



Set using ISO screws

STR-6045

USA and CANADA Model



SONY®
SERVICE MANUAL

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SECTION 1 TECHNICAL DESCRIPTION

1-1. TECHNICAL SPECIFICATIONS

Technical specifications for the STR6045 are given in Table 1-1.

TABLE 1-1. TECHNICAL SPECIFICATIONS

Fm Tuner Section

Antenna	: 300 ohms balanced
Intermediate frequency	: 10.7 MHz
Tuning range	: 87.5 to 108 MHz
Sensitivity	: 2.6 μ V (IHF usable sensitivity) 2.2 μ V (S/N, 30 dB)
S/N ratio	: 70 dB
Capture ratio	: 1.5 dB
Selectivity	: 80 dB
Image rejection	: 75 dB
I-f rejection	: 90 dB
Suprious rejection	: 100 dB
A-m suppression	: 65 dB
Frequency response	: 20 Hz to 15 kHz \pm 9 dB
Stereo separation	: 35 dB at 400 Hz
Harmonic distortion:	Mono : 0.4 % IHF (400 Hz 100 % Mod.) Stereo : 0.8 % IHF (400 Hz 100% Mod.)
19 kHz, 38 kHz suppression	: 50 dB

A-m Tuner Section

Antenna	: Built-in ferrite bar antenna with external antenna terminal
Tuning range	: 530 kHz to 1605 kHz
Sensitivity	: 50 dB/m, built-in antenna (S/N : 20 dB) 30 μ V, external antenna
I-f rejection	: 41 dB at 1000 kHz
Harmonic distortion	: 0.8%
Image rejection	: 45 dB at 1000 kHz

Audio Amplifier Section

Dynamic power output	: 75 watts (8 ohms), both channels operating
(IHF constant supply method)	: 84 watts (4 ohms), both channels operating

Continuous RMS power	: 25 watts (8 ohms) per channel both channels operating
20 Hz to 20 kHz power	: 20 watts (8 ohms) both channels operating
Power bandwidth	: 10 Hz to 30 kHz, IHF
Harmonic distortion	: Less than 0.5 % at 1 kHz at rated continuous RMS power output Less than 0.5 % at 1 watt output
IM distortion	: Less than 0.5 % at rated continuous RMS power output
Frequency response	: PHONO : RIAA curve \pm 1 dB TAPE } 10 Hz to 50 kHz \pm 9 dB AUX }
Input sensitivity and impedance	: PHONO : 2.5 mV, 47 k TAPE } 250 mV, 100 k AUX }
Signal output and impedance	: REC OUT : 250 mV, 15 k
S/N ratio	: PHONO : greater than 65 dB (weighting network "B") TAPE : greater than 90 dB (weighting network "A") AUX : greater than 70 dB (weighting network "A")
Tone controls	: BASS : \pm 10 dB at 100 Hz TREBLE : \pm 10 dB at 10 kHz
Filters	: HIGH 6 dB/oct. above 5 kHz
Loudness control	: +8 dB at 50 Hz +4 dB at 10 kHz (with 30 dB attenuation)

General

Power consumption	: 95 watts
Power requirement	: 120 volts, 50/60 Hz ac
Dimensions	: 400 mm (width) \times 145 mm (height) \times 310 mm (depth) 15 ³ / ₄ " (width) \times 5 ³ / ₄ " (height) \times 12 ¹ / ₄ " (depth)
Net weight	: 8.3 kg (18 lbs 5 oz)
Shipping weight	: 11.4 kg (25 lbs 2 oz)

1-2. DETAILED CIRCUIT ANALYSIS

The following describes the function or operation of all stages and controls. The text sequence follows signal paths. Stages are listed by transistor reference designation at the left margin; major components are also listed in a similar manner.

Refer to the block diagram on pages 9 to 10 and the schematic diagram on pages 39 to 42.

Stage/ControlFunction**FM Front End**

Passive rf circuit	A triple-tuned circuit is employed between the antenna and mixer transistor. This passive coupling circuit contains no active amplifiers, so it is perfectly linear and cannot produce distortion and overload components. Thus, the factors that contribute to spurious responses are eliminated ahead of the mixer.
Local oscillator Q102	Supplies heterodying voltage to the mixer via L104. The circuit is a modified Hartley type with feedback applied to the emitter from the tap on L104.
Mixer Q101	Rf signals and local oscillator voltage are heterodyned in the gate-source junction of mixer Q101 to produce 10.7 MHz i-f output signal. IFT101 is a tuned transformer for 10.7 MHz and its low impedance output winding supplies link coupling to i-f preamplifier Q103.
I-f preamplifier Q103	The i-f signal coupled to the base of i-f preamplifier Q103 by the secondary winding of IFT101 is amplified to achieve a favorable signal-to-noise ratio before application to the filters in the i-f strip.

Stage/ControlFunction**Fm I-f Section**

I-f amplifiers
Q201 to Q206

These i-f stages are basically RC coupled amplifiers that provide essentially flat response.

CF201 to CF206

The selectivity of this section is determined by the solid-state filters in the interstage coupling paths. These ceramic filters are made up of two individual sections that operate in a "trapped-energy" mode. The filters provide extremely sharp skirt selectivity and flat response inside the pass band. These filters determine overall selectivity in the tuner.

TUNER INPUT
meter M
D210, D211

I-f signal from the collector of Q204 is coupled through C206 to a rectifier-doubler consisting of diodes D210 and D211. At this point in the circuit, the i-f signal is proportional to the r-f signal strength for all but very-strong input signals. Therefore, the filtered dc output voltage of the rectifier-doubler is proportional to the r-f signal strength, and is used to drive TUNER INPUT meter M. D209 is shunted across the meter to protect it from overload.

D209

I-f output
Q206

Signal at the base of Q206 has had all amplitude variations removed by the preceding limiters, and only selected signals have been passed by ceramic filters. Q206 provides power to drive the ratio detector.

Diode limiters
D201 to D206

Limiting is accomplished by diode pairs, connected in parallel and poled in opposite directions. The diodes conduct when the signal across them exceeds the barrier potential of about 0.6

<u>Stage/Control</u>	<u>Function</u>	<u>Stage/Control</u>	<u>Function</u>
	volts in the forward direction. Thus the signal is limited in both directions to 1.2 volts peak-to-peak. The diodes provide symmetrical limiting.		
Ratio detector D207, D208	T201 and diodes D207 and D208 form a balanced ratio detector that transforms the frequency-modulated signal into an audio signal. Output appears across C215.	Stereo-mono automatic switching circuit Q304, D303, D304 D305, D306.	This prevents noisy stereo reception by automatically switching the MPX decoder's operation into the monaural mode. Noise signals above 19 kHz are extracted from the emitter circuit of Q301 and applied to the base of Q304 through a high-pass filter (L302, C306). The coupling capacitor C307 filters out audio components so that the input signal is primarily high-frequency noise. This noise signal is amplified by Q304 to drive voltage doubler D304 and D306. D305 provides positive fixed bias for Q304 through D306 and D304. When a weak stereo signal or interstation noise is received the output of D304 is fed back to the base of Q304, and drives Q304 into conduction. This in turn shorts the frequency doubler output to ground through R315, preventing amplification of the incoming signal, and therefore operation of the 38 kHz amplifier and stereo indicator circuit, Q302 and Q303. When a stereo signal is received, the signal-to-noise ratio increases, reducing the noise signal at the base of Q304. Therefore Q304 turns off and enables the stereo demodulator circuit to operate. The 38 kHz pulses produced by D301 and D302 are amplified by Q302. The tank circuit at the collector of Q302 is tuned to 38 kHz to restore these pulses to a sinusoidal waveform. This signal is transformer coupled to the bridge type demodulator to supply sampling drive for the demodulator.
MPX Decoder			
SCA trap L301, C302	The composite signal containing monaural information from 0 to 15 kHz, the 19 kHz pilot carrier, and the fm stereo signal at 38 kHz, is fed to Q301 through trap L301-C302. This trap removes the unwanted SCA signals to feed a clean composite signal to the base of Q301 (the 19 kHz amplifier).		
19 kHz amplifier Q301	This stage serves two functions. It extracts the 19 kHz pilot signal by means of a tuned circuit at its collector, and provides a low-impedance source of composite stereo signal (without the pilot carrier) at its emitter. A series-resonant circuit in the emitter circuit eliminates the 19 kHz pilot signal in the composite stereo signal.		
Frequency doubler D301, D302	Signals developed at the collector of Q301 are transformer coupled to a fullwave rectifier consisting of D301 and D302. The output of this rectifier is not filtered, resulting in two positive pulses for each input cycle. Thus, the 19 kHz pilot-carrier frequency is effectively doubled by D301 and D302. However, the waveform is not sinusoidal at the base of Q302.	38 kHz amplifier Q302	
		STEREO lamp circuit Q303	The STEREO indicator lights when the FUNCTION switch is set to the FM AUTO STEREO

