46-G//-1	Varistor, Bias Stabilizer (HV-46 (GR))	
Q501, Q502	VS2SA798-G/-1	Dual Transistor, Differential Amplifier (2SA798 (G))	AF	D503, D504	VHVMV203Y//-1	Varistor, Bias Circuit (Idle Current) (MV-203 (Y))	AD
Q503, Q504	VS2SA561-Y/-1	Constant Current Circuit (2SA561 (Y))	AF	D505, D506	VHD1S2076//-1	Voltage Detector (1S2076)	AB
Q505, Q506	VS2SA818-Y/-1	Constant Current Circuit (2SA818 (Y))	AH	D507, D508, D509, D510, D511, D512, D513, D514	VHDSR3AM-4/-1	Power Rectifier, Main Amplifier (SR3AM-4)	AF
Q507, Q508	VS2SC1628-Y-1	Audio Amplifier, Class "A" (2SC1628 (Y))	AH	D601	VHD1S2076//-1	Voltage Detector, Protection Circuit (1S2076)	AB
Q509, Q510	VS2SC1624-O-1	Drive Amplifier (2SC1624 (O))	AF	D602	VHD1S2076//-1	Rectifier (1S2076)	AB
Q511, Q512	VS2SA814-O/-1	Drive Amplifier (2SA814 (O))		D603	VHD1S2076//-1	Surge Current Provention (1S2076)	AB
Q513, Q514	VS2SD425-O/-1	Power Amplifier (2SD425 (O))		D604, D605, D606, D607	VHD1S1885//-1	Power Rectifier (1S1885)	AC
Q515, Q516	VS2SB555-O/-1	Power Amplifier (2SB555 (O))		D608	VHD1S2076//-1	Voltage Detector (1S2076)	AB
Q517, Q518	VS2SA561-Y/-1	Voltage Detector, Protection Circuit (2SA561 (Y))		D609, D610, D611, D612	VHD1S1887//-1	Power Rectifier, Equalizer Circuit (1S1887)	AC
Q601	VS2SC458-D/-1	Protection Circuit, Voltage Detector (2SC458 (D))	AE	D613	VHD1S2076//-1	Noise Prevention (1S2076)	AB
Q602	VS2SC458-D/-1	Protection Circuit, Voltage Detector (2SC458 (D))	AE	D614	VHD1S2076//-1	Noise Prevention (1S2076)	AB
Q603	VS2SC458-D/-1	Protection Circuit, Switching (2SC458 (D))	AE				