Stage/Control	Function
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position and an fm stereo signal is received. The emitter of Q302 is connected to the base of Q303 which is normally cut off.

The circuit operates as follows: When a composite stereo signal is applied to the multiplex decoder, the 38 kHz pulses produced at the output of the frequency doubler yield a higher average current flow through Q302. This forces Q303 into conduction, lighting STEREO indicator lamp PL901.

Multiplex demodulator
D307, D308
D309, D310

The demodulator circuit employs four diodes in a balanced-bridge arrangement. This system has the advantage of cancelling residual rf components (38 kHz signal, some 19 kHz signal, and higher order harmonics of these frequencies.)

"L" and "R" components are developed at each side of the bridge as the result of demodulation, when the receiver is operated in the stereo mode. (See Fig. 1-1.)

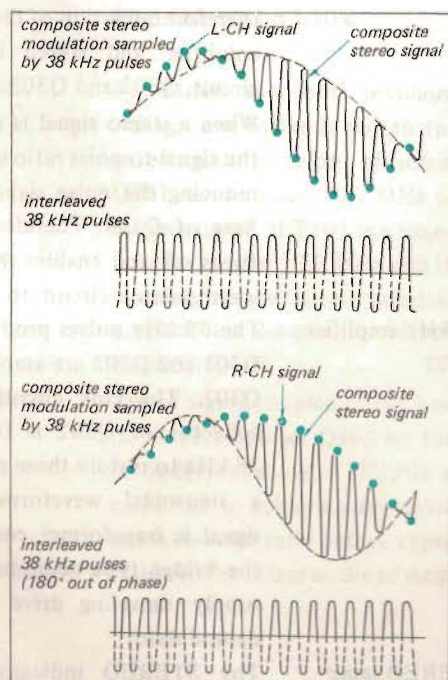


Fig. 1-1 Stereo demodulation operation

Stage/Control	Function
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In the monaural mode, diodes D307 and D310 are forward biased by supply voltage through R316, the STEREO indicator lamp, R318, R323, and R322, so these diodes merely act as small resistances. Under this condition, the monaural signal is applied to both "L" and "R" audio amplifiers.

Twin-T filter
R330, R332, R329
R331, R333, R328
C324, C328, C327
C325, C329, C326

This filter eliminates the 38 kHz carrier and residual rf components, thereby preventing carrier leak.

A-m Tuner

Antenna circuit
L901, C401, L402, CV401,
CT401, C402 and C403. C401 is selected not for its effect upon tuning, but to reduce spurious radiation by the local oscillator. The low pass filter (L401 - C401) reduces the spurious radiation caused by local oscillator which may interfere another receiver or communication system through the external antenna.

Local oscillator
Q405

This stage supplies the injection voltage necessary to receive a-m signals.

In this modified Hartley oscillator circuit, feedback is applied to the emitter of Q405 from a low-impedance winding on oscillator coil L404.

S2 FUNCTION (2) switch

Mixer Q401

S2 is a rotary-slide switch which is interconnected with rotary switch's shaft to perform proper changeover of tuner operation. Incoming rf signal is fed to the base of Q401, while the local oscillator voltage is injected to the emitter circuit of Q401. These two signals are heterodyned in

Stage/Control Function

the base-emitter junction of Q401 to produce the 455-kHz output. This stage functions as the gain control element of the agc system due to Q402 in the emitter circuit, as will be explained later.

CFT401 CFT401 is a combination unit which contains a double-tuned circuit and one ceramic filter tuned to 455 kHz. It develops the i-f signal, and determines the selectivity inside the passband. It also provides link coupling to i-f amplifier Q403.

AGC circuit There are two feedback loops which provide proper agc operation. One is the minor loop applying AGC to the i-f amplifier Q404's base circuit. The other is the major feedback loop applying dc from the emitter circuit of Q404 to the emitter circuit of Q401 through Q402. The minor feedback loop consists of D401, R418, R438, C431 and R415. The a-m i-f signal is extracted from the collector circuit of Q404 through C413 and rectified by diode D401. The output of the diode D401 is a positive dc voltage roughly proportional (not exactly due to agc action) to the carrier levels of input signal and fed to the base of Q402 through a filter circuit. Thus the output of diode D401 controls the current flow in Q404 and its emitter voltage as well. Major feedback is produced by the emitter circuit of Q404, R416, C429, C427, R433 and Q402. The emitter voltage of

Stage/Control Function

Q404 is applied to the base of Q402 through the filter circuit, determining the positive bias on Q402. As the Q402 shunts the emitter resistor of mixer Q401, it controls the operation of Q401 as a forward agc element. When the strong signal is received, Q402 is forced into conduction, shorting Q401's emitter to ground through R405. As a result, current flow in the Q401 (mixer) increase, reducing its current gain and allowing stable operation in a strong field-strength area.

I-f amplifier Q403 This stage is basically an RC-coupled amplifier and amplifies the i-f signal to the proper level required by the following stages.

I-f amplifier Q404 Q404 and IFT401 from a tuned amplifier circuit which provides power to drive diode detector D402.

Detector D402 The i-f signal from the secondary side of IFT401 is rectified by diode D402. The i-f components of the output signal are filtered by C416, R422 and C417, and then cleaned audio signal is fed to the audio preamplifier through FUNCTION switch S2.

TUNER INPUT Meter M The detector's (D402) output is also fed to TUNER INPUT meter M as the dc component in the rectified a-m signal is roughly proportional to the input signal level (not exactly for strong signals due to agc action).

Stage/ControlFunction**Audio Preamplifier Section**

Equalizer/ Preamplifier Q501, Q502	This direct-coupled two stage amplifier amplifies the small signal produced by the tuner, phono cartridge, tape recorder, or signal applied to the AUX input jacks, to the level required at the input of the following tone-control buffer amplifier.
Bias circuit	Dc bias voltage for Q501 is extracted from R511 in the emitter circuit of Q502 through R505 and R504. This dc negative feedback technique provides stable operation during temperature changes.
Equalization circuit	RIAA equalization is achieved by the negative-feedback loop containing R516, R517, R518, C511 and C512 when the FUNCTION switch is set to PHONO.
De-emphasis circuit	The proper de-emphasis operation is achieved by the negative-feedback loop containing R513, R514, C509 and C513. Specified de-emphasis time constant is 75 micro-seconds in USA and CANADA, 50 micro-seconds in Europe. The de-emphasis circuit operates even in the a-m reception mode, but it has no effect upon these operation because the a-m signal frequency response is so inferior to that of an fm signal. In addition, the channel separation control circuit works at the same time when FUNCTION switch S1 is set to TUNER position.
Separation control RT551	The network that connects the emitters of Q501 and Q551 provides a form of negative feedback between left and right channels for fm stereo signals. Any residual "R" signal in the

Stage/ControlFunction

	"L" channel (which is about 180° out of phase) is cancelled out by the "R" signal from the "R" channel. The same is true of residual "L" signal in the "R" channel. RT551 is therefore set for maximum separation. In the AUX position of the FUNCTION switch, feedback is applied through R515 and C510 to provide a flat response in the equalizer/preamplifier. Signals applied to the AUX input jack are attenuated about 40 dB by R501 and R502. This allows the STR-6045 to accept signals at about 250 mV and amplify them without distortion.
VOLUME control RV901	The equalized phono signal and signals applied to the other input terminals are fed to the VOLUME control through the MONITOR and MODE switches. The level of the signal applied to the following tone-control amplifier is determined by the setting of RV601.
LOUDNESS switch S6	This switch and R601, R602, C601, and C602 compensate for the characteristics of the human ear which vary according to the loudness of the sound being heard. When this switch is set to ON and the VOLUME control is set for 30 dB attenuation, the overall frequency response is increased +8 dB at 50 Hz and +4 dB at 10 kHz with reference to the level at 1 kHz.
Buffer amplifier Q601	This amplifier provides +14 dB voltage gain to compensate for the tone-control insertion loss and isolates the volume control and tone control to eliminate mutual interference.
TREBLE control RV602	This control has a range of ±10 dB at 10 kHz.
BASS control RV603	This control has a range of ±10 dB at 100 Hz.

<u>Stage/Control</u>	<u>Function</u>
HIGH filter switch S5	The high-cut off filter (R611 and C609) eliminates unwanted high-frequency components (5 kHz and higher) from the input signal when this switch is ON.

Power Amplifier Section

Preamplifier Q701, Q702	Q701 and Q702 form a paraphase amplifier but signal output is extracted from the collector circuit of Q701. This circuit has various advantages in direct coupling systems. One is high stability despite temperature variations and another is high input impedance without reducing the amplifier's gain. The ac output appears across load resistor R703 in the collector circuit of Q701. An emitter decoupling circuit is formed by the emitter-base resistance of Q702, C702 and R706 in the base circuit of Q702. This circuit forms a frequency-selective ac bypass circuit to reduce the amplifier's gain at very low frequencies. Common emitter resistor R704 keeps the dc current flow constant in Q701 and Q702, thus increasing dc stability.
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Thermal compensation and noise suppressor D701	As all the stages are directly coupled, dc stability is required. The negative temperature coefficient of D701 provides thermal compensation for the following driver stage. It also acts as a noise suppressor to reduce the popping noise due to unbalanced current flow in the following stages when the power switch is turned off.
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Driver Q703	Though this stage is a conventional flat amplifier, it determines the output voltage swings because the following stages are basically emitter-followers.
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<u>Stage/Control</u>	<u>Function</u>
Dc bias adj. (idling current) Q704, RT701	The ac load resistor for this stage is R710 (5.6k). Q704 is forced to conduct and operates as a small resistance providing the necessary forward bias on the two cascaded emitter-followers. RT701 controls the base bias of Q704, determining the impedance between the emitter and collector of Q704, and thereby controls the dc bias voltage for the following complementary circuit.
Thermal compensator for dc bias D702	The negative temperature coefficient of D702 provides thermal compensation for the complementary and power transistor circuits. D702 is attached to the power transistor's heat sink to detect temperature increases in the power transistor.
Complementary circuit Q705, Q706	These transistors operate as emitter-followers to provide the current swings demanded of the output stages and also provide the necessary phase inversion. Phase inversion is performed by using PNP and NPN type transistors.
Power transistor Q901, 902	The output transistors (Q901 and Q902) are connected directly to a power supply of about ± 36 V. Q901 supplies power to the load during the positive half cycle and Q902 operates during the negative half cycle. As all the stages are directly coupled and designed to obtain zero potential at the output terminal, the large coupling capacitor at the output (which may cause power loss or distortion at low frequencies) is eliminated.
Power Supply	
Rectifier D802, D803 D804, D805	A full-wave bridge rectifier provides a positive and a negative dc power supply for the power amplifier.

Stage/Control

Function

Ripple filter
Q707
R724, R725
C707, C708

These components reduce the ripple voltages in the dc power supply for the preamplifier and driver stages of power amplifier section to an extremely low value. Q707 and Q757 serve as an electronic filter to supply well filtered dc of about ± 33 V to each stage.

Voltage regulator
Q801, Q802
D801

Dc output from the bridge rectifier is filtered by C902 and applied to series regulator Q801. Q802 compares a sample of the output voltage picked off across R805 with reference voltage supplied by voltage stabilizer

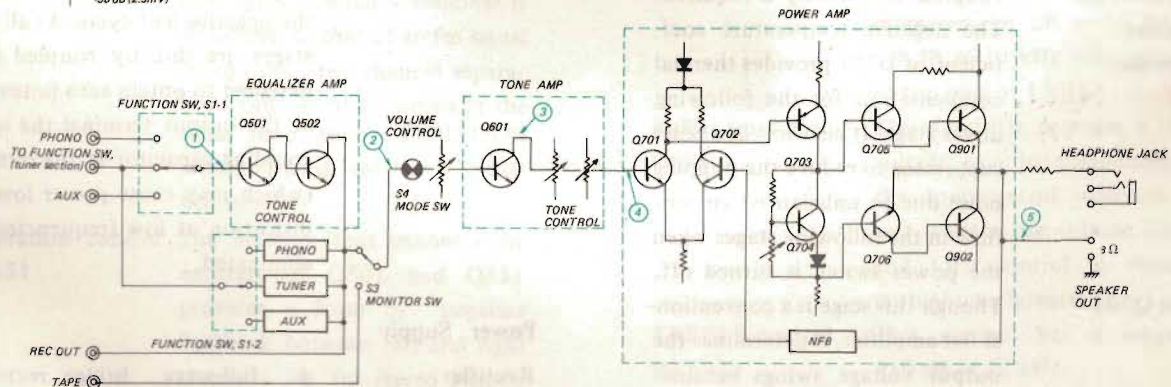
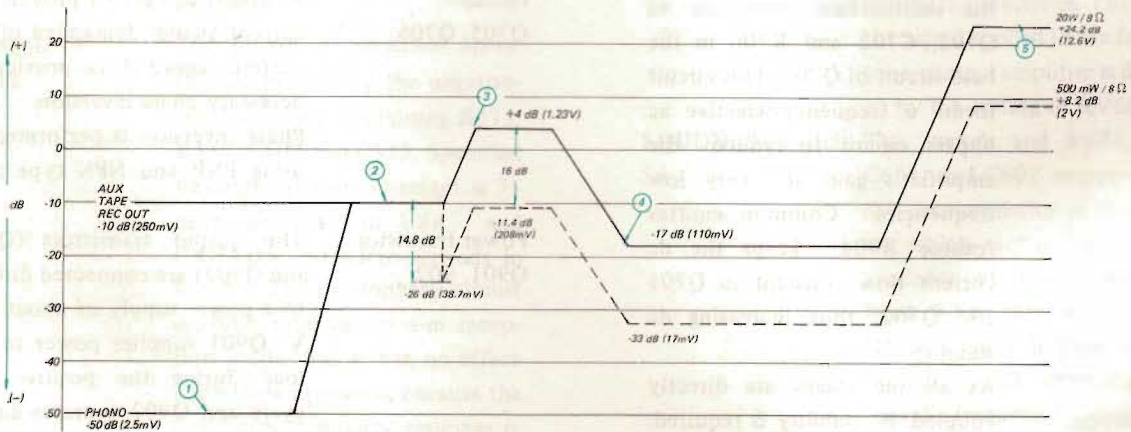
Stage/Control

Function

D801. A change in output voltage is detected at the base of Q802 and therefore alters its collector voltage.