# PARTS LIST

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
ZD601	VHEHZ15///-1	Zener Diode, Voltage Regulator (13.9 ~ 15.6V) (HZ-15)	AC	VR102	RVR-M0078AGZZ	10K(B) ohm, V.C.O. Frequency Adjust	AF
ZD602	VHEHZ15///-1	Zener Diode, Voltage Regulator (13.9 ~ 15.6V) (HZ-15)	AC	VR103	RVR-M0145AFZZ	220K(B) ohm, Stereo Separation Adjust	AD
ZD603	VHEHZ12-BBK-1	Zener Diode, Voltage Regulator (12.7 ~ 13.5V) (HZ-12 (B))	AD	VR201- A, B	RVR-B0148AFZZ	100K ohm, Volume Control	AM
ZD604	VHEWZ250///-1	Zener Diode, Voltage Regulator (23.8 ~ 26.2V) (WZ-250)	AD	VR202- A, B	RVR-G0052AFZZ	100K ohm, Balance Control	AK
D801	VHPSR105D//1	Light Emitting Diode, Stereo Indicator (SR105D)	AD	VR203- A, B	RVR-C0066AFZZ	100K ohm, Bass Control	AL
D802	VHPGL-52RG/1F	Light Emitting Diode, Power Source/Circuit Protection Indicator (GL-52RG)	AH	VR204- A, B	RVR-C0066AFZZ	100K ohm, Treble Control	AL
<b>COILS</b>				VR301	RVR-M0126AFZZ	5K(B) ohm, Air Check Level Adjust	AC
L101	VP-LH100M0000	10μH, +B Choke	AB	VR401, VR402	RVR-M0065AGZZ	4.7K(B) ohm, Equalizer Circuit	AF
L102	VP-LH100M0000	10μH, +B Choke		VR501, VR502	RVR-M0139AFZZ	330(B) ohm, Idle Current Adjust	AD
L103	VP-LH1R0M0000	1μH, Phase Compensation		<b>ELECTROLYTIC CAPACITORS</b>			
L104	RCILZ0052AFZZ	18μH, Phase Shifter		C109	VCEAAU1CW107Y	100μF, 16V, +50 -10%	AC
L105	VP-LH100M0000	10μH, +B Choke	AD	C115	VCEAAU1HW105A	1μF, 50V, +75 -10%	AB
L301	RCILB0395AFZZ	MW Oscillator		C116	VCEAAU1HW105A	1μF, 50V, +75 -10%	AB
L302	RCILB0411AFZZ	LW Oscillator		C119	VCAAAU1AB335M	3.3μF, 10V, ±20%, Aluminum	AD
L303	RCILI0209AFZZ	AM IF with Ceramic Filter		C121	VCEAAU1CW107Y	100μF, 16V, +50 -10%	AC
L304	VP-LH1R0M0000	1μH, Choke	AB	C123	VCAAAU1EB224K	.22μF, 25V, ±10%, Aluminum	AC
L305	VP-LH1R0M0000	1μH, Choke	AB	C124	VCAAAU1AB335M	3.3μF, 10V, ±20%, Aluminum	AD
L501, L502	RCILZ0050AFZZ	.8μH, Oscillation Prevention	AC	C125	VCAAAU1EB155K	1.5μF, 25V, ±10%, Aluminum	AC
L601, L602, L603	VP-LH100M0000	10μH, Choke	AB	C127	VCEAAU1CW106Y	10μF, 16V, +50 -10%	AB
L801	RCILA0231AFZZ	Balun (Antenna Matching)	AC	C128	VCEAAU1CW106Y	10μF, 16V, +50 -10%	AB
L802- A, B	RCILA0403AFZZ	LW/MW Bar Antenna	AS	C131, C132	VCEAAU1CW106Y	10μF, 16V, +50 -10%	AB
<b>TRANSFORMERS</b>				C133	VCEAAU1AW227Y	220μF, 10V, +50 -10%	AC
T101	RCILD0053AFZZ	Quadrature (10.7MHz)	AE	C205, C206	VCEALU1EC335A	3.3μF, 25V, +75 -10%, LR (Orange)	AC
T102	RCILD0054AFZZ	Quadrature (10.7MHz)	AE	C207, C208	VCAAAU1AB224M	.22μF, 10V, ±20%, Aluminum	AC
T801, CNS801	RTRNP0474AFZZ	Power with Connecting Socket	BR	C217, C218	VCEALU1AC336Y	33μF, 10V, +50 -10%, LR (Orange)	AC
<b>FILTERS</b>				C223, C224	VCEALU1HC105A	1μF, 50V, +75 -10%, LR (Orange)	AC
CF101, CF102, CF103	RFILF0001AGZZ	FM IF, Ceramic	AF	C229, C230	VCEAAU1CW107Y	100μF, 16V, +50 -10%	AC
LPF101, LPF102	RFILL0050AFZZ	Low Pass Filter	AK	C309	VCEAAU1CW476Y	47μF, 16V +50 -10%	AB
<b>CONTROLS</b>				C310	VCEAAU1AW227Y	220μF, 10V, +50 -10%	AC
TC301, TC302	RTO-H2033AGZZ	Trimmer Capacitors TC301: MW Antenna Trimmer TC302: LW Antenna Trimmer	AD	C315	VCEALU1HW224M	.22μF, 50V, ±20%, LL (Yellow)	AB
TC303, TC304	RTO-H2051AFZZ	Trimmer Capacitors TC303: MW Oscillator Trimmer TC304: LW Oscillator Trimmer	AE	C318	VCEAAU1CW476Y	47μF, 16V, +50 -10%	AB
VR101	RVR-M0140AFZZ	470(B) ohm, FM Muting Level Adjust	AD	C319	VCEAAU1EW475A	4.7μF, 25V, +75 -10%	AB
				C321	VCEAAU1CW107Y	100μF, 16V, +50 -10%	AC
				C326	VCEAAU1AW336Y	33μF, 10V, +50 -10%	AB
				C327	VCEAAU1HW105A	1μF, 50V, +75 -10%	AB
				C328	VCEAAU1CW106Y	10μF, 16V, +50 -10%	AB
				C329	VCEAAU1HW105A	1μF, 50V, +75 -10%	AB
				C405, C406	VCEAAU1AW227Y	220μF, 10V, +50 -10%	AC
				C407	VCEAAU1HW227Y	220μF, 50V, +50 -10%	AD
				C411, C412	VCEAAU1CW107Y	100μF, 16V, +50 -10%	AC
				C417, C418	VCEALU2AC335A	3.3μF, 100V, +75 -10%, LR (Orange)	AD
				C419, C420	VCEALU1EC335A	3.3μF, 25V +75 -10%, LR (Orange)	AC

# PARTS LIST

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
C501,	VCEALU1EC335A	3.3 $\mu$ F, 25V, +75 -10%, LR (Orange)	AC	C130	VCQSMT1HS122J	1200pF, 50V, $\pm$ 5%, Styrol	AB
C502				C134	VCKZPU1HF223Z	.022 $\mu$ F	AA
C505,	VCEAAU1CW476Y	47 $\mu$ F, 16V, +50 -10%	AB	C135	VCCSPU1HL511J	510pF, 50V, $\pm$ 5%, Ceramic	AA
C506				C201,	VCCSPU1HL271K	270pF, 50V, $\pm$ 10%, Ceramic	AB
C509,	VCEAAU1HW476Y	47 $\mu$ F, 50V, +50 -10%	AC	C202			
C510				C203,	VCQYKU1HM683J	.068 $\mu$ F, 50V, $\pm$ 5%, Mylar	AC
C513,	RC-EZ1008AFZZ	6800 $\mu$ F $\times$ 2, 50V, +50 -10% (Dual Capacitor)	AZ	C204			
C515				C209,	VCCSPU1HL120K	12pF, 50V, $\pm$ 10%, Ceramic	AA
C514,	RC-EZ1008AFZZ	6800 $\mu$ F $\times$ 2, 50V, +50 -10% (Dual Capacitor)	AZ	C210			
C516				C211,	VCCSPU1HL5R0C	5pF, 50V, $\pm$ 0.25pF, Ceramic	AA
C525,	VCEAAU1AW476Y	47 $\mu$ F, 10V, +50 -10%	AB	C212			
C526				C213,	VCCSPU1HL560K	56pF, 50V, $\pm$ 10%, Ceramic	AA
C527,	VCEAAU1CW106Y	10 $\mu$ F, 16V, +50 -10%	AB	C214			
C528				C215,	VCCSPU1HL471K	470pF, 50V, $\pm$ 10%, Ceramic	AB
C529	VCEAAU1HW105A	1 $\mu$ F, 50V, +75 -10%	AB	C216			
C601	VCEAAU1CW106Y	10 $\mu$ F, 16V, +50 -10%	AB	C219,	VCQYKU1HM223J	.022 $\mu$ F, 50V, $\pm$ 5%, Mylar	AB
C602	VCEAAU1CW106Y	10 $\mu$ F, 16V, +50 -10%	AB	C220			
C603	VCEAAU1CW337Y	330 $\mu$ F, 16V, +50 -10%	AD	C221,	VCQYKU1HM124J	.12 $\mu$ F, 50V, $\pm$ 5%, Mylar	AE
C604	VCEAAU1CW337Y	330 $\mu$ F, 16V, +50 -10%	AD	C222			
C605	VCEAAU1CW476Y	47 $\mu$ F, 16V, +50 -10%	AB	C225,	VCQYKU1HM222J	.0022 $\mu$ F, 50V, $\pm$ 5%, Mylar	AB
C607	VCEAAU1HW476Y	47 $\mu$ F, 50V, +50 -10%	AC	C226			
C612	VCEAAU1EW228Y	2200 $\mu$ F, 25V, +50 -10%	AH	C227,	VCQYKU1HM103J	.01 $\mu$ F, 50V, $\pm$ 5%, Mylar	AB
C613	VCEAAU1EW228Y	2200 $\mu$ F, 25V, +50 -10%	AH	C228			
C614	VCEAAU1EW227Y	220 $\mu$ F, 25V, +50 -10%	AC	C301	VCQSMT1HS331J	330pF, 50V, $\pm$ 5%, Styrol	AB
C615	VCEAAU1CW227Y	220 $\mu$ F, 16V, +50 -10%	AC	C302	VCCUPU1HJ150K	15pF (UJ), 50V, $\pm$ 10%, Ceramic	AB
C616	VCEAAU1EW227Y	220 $\mu$ F, 25V, +50 -10%	AC	C303	VCQSMT1HS121J	120pF, 50V, $\pm$ 5%, Styrol	AB
C617	VCEAAU1CW227Y	220 $\mu$ F, 16V, +50 -10%	AC	C304	VCCCPU1HH470J	47pF(CH), 50V, $\pm$ 5%, Ceramic	AB
C618	VCEAAU1EW227Y	220 $\mu$ F, 25V, +50 -10%	AC	C306	VCKZPU1HF103P	.01 $\mu$ F, 50V, +100 -0%, Ceramic	AE
C619	VCEAAU1CW227Y	220 $\mu$ F, 16V, +50 -10%	AC	C307	VCKZPU1HF103P	.01 $\mu$ F, 50V, +100 -0%, Ceramic	AE
C620	VCEAAU1CW476Y	47 $\mu$ F, 16V, +50 -10%	AB				
C621	VCEAAU1CW476Y	47 $\mu$ F, 16V, +50 -10%	AB	C308	VCCSPU1HL221K	220pF, 50V, $\pm$ 10%, Ceramic	AB
C622	VCEAAU1CW476Y	47 $\mu$ F, 16V, +50 -10%	AB	C311	VCCSPU1HL470K	47pF, 50V, $\pm$ 10%, Ceramic	AA
C626	VCEAAU1HW336Y	33 $\mu$ F, 50V, +50 -10%	AC	C312	VCQYKU1HM473K	.047 $\mu$ F, 50V, $\pm$ 10%, Mylar	AC
C627	VCEAAU1HW475A	4.7 $\mu$ F, 50V, +75 -10%	AB	C313	VCKZPU1HF473Z	.047 $\mu$ F	AB
C629	VCEAAU2AW106Y	10 $\mu$ F, 100V, +50 -10%	AC	C314	VCKZPU1HF473Z	.047 $\mu$ F	AB
C630	VCEAAU2AW107Y	100 $\mu$ F, 100V, +50 -10%	AF	C316	VCQYKU1HM223K	.022 $\mu$ F, 50V, $\pm$ 10%, Mylar	AB
C631	VCEAAU2AW107Y	100 $\mu$ F, 100V, +50 -10%	AF	C317	VCQYKU1HM103K	.01 $\mu$ F, 50V, $\pm$ 10%, Mylar	AB
C636,	VCEALU1HW105M	1 $\mu$ F, 50V, $\pm$ 20%, LL (Yellow)	AD	C320	VCKZPU1HF473Z	.047 $\mu$ F	AB
C637				C322,	VCQYKU1HM223J	.022 $\mu$ F, 50V, $\pm$ 5%, Mylar	AB
C638	VCEAAU1EW106Y	10 $\mu$ F, 25V, +50 -10%	AB	C323,			
C639	VCEAAU1EW106Y	10 $\mu$ F, 25V, +50 -10%	AB	C324,	VCCSPU1HL101K	100pF, 50V, $\pm$ 10%, Ceramic	AA
				C325			
				C401,	VCKZPU1HF102Z	.001 $\mu$ F	AA
				C402			
				C403,	VCCSPU1HL220K	22pF, 50V, $\pm$ 10%, Ceramic	AA
				C404			
				C409,	VCQSMU1HD562G	5600pF, 50V, $\pm$ 2%, Styrol	AD
				C410			
				C413,	VCQSMU1HD162G	1600pF, 50V, $\pm$ 2%, Styrol	AD
				C414			
				C415,	VCKZPU2TE103Z	.01 $\mu$ F, 150VAC, +80 -20%, Ceramic	AB
				C416			
				C503,	VCCSPU1HL391K	390pF, 50V, $\pm$ 10%, Ceramic	AB
				C504			
				C507,	VCCSPU1HL330K	33pF, 50V, $\pm$ 10%, Ceramic	AA
				C508			
				C511,	VCQYKU1HM104K	.1 $\mu$ F, 50V, $\pm$ 10%, Mylar	AC
				C512			
				C517,	VCKZPU2TE103Z	.01 $\mu$ F, 150VAC, +80 -20%, Ceramic	AB
				C518,			
				C519,			
				C520			