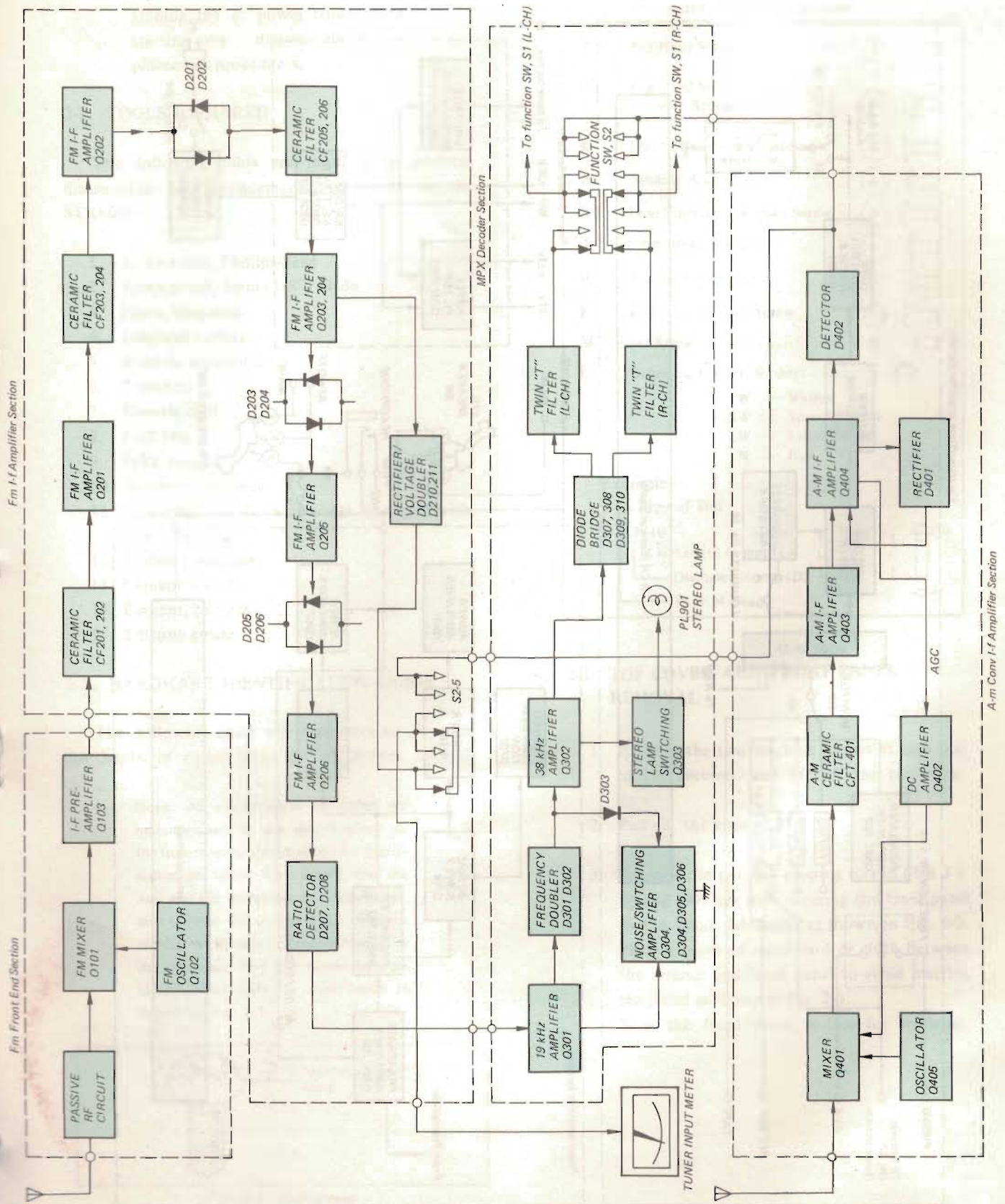
Since the collector of Q802 is directly coupled to the base of Q801, the change in output voltage alters the conduction of Q801 by the amount necessary to maintain the output voltage constant. An increase in output voltage causes an increase in the impedance (decrease in conduction) of Q801, and vice versa. The dc output voltage supplied to the tuner section is therefore externally stable.

i-3. LEVEL DIAGRAM

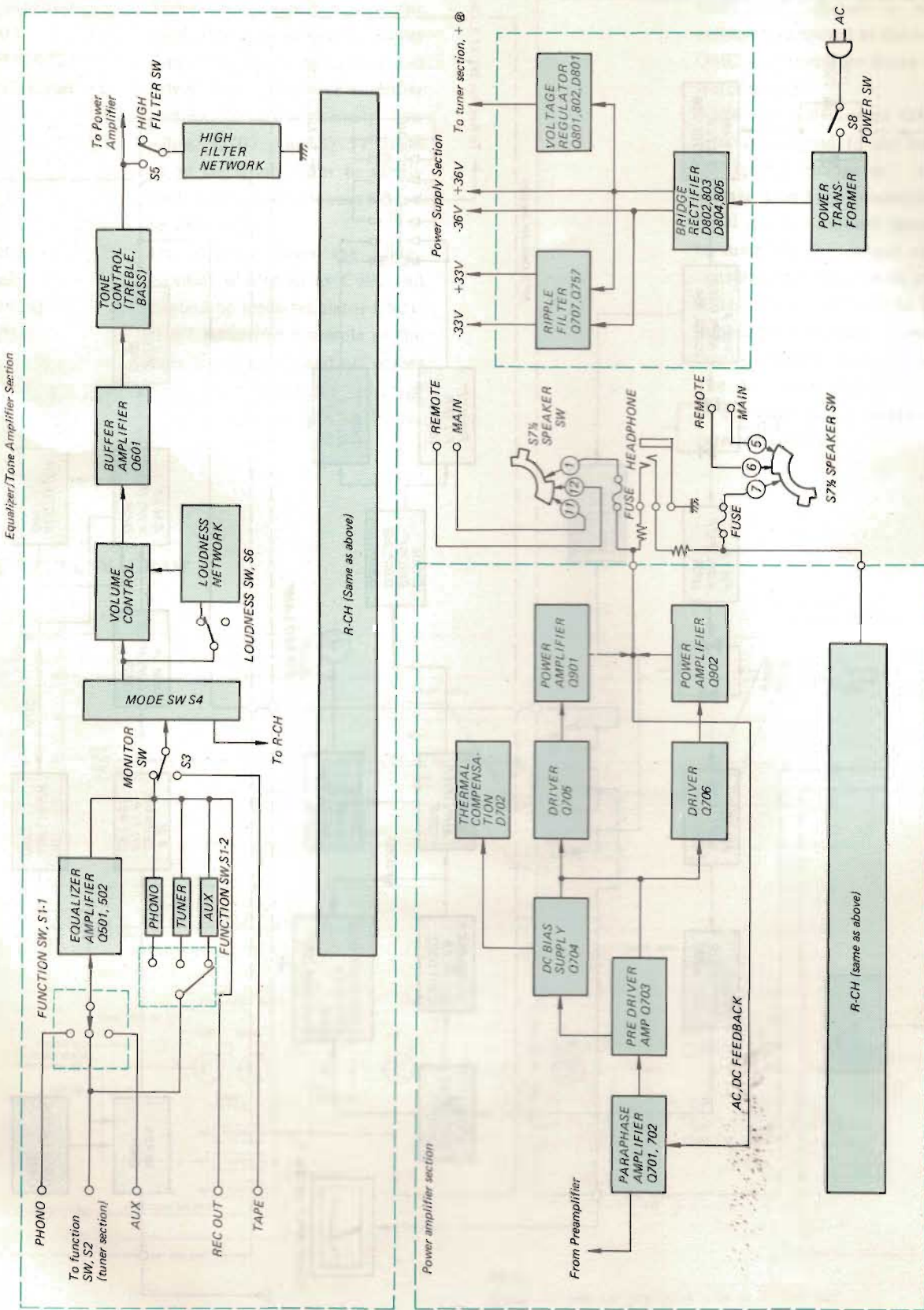


Note :
Signal voltages are measured with ac VTVM and expressed in dB referred to 0.775V, 1kHz.

1-4. BLOCK DIAGRAM—Tuner Section



1-5. BLOCK DIAGRAM—Audio Section



SECTION 2

DISASSEMBLY AND REPLACEMENT PROCEDURES

WARNING

Unplug the ac power cord before starting any disassembly or replacement procedures.

2-1. TOOLS REQUIRED

The following tools are required to perform disassembly and replacement procedures on the STR6045.

1. Screwdriver, Phillips-head
2. Screwdriver, 3mm (1/8") blade
3. Pliers, long-nose
4. Diagonal cutters
5. Wrench, adjustable
6. Tweezers
7. Electric drill
8. Drill bits
9. Prick punch
10. Hammer, ball-peen
11. Soldering iron, 40 to 50 watts, equipped with solder sucker
12. Solder, rosin core
13. Cement solvent
14. Cement, contact
15. Silicone grease

2-2. HARDWARE IDENTIFICATION GUIDE

The following chart will help you to decipher the hardware codes given in this service manual.

Note: All screws in the STR-6045 are manufactured to the specifications of the International Organization for Standardization (ISO). This means that the new and old screws are not interchangeable because ISO screws have a different number of threads per mm compared to the old ones. The ISO screws have an identification mark on their heads as shown in Fig. 2-1.

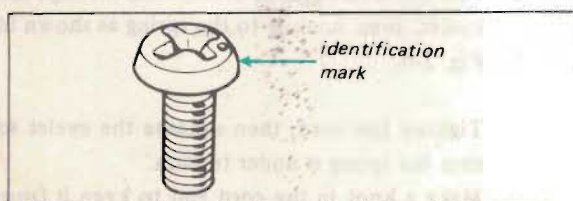


Fig. 2-1 ISO screw

Hardware Nomenclature

P	Pan Head Screw		
PS	Pan Head Screw with Spring Washer		
K	Flat Countersunk Head Screw		
B	Binding Head Screw		
RK	Oval Countersunk Head Screw		
T	Truss Head Screw		
R	Round Head Screw		
F	Flat Fillister Head Screw		
SC	Set Screw		
E	Retaining Ring (E Washer)		
	W	Washer	
	SW	Spring Washer	
	LW	Lock Washer	
	N	Nut	

-- Example --

Type of Slot

⊕ P 3x10

Length in mm (L)

Diameter in mm (D)

Type of Head

-D- -D-

2-3. TOP COVER AND FRONT PANEL REMOVAL

1. Remove the two machine screws at each side of the receiver, and lift off the top cover.
2. Pull all the knobs off.
3. Remove the two self-tapping screws (\oplus 3 X 6) and two hex nuts securing the front panel to the front subchassis as shown in Fig. 2-2. Place a piece of cardboard or cloth between the wrench and front panel to avoid marring the panel as shown in Fig. 2-3. Now the front panel is free for servicing.

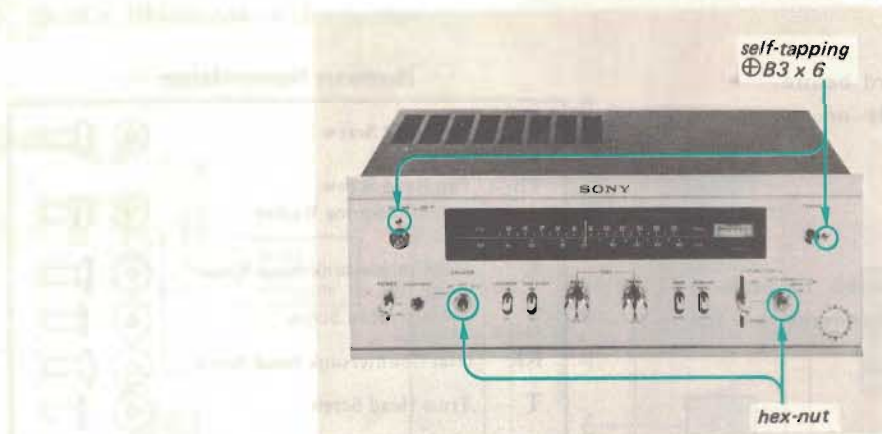
SECTION 2
DISASSEMBLY AND REPLACEMENT PROCEDURES

Fig. 2-2 Front panel removal

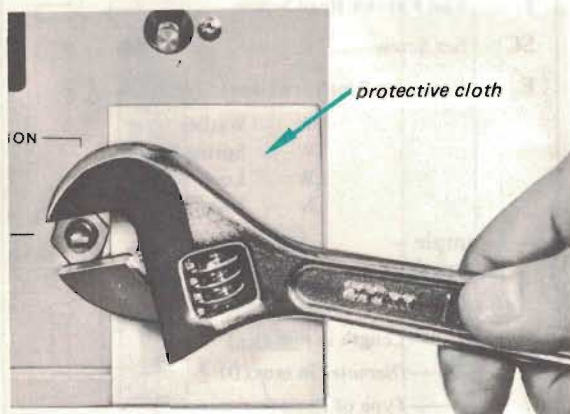


Fig. 2-3 Hex nut removal

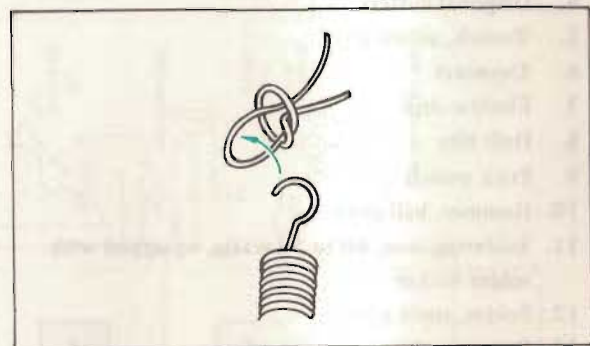


Fig. 2-4 Tying a square knot to the coil spring

2-4. DIAL-CORD RESTRINGING

Preparation

1. Remove the top cover as described in Procedure 2-3.
2. Cut a 1500 mm (59") length of dial cord.
3. Tie the end of the cord to a spring as shown in Fig. 2-4.
4. Rotate the tuning-capacitor drive drum fully clockwise (minimum capacitance position).

Procedure

While referring to Fig. 2-5, proceed as follows:

1. Hook the spring to one hole of the drive drum as shown in Fig. 2-6.

2. Run the cord through the slot in the rim of the drum and wrap a half clockwise turn in the inner side groove.
3. Run the cord over pulley "A", and then wrap two counterclockwise turns around the tuning shaft.
4. Run the cord over pulleys "B", "C" and "D" then wrap two clockwise turns around the drum from outer groove to inner groove as shown in Fig. 2-7.
5. Pass the doubled end of the cord through the eyelet, then hook it to the spring as shown in Fig. 2-8.
6. Tighten the cord, then squeeze the eyelet so that the spring is under tension. Make a knot in the cord end to keep it from slipping out of the eyelet.

- 7. After completing the dial-cord stringing, make sure that the tuning system works properly. Apply a drop of contact cement to the finish point.