## CAPACITORS

Unless otherwise specified capacitors are  
50V, +80 -20%, Ceramic Type

C101	VCKZPU1HF102Z	.001 $\mu$ F	AA
C102	VCKZPU1HF223Z	.022 $\mu$ F	AA
C103	VCKZPU1HF223Z	.022 $\mu$ F	AA
C104	VCKZPU1HF223Z	.022 $\mu$ F	AA
C105	VCKZPU1HF223Z	.022 $\mu$ F	AA
C106	VCKZPU1HF223Z	.022 $\mu$ F	AA
C107	VCKZPU1HF223Z	.022 $\mu$ F	AA
C108	VCKZPU1HF223Z	.022 $\mu$ F	AA
C110	VCKZPU1HF223Z	.022 $\mu$ F	AA
C111	VCKZPU1ND474M	.47 $\mu$ F, 12V, $\pm$ 20%, Ceramic	AD
C112	VCKZPU1HF223Z	.022 $\mu$ F	AA
C113	VCKZPU1HF223Z	.022 $\mu$ F	AA
C114	VCKZPU1HF223Z	.022 $\mu$ F	AA
C117	VCKZPU1HF223Z	.022 $\mu$ F	AA
C118	VCKZPU1HF223Z	.022 $\mu$ F	AA
C120	VCCSPU1HL331K	330pF, 50V, $\pm$ 10%, Ceramic	AB
C122	VCQYKU1HM473K	.047 $\mu$ F, 50V, $\pm$ 10%, Mylar	AC
C126	VCQSMT1HS391K	390pF, 50V, $\pm$ 10%, Styrol	AB
C129	VCQSMT1HS122J	1200pF, 50V, $\pm$ 5%, Styrol	AB