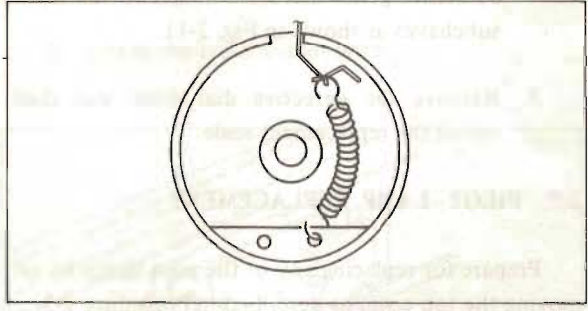


Fig. 2-6 Coil spring installation

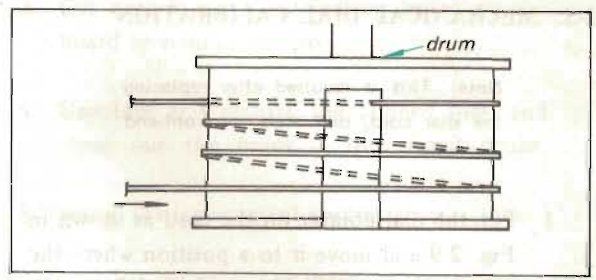


Fig. 2-7 Wrapping the dial cord

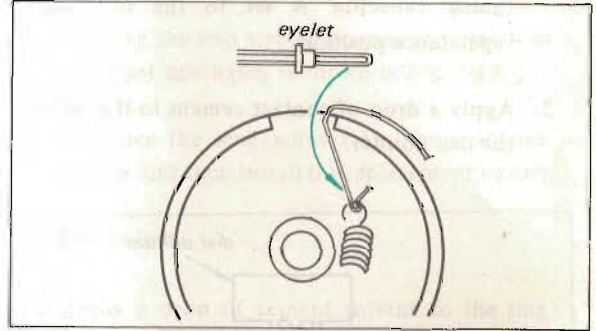


Fig. 2-8 Finishing dial cord stringing

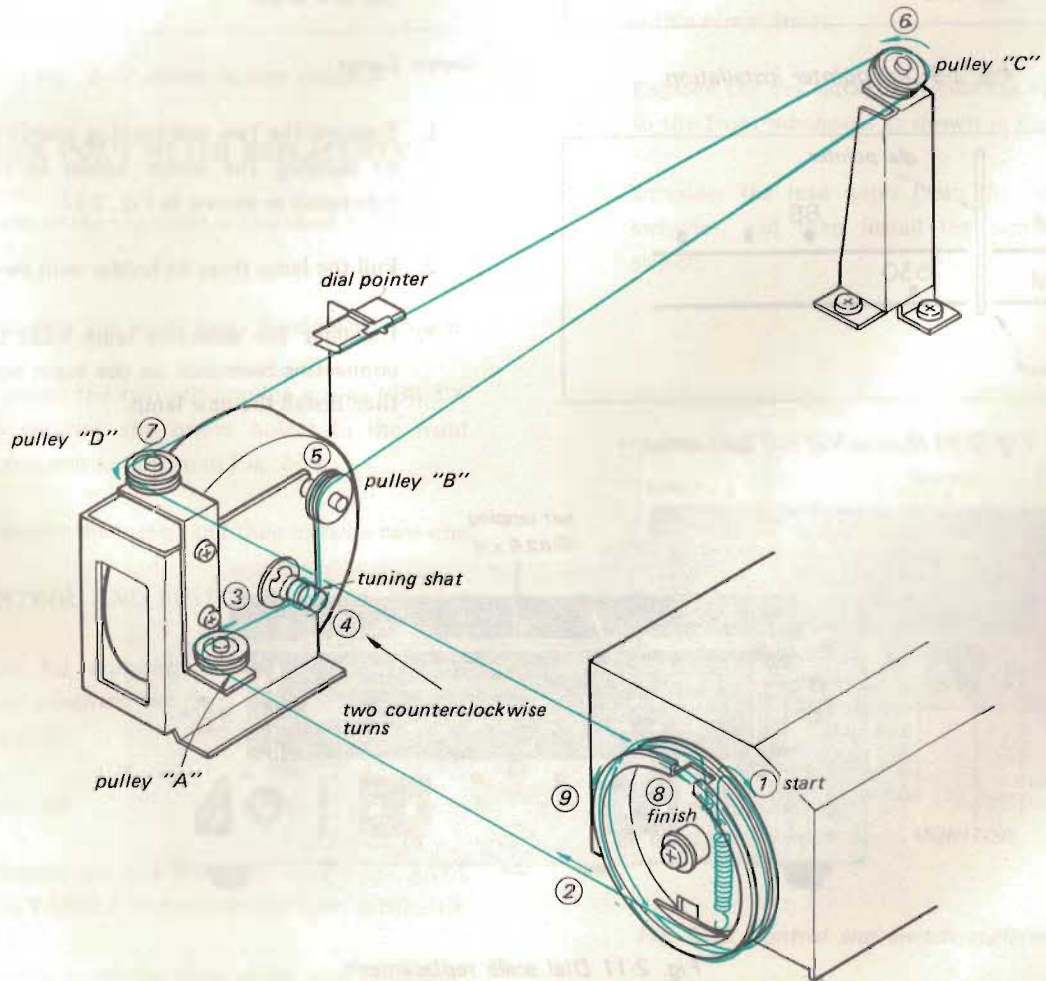


Fig. 2-5 Dial cord stringing

2-5. MECHANICAL DIAL CALIBRATION

Note: This is required after replacing the dial cord, dial scale or front-end assembly.

1. Put the dial pointer on the cord as shown in Fig. 2-9 and move it to a position where the pointer coincides with the left slot on the dial scale as shown in Fig. 2-10, when the tuning capacitor is set to the maximum capacitance position.
2. Apply a drop of contact cement to the tab of the dial pointer.

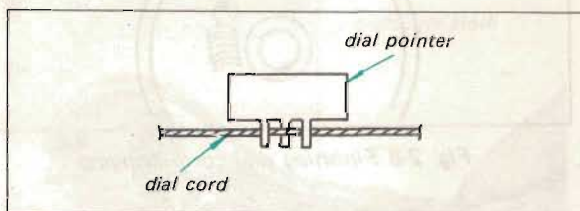


Fig. 2-9 Dial pointer installation

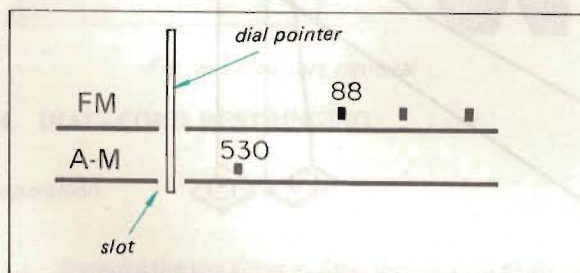


Fig. 2-10 Mechanical dial calibration

2-6. DIAL SCALE REPLACEMENT

1. Remove the top cover and front panel as described in Procedure 2-3.
2. Remove the two self-tapping screws ($\oplus B 2.6 \times 6$) securing the dial-scale holder to the front subchassis as shown in Fig. 2-11.
3. Remove the defective dial scale, and then install the replacement scale.

2-7. PILOT-LAMP REPLACEMENT

Prepare for replacing any of the pilot lamps by removing the top cover as described in Procedure 2-3.

Meter Lamp

1. Pull out the meter-lamp socket, and then unscrew the lamp from the socket and install the new lamp.

Stereo Lamp

1. Remove the two self-tapping screws ($\oplus B 3 \times 6$) securing the meter holder to the front subchassis as shown in Fig. 2-12.
2. Pull the lamp from its holder with tweezers.
3. Unsolder the defective lamp leads from the connecting terminals on the tuner board, and then install the new lamp.



Fig. 2-11 Dial scale replacement

Dial Lamp

1. Remove the front panel as described in Procedure 2-3.
2. Pry out the fiber lamp shade, and then remove the lamp.
3. Install the replacement lamp.