# PARTS LIST

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
C521, C522, C523, C524	VCKZPU2TE103Z	.01μF, 150VAC, +80 -20%, Ceramic	AB	R141, R142	VRD-ST2EE682J	6.8K ohm	AA
C606	VCKZPU1HF223Z	.022μF	AA	R143, R144	VRD-ST2EE473J	47K ohm	AA
C608, C609, C610, C611	VCKZPU1HF223Z	.022μF	AA	R145, R146	VRD-ST2EE272J	2.7K ohm	AA
C623, C624, C625	VCKZPU1HF223Z	.022μF	AA	R147, R148	VRD-ST2EE392J	3.9K ohm	AA
C632, C633, C634, C635	VCKZPU2TE103Z	.01μF, 150VAC, +80 -20%, Ceramic	AB	R149, R150	VRD-ST2EE222J	2.2K ohm	AA
C801, C802	VCKZPU1HF223Z	.022μF	AA	R151	VRD-ST2EE333J	33K ohm	AA
C803, C804	RC-PZ061CAFZZ	.05μF, 250VAC, ±20%, Oil	AF	R152	VRD-ST2EE101J	100 ohm	AA
				R153	VRD-ST2EE474J	470K ohm	AA
				R154	VRD-ST2EE223J	22K ohm	AA
				R155	VRD-ST2EE334J	330K ohm	AA
				R156	VRD-ST2EE473J	47K ohm	AA
				R157	VRD-ST2EE473J	47K ohm	AA
				R201, R202	VRD-ST2EE333J	33K ohm	AA
				R203, R204	VRD-ST2EE103J	10K ohm	AA
				R205, R206	VRD-ST2EE474J	470K ohm	AA
				R207, R208	VRD-ST2EE563J	56K ohm	AA
				R209, R210	VRD-ST2EE104J	100K ohm	AA
				R211, R212	VRD-ST2EE471J	470 ohm	AA
				R213, R214	VRD-ST2EE102J	1K ohm	AA
				R215, R216	VRD-ST2EE183J	18K ohm	AA
				R217, R218	VRD-ST2EE332J	3.3K ohm	AA
				R219, R220	VRD-ST2EE332J	3.3K ohm	AA
				R221, R222	VRD-ST2EE562J	5.6K ohm	AA
				R223, R224	VRD-ST2EE122J	1.2K ohm	AA
				R225, R226	VRD-ST2HD221J	220 ohm, 1/2W, ±5%, Carbon	AA
				R227, R228	VRD-ST2EE224J	220K ohm	AA
				R301	VRD-ST2EE681J	680 ohm	AA
				R302	VRD-ST2EE102J	1K ohm	AA
				R303	VRD-ST2EE332J	3.3K ohm	AA
				R304	VRD-ST2EE222J	2.2K ohm	AA
				R305	VRD-ST2EE183J	18K ohm	AA
				R306	VRD-ST2EE822J	8.2K ohm	AA
				R307	VRD-ST2EE562J	5.6K ohm	AA
				R308	VRD-ST2EE393J	39K ohm	AA
				R309	VRD-ST2EE101J	100 ohm	AA
				R310	VRD-ST2EE470J	47 ohm	AA
				R311	VRD-ST2EE101J	100 ohm	AA
				R312	VRD-ST2EE823J	82K ohm	AA
				R313	VRD-ST2EE103J	10K ohm	AA
				R314	VRD-ST2EE223J	22K ohm	AA
				R315	VRD-ST2EE103J	10K ohm	AA
				R316	VRD-ST2EE103J	10K ohm	AA
				R317	VRD-ST2EE223J	22K ohm	AA
				R318	VRD-ST2EE151J	150 ohm	AA
				R319	VRD-ST2EE332J	3.3K ohm	AA
				R320	VRD-ST2EE123J	12K ohm	AA

## RESISTORS

Unless otherwise specified resistors are 1/4W, ±5%, Carbon Type.

# PARTS LIST

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
R321	VRD-ST2EE122J	1.2K ohm	AA	R535,	VRD-ST2EE182J	1.8K ohm	AA
R322	VRD-ST2EE473J	47K ohm	AA	R536			
R324	VRD-ST2EE822J	8.2K ohm	AA	R537,	VRD-ST2EE182J	1.8K ohm	AA
R325	VRD-ST2EE103J	10K ohm	AA	R538			
R326	VRD-ST2EE103J	10K ohm	AA	R539,	VRD-ST2EE182J	1.8K ohm	AA
R401,	VRD-ST2EE471J	470 ohm	AA	R540			
R402				R541,	VRD-ST2EE223J	22K ohm	AA
R403,	VRD-ST2EE473J	47K ohm	AA	R542			
R404				R543,	VRD-ST2EE222J	2.2K ohm	AA
R405,	VRD-ST2EE332J	3.3K ohm	AA	R544			
R406				R545,	VRD-ST2EE123J	12K ohm	AA
R407,	VRD-ST2EE102J	1K ohm	AA	R546			
R408				R547,	VRW-KT3DD2R2K	2.2 ohm, 2W, $\pm 10\%$ , Wire Wound	AC
R409,	VRD-ST2EE103J	10K ohm	AA	R548			
R410				R549,	VRW-KT3DD100K	10 ohm, 2W, $\pm 10\%$ , Wire Wound	AC
R411,	VRD-ST2HD103J	10K ohm, 1/2W, $\pm 5\%$ , Carbon	AA	R550			
R412				R551,	VRG-ST2HA1R0J	1 ohm, 1/2W, Fusible	AC
R413,	VRD-ST2EE624J	620K ohm	AA	R552			
R414				R553,	VRG-ST2HA1R0J	1 ohm, 1/2W, Fusible	AC
R415,	VRD-ST2EE473J	47K ohm	AA	R554			
R416				R555	VRD-ST2EE332J	3.3K ohm	AA
R417,	VRD-ST2EE104J	100K ohm	AA	R557,	VRD-ST2EE392J	3.9K ohm	AA
R418				R558			
R419,	VRD-ST2EE224J	220K ohm	AA	R559,	VRD-ST2EE472J	4.7K ohm	AA
R420				R560			
R421,	VRD-ST2EE102J	1K ohm	AA	R601	VRD-ST2EE153J	15K ohm	AA
R422				R602	VRD-ST2EE333J	33K ohm	AA
R423,	VRD-ST2EE222J	2.2K ohm	AA	R603	VRD-ST2EE393J	39K ohm	AA
R424				R604	VRD-ST2EE392J	3.9K ohm	AA
R501,	VRD-ST2EE564J	560K ohm	AA	R605	VRD-ST2EE682J	6.8K ohm	AA
R502				R606	VRD-ST2EE682J	6.8K ohm	AA
R503,	VRD-ST2EE821J	820 ohm	AA	R607	VRD-ST2EE470J	47 ohm	AA
R504				R608	VRD-ST2EE563J	56K ohm	AA
R505,	VRD-ST2EE223J	22K ohm	AA	R609	VRD-ST2EE273J	27K ohm	AA
R506				R610	VRD-ST2EE121J	120 ohm	AA
R507,	VRD-ST2EE331J	330 ohm	AA	R611	VRD-ST2EE473J	47K ohm	AA
R508				R612	VRD-ST2EE221J	220 ohm	AA
R509,	VRD-ST2EE681J	680 ohm	AA	R613	VRD-ST2EE223J	22K ohm	AA
R510				R614	VRD-ST2EE223J	22K ohm	AA
R511,	VRD-ST2EE102J	1K ohm	AA	R615	VRD-ST2EE221J	220 ohm	AA
R512				R616	VRS-PT3DB681K	680 ohm, 2W, $\pm 10\%$ , Oxide Film	AB
R513,	VRD-ST2EE563J	56K ohm	AA				
R514				R617	VRS-PT3AB331K	330 ohm, 1W, $\pm 10\%$ , Oxide Film	AB
R515,	VRD-ST2EE223J	22K ohm	AA				
R516				R618,			
R517,	VRG-ST2EA680J	68 ohm, 1/4W, Fusible	AB	R619,	VRG-ST2EA680J	270 ohm, 2W, $\pm 10\%$ , Oxide Film	AB
R518				R620,			
R519,	VRG-ST2EA101J	100 ohm, 1/4W, Fusible	AB	R621			
R520				R622	VRD-ST2EE102J	1K ohm	AA
R521,	VRG-ST2EA4R7J	4.7 ohm, 1/4W, Fusible	AB	R623	VRD-ST2EE391J	390 ohm	AA
R522				R624	VRD-ST2EE102J	1K ohm	AA
R523,	VRG-ST2EA101J	100 ohm, 1/4W, Fusible	AB	R625	VRD-ST2EE391J	390 ohm	AA
R524				R626	VRD-ST2EE102J	1K ohm	AA
R525,	VRG-ST2EA101J	100 ohm, 1/4W, Fusible	AB	R627	VRD-ST2EE391J	390 ohm	AA
R526				R628	VRD-ST2HD472J	4.7K ohm, 1/2W, $\pm 5\%$ , Carbon	AA
R527,	VRG-ST2EA4R7J	4.7 ohm, 1/4W, Fusible	AB				
R528				R629	VRD-ST2HD103J	10K ohm, 1/2W, $\pm 5\%$ , Carbon	AA
R529,	VRD-ST2EE182J	1.8K ohm	AA				
R530				R630	VRD-ST2EE153J	15K ohm	AA
R531,	VRW-KT3H3DR33K	.33 ohm, 5W, $\pm 10\%$ , Wire Wound	AD	R631	VRD-ST2EE103J	10K ohm	AA
R532				R632	VRD-ST2EE332J	3.3K ohm	AA
R533,	VRW-KT3H3DR33K	.33 ohm, 5W, $\pm 10\%$ , Wire Wound	AD	R633	VRD-ST2EE104J	100K ohm	AA
R534				R634	VRD-ST2EE334J	330K ohm	AA
				R635	VRD-ST2EE101J	100 ohm	AA