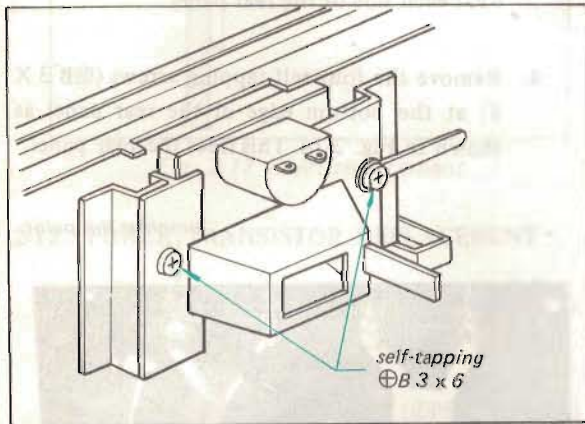


Fig. 2-12 Meter holder removal

2-8. TUNER INPUT METER REPLACEMENT

1. Remove the top cover as described in Procedure 2-3.
2. Unsolder the leads from the defective meter.
3. Remove the two self-tapping screws ($\oplus B 3 \times 6$) securing the meter holder to the front subchassis as shown in Fig. 2-12.
4. Remove the meter, and then install a new one.

2-9. CONTROL AND SWITCH REPLACEMENT

Prepare for replacing any of the controls or switches by removing the front panel as described in Procedure 2-3.

TONE Controls

1. Remove the hex nuts that secure the BASS and TREBLE controls to the front subchassis.
2. Carefully remove them along with the tone control circuit board.

3. Cut each lug of the defective control on the board to remove the part.
4. Unsolder and remove the clipped lugs, and clean out the holes in the circuit board.
5. Install the replacement control.

POWER, HIGH FILTER, LOUDNESS, MONITOR, MODE FUNCTION (1) Switches

1. Remove the two screws securing the switch to the front subchassis as shown in Fig. 2-13.
2. Unsolder the lead wires from the defective switch, and then install the replacement switch.

SPEAKER Switch

1. Apply a drop of cement solvent to the ring spacer on the switches. Wait a few second for the cement to dissolve, and pry out the spacer with a screw driver.
2. Remove the hex nuts that secure the switches to the front-subchassis as shown in Fig. 2-13.
3. Unsolder the lead wires from the defective switches, and then install the replacement switch.

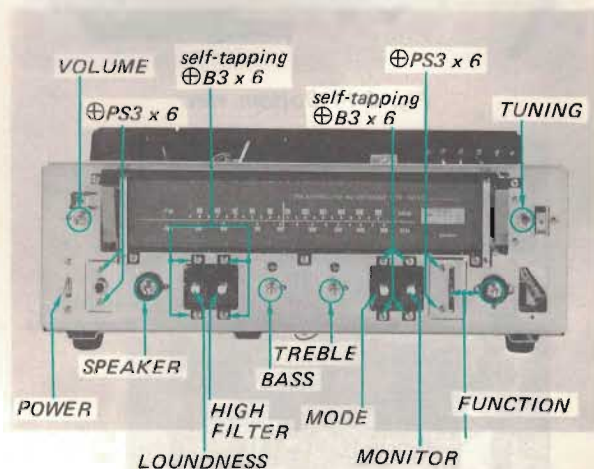


Fig. 2-13 Control and switch replacement

FUNCTION (2) switch (slide/rotary switch) REPLACEMENT

1. Apply a drop of cement solvent to the ring spacer on the switch. Wait a few second for the cement to dissolve and pry out the spacer with a screw driver.
2. Remove the six self-tapping screws ($\oplus B 3 \times 6$) securing bottom masking plate as shown in Fig. 2-14 and then remove the mask.
3. Remove the hex nut securing the switch to the front subchassis.
4. With a soldering-iron having a solder-sucking tip, clean the solder from each lug of the defective switch and the printed board, as shown in Fig. 2-15. This frees the switch.
5. Install the replacement switch.

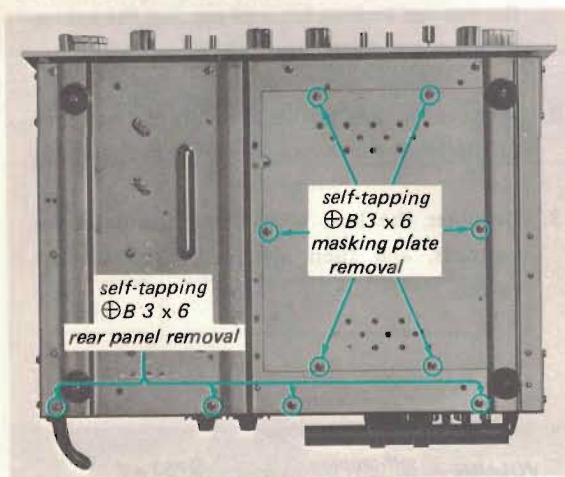


Fig. 2-14 Bottom view

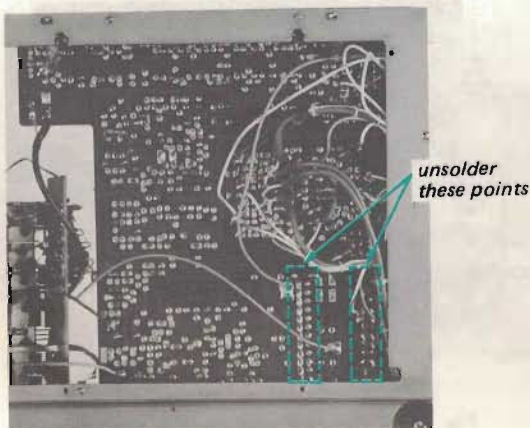


Fig. 2-15 FUNCTION (2) switch removal

2-10. REAR PANEL REMOVAL

1. Remove the top cover and bottom plate as described in Procedure 2-3.
2. Unsolder the braided wire connecting between the ground terminal and chassis as shown in Fig. 2-16.
3. Remove the two self-tapping screws ($\oplus B 3 \times 6$) at each side of the rear panel.
4. Remove the four self-tapping screws ($\oplus B 3 \times 6$) at the bottom edge of the rear panel as shown in Fig. 2-14. This frees the rear panel.

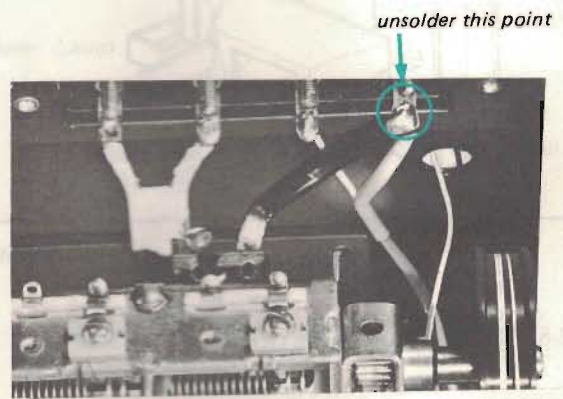


Fig. 2-16 Preparation for rear panel removal

2-11. REPLACEMENT OF COMPONENTS SECURED TO THE REAR PANEL BY RIVETS

1. Remove the rear panel as described in Procedure 2-10.
2. Bore out the rivets using a drill bit slightly larger in diameter than the rivet. See Fig. 2-17.
3. Punch out the remainder of the rivet with a nail set or prick punch.
4. Remove the defective component, and then install a new one.
5. Secure the new component with a suitable screw and nut, or a repair rivet screw (part number 3-701-402).