# PARTS LIST

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
R636	VRD-ST2HD123J	12K ohm, 1/2W, ±5%, Carbon	AA	LANGT0622AFZZ	Bracket, Heat Sink	—	
R638	VRD-ST2EE332J	3.3K ohm	AA	LBSHC0002AGZZ	Bushing, LW/MW Bar Antenna Wire	AB	
R639	VRD-ST2EE121J	120 ohm	AA	LBSHC0004AGZZ	Bushing, Power Supply Cord (SEMKO, KEMA)	AC	
R640, R641	VRD-ST2EE221J	220 ohm	AA	LBSHC0007AFZZ	Bushing, Power Supply Cord (SEV, A-club)	AB	
R642, R643	VRD-ST2EE272J	2.7K ohm	AA	LCHSM0257AFZZ	Chassis Assembly	AW	
R644, R645	VRD-ST2EE682J	6.8K ohm	AA	LHLDP3055AFZZ	Holder, Dial Lamp (Part of PREFL0061AFZZ)	—	
R646, R647	VRD-ST2EE183J	18K ohm	AA	LHLDW1050AFZZ	Wire Clip	AA	
R648, R649	VRD-ST2EE222J	2.2K ohm	AA	LHLDW1051AFZZ	Wire Clip	AA	
R650	VRD-ST2EY822J	8.2K ohm	AA	LHLDW1052AFZZ	Wire Clip	AA	
R701, R702, R703, R704	VRD-ST2EY102J	1K ohm	AA	LHLDW1053AFZZ	Wire Clip	AA	
R705, R706	VRD-ST2EY104J	100K ohm	AA	LHLDW1060AFZZ	Wire Clip	AA	
R707, R708	VRD-ST2EY394J	390K ohm	AA	LHLDW1062AFZZ	Wire Clip	AA	
R709, R710, R711, R712	VRD-ST2EY102J	1K ohm	AA	LHLDW1066AFZZ	Wire Holder, AM Antenna Wire	AD	
R713, R714	VRD-ST2EY104J	100K ohm	AA	LPLTP0053AFZZ	Acryl, Dial Illumination (Part of PREFL0061AFZZ)	—	
R715, R716	VRD-ST2EY394J	390K ohm	AA	LX-HZ0053AFFD	Flange Head Screw, P.W. Board	AA	
				LX-LZ0055AF00	Plastics Rivet, FM Tuner Ass'y, 4φ	AA	
				LX-NZ0001SGFD	Flange Nut, Antenna Terminals	AA	
				LX-NZ0118AFFD	Nut, Speaker Selector Switch Shaft, Function Selector Switch Shaft and Headphone Jacks	AA	
				LX-NZ0119AFFW	Hexagon Head Cap Screw, Speaker Selector Switch and Function Selector Switch	AD	
				LX-NZ0120AFFD	Flange Nut (5φ), Power Transformer	AA	
				MSPRP0152AFZZ	Plate Spring, Grounding (Earth)	AA	
				MSPRT0304AFFJ	Spring, Dial Cord	AA	
				NDRM-0150AFZZ	Drum	AF	
				NPLYB0001SGZZ	Pulley, Dial Cord	AB	
				NPLYC0101AFFD	Shaft, Pulley	AA	
				NSFTD0171AFFW	Tunning Shaft with Flywheel	AN	
				PCOVP1158AFZZ	Cover, Fuse, Rear Panel	AF	
				PRDAR0139AF00	Heat Sink, Power Transistor	BA	
				PREFL0061AFZZ	Dial Illumination Assembly	BA	
				PSHEF0110AFZZ	Felt (Long), Lever Switch	AA	
				PSHEF0114AF00	Felt (Short), Power Switch	—	
				PSLDM3126AFZZ	Shield Plate	AA	
				PSPAS0053AFSA	Spacer, Push Knob	AB	
				PSPAS0054AFZZ	Spacer, Headphone Jack	AC	
				PSPAZ0050AFZZ	Insulator, Mica, Power Transistor	AB	
				PSPAZ0060AFZZ	Spacer, LED (D801)	AA	
				PZETF0128AFZZ	Insulator, Fuse P.W. Board	—	
				QACCN0001AGZZ	Power Supply Cord with Plug (SEMKO)	AP	
				QACCS9001SE00	Power Supply Cord (SEV)	AF	
				QPLGA0205AGZZ	Plug, Power Supply Cord (SEV)	AH	
				QACCV0001AGZZ	Power Supply Cord with Plug (KEMA)	AN	
				QACCC0002TA0F	Power Supply Cord with Plug (USA type Plug)	AF	
				QACCC0002AG08	Power Supply Cord	AF	

# PARTS LIST

REF. NO.	PART NO.	DESCRIPTION	CODE	REF. NO.	PART NO.	DESCRIPTION	CODE
R		QPLGA0201AGZZ	AE	SO801-}		Socket, Auxiliary Input	AG
R		QANTW0055AFZZ	AH	A ~ F }	QSOCJ2660AFZZ	(SO801-A, B), PHONO-1	
R	CN201	QCNCM135LAFZZ	AE			Input (SO801-C, D),	
R	CN202	QCNCM132FAFZZ	AD			PHONO-2 Input	
R	CN203	QCNCM132FAFZZ	AD			(SO801-E, F)	
R	CN301	QCNCM133GAFZZ	AD	SW201-}	QSW-R0141AFZZ	Switch, Function Selector	AR
R	CN302	QCNCM134HAFZZ	AD	A, B }	QSW-B0073AFZZ	Switch, Tape Monitor	AH
R	CNP801	QCNCW108CAFZZ	—	SW202	QSW-B0054AFZZ	Switch, Tape Dubbing	AK
R		(Part of PREFL0061AFZZ)		SW203-}			
R	CNS101	QCNCW104GAFZZ	AB	A ~ D }	QSW-B0051AFZZ	Switch, Mode Selector	AH
R	CNS102	QCNCW105HAFZZ	AB	SW204	QSW-B0051AFZZ	Switch, Loudness	AH
R	CNS201	QCNCW106LAFZZ	AC	SW205			
R	CNS202	QCNCW103FAFZZ	AB				
R	CNS203	QCNCW103FAFZZ	AB	SW301-}	QSW-P0142AFZZ	Switch, Band (LW/MW/FM)	AS
R		QFS-C101CAGNI	AE	A ~ E }		Selector (SW301-A ~ C), FM	
R		QFS-C201CAGNI	AE			Muting (SW301-D), Air	
R		QFS-C202CAGNI	AE			Check Calibrator (SW301-E)	
R		QFSDH1001AGZZ	AA	SW601	QSW-R0140AFZZ	Switch, Speakers Selector	AN
R	J601	QJAKJ0057AFZZ	AG	SW602	QSW-B0051AFZZ	Switch, Low Cut Filter	AH
R	J602	QJAKJ0057AFZZ	AG	SW603	QSW-B0051AFZZ	Switch, Audio Muting	AH
R		QLUGL0250AFZZ	AC	SW801	QSW-B9059AFZZ	Switch, Power	AQ
R		QLUGZ011AAFZZ	AA	TB801	QTANN0453AFZZ	Antenna Terminals, FM	AH
R		QPLGS0102AGZZ	AD			(75 ohms and 240 ohms)	
R		QPWBE0077AFZZ	AQ			and AM	
R		Printed Wiring Board, Power		TB802	QTANN0150AFZZ	Terminal, Grounding (Earth)	AD
R		Amplifier Circuit		TB803	QTANN0454AFZZ	Speaker Terminals-A	AG
R		QPWBF0353AFZZ	AD	TB804	QTANN0454AFZZ	Speaker Terminals-B	AG
R		Printed Wiring Board, Tape		ME801	RMTRL0135AFSA	Meter, Signal (Strength)	AU
R		Circuit		ME802	RMTRL0134AFSA	Meter, Tuning (Center)	AU
R		QPWBF0423AFZZ	AE	RLY601	RRLYZ0050AFZZ	Relay, DC24V, Protection	AW
R		Printed Wiring Board, Fuse		-A, B }		Circuit	
R		Circuit			RTUNF0060AFZZ	FM Tuner (Front-end)	BF
R		QPWBF0593AFZZ	—			Assembly	
R		Printed Wiring Board, Dial					
R		Lamp Circuit		PL801,		Dial Illumination Lamp	
R		(Part of PREFL0061AFZZ)		PL802,		(8V, 0.3A)	
R		QPWBF0594AFZZ	AS	PL803,	RLMPP0057AFZZ	(Part of PREFL0061AFZZ)	
R		Printed Wiring Board, FM		PL804,			
R		RF/IF, Equalizer and Tone		PL805,			
R		Circuits		PL806			
R		QPWBF0595AFZZ	AM		XBBSD40P45000	Screw, Bar Antenna Bracket	AA
R		Printed Wiring Board, Power			XHBSF40P18XSO	Screw, Cabinet	
R		Supply and Relay-Circuits			XHBSD40P12000	Screw, Leg	
R		QPWBF0597AFZZ	AU		XNESD40-32000	Nut, Bar Antenna Bracket	AA
R		Printed Wiring Board, AM			XWHSD91-10140	Washer, Function Selector	
R		RF/IF Circuit				Switch	
R		QSOCT0353AFZZ	AD		XWUSE84-08000	Shakeproof Lockwasher	AA
R		Socket, Power Transistor				Internal Type, Grounding	
R						(Earth) Terminal	
R	SO701-}						
R	A ~ E }	QSOCZ2450AFZZ	AK				
R		TAPE-1 Socket,					
R		REC (SO701-A, B),					
R		PB (P) (SO701-C, D),					
R		DIN (SO701-E)					
R	SO702-}						
R	A ~ E }	QSOCZ2450AFZZ	AK				
R		TAPE-2 Socket,					
R		REC (SO702-A, B),					
R		PB (P) (SO702-C, D),					
R		DIN (SO702-E)					