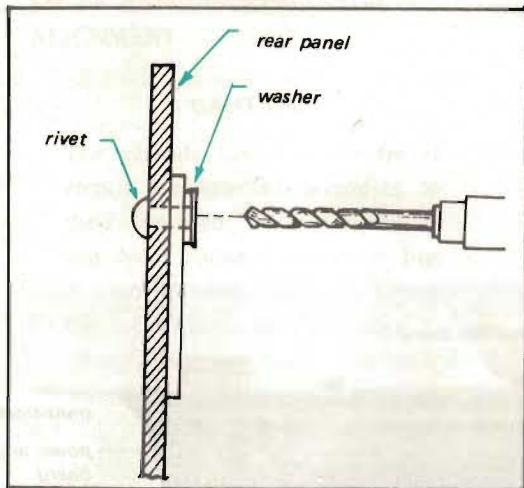
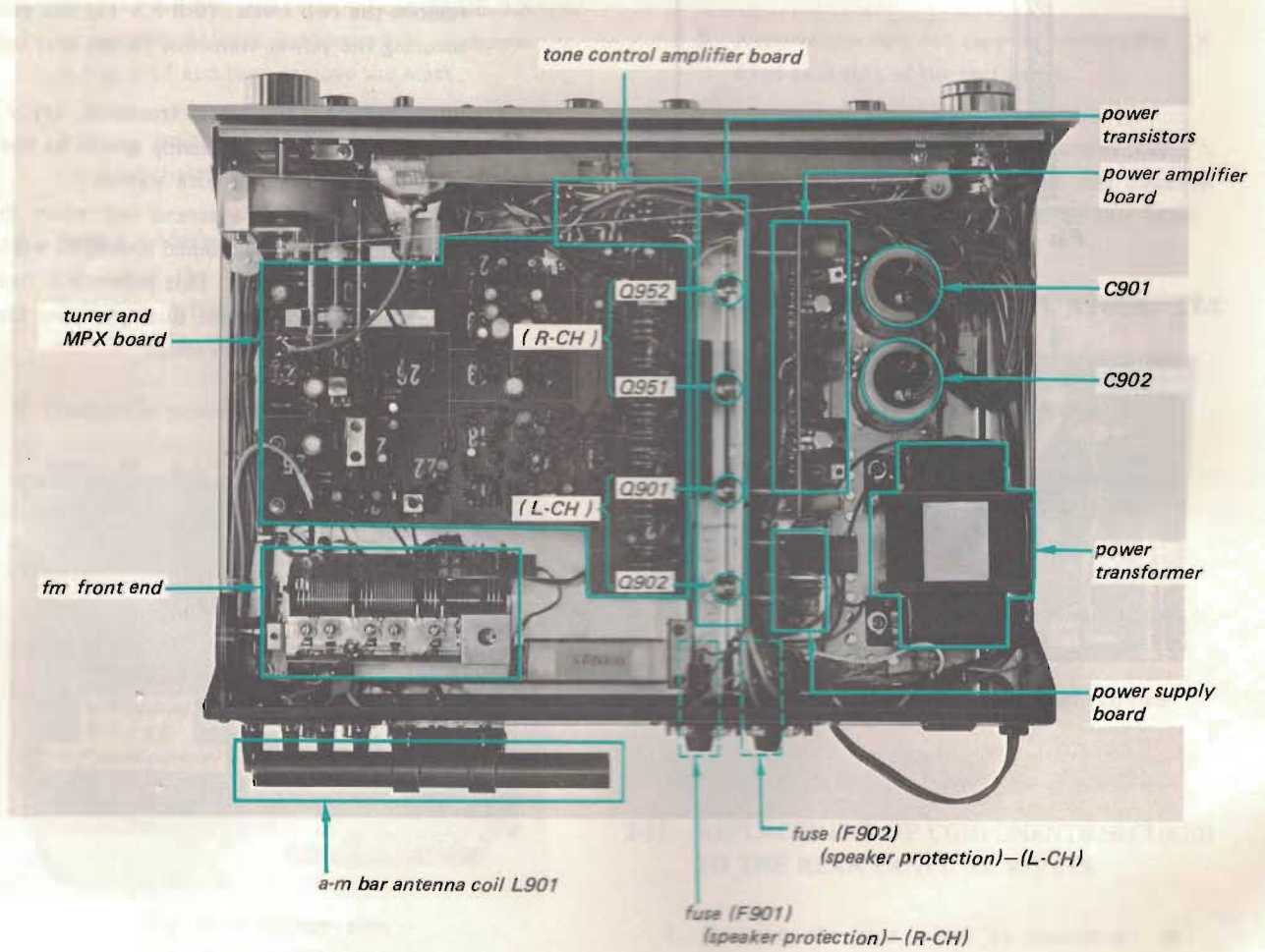


Fig. 2-17 Rivet replacement

2-12. POWER TRANSISTOR REPLACEMENT

1. Remove the top cover as described in Procedure 2-3.
2. Remove the four screws (\oplus PSW 3 \times 6) securing the power supply board and power amplifier board to the heat sink.
3. Remove the four self-tapping screws (\oplus B 3 \times 6) securing heat sink to the chassis. Cut the emitter and base leads of the defective power transistor with a diagonal cutter. This prevents a eventual mica washer damage when removing the defective power transistor.
4. Carefully pull out the heat sink, and then remove the two screws (\oplus B 3 \times 12) and nuts securing the power transistor to the heat sink.
5. When replacing the power transistor, apply a coating of a heat-transferring grease to both sides of the insulating mica washer. Any excess grease squeezed out when the mounting bolts are tightened should be wiped off with a clean cloth. This prevents it from accumulating conductive dust particles that might eventually cause a short.

2-13. CHASSIS LAYOUT



SECTION 3 ALIGNMENT AND ADJUSTMENT PROCEDURES

3-1. FM I-F AND DISCRIMINATOR ALIGNMENT

CAUTION

The ceramic filters in the fm i-f circuit are selected according to their specified center frequencies and color coded as shown in Fig. 3-1 and listed in Table 3-1. Check the color code of the filters to identify the same center frequency when replacing any of these filters.

TABLE 3-1.
FM I-F CERAMIC FILTERS

Part No.	Color	Specified Center Freq.
1-403-562-11	red	10.70 MHz
1-403-562-12	black	10.66 MHz
1-403-562-31	white	10.74 MHz
1-403-562-41	green	10.62 MHz
1-403-562-51	yellow	10.78 MHz

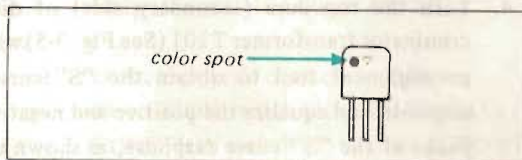


Fig. 3-1 Fm i-f ceramic filter

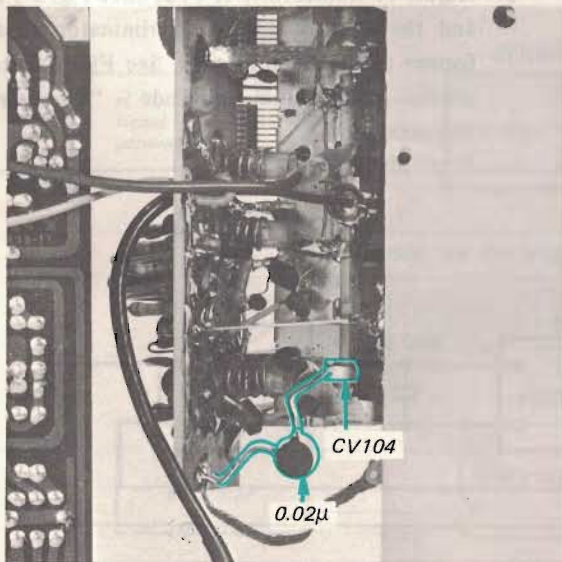


Fig. 3-2 Interruption of fm local oscillator operation

Note: Two methods of i-f discriminator alignment are available, sweep generator alignment and signal generator alignment. You can use either of them. In either case, the local oscillator should be killed. To stop the local oscillator's operation, remove the masking plate at the bottom of the chassis, and then shunt the oscillator capacitor with a $0.02\mu\text{F}$ capacitor. See Fig. 3-2.

Sweep Generator Alignment

Test Equipment Required

1. 10.7 MHz sweep generator
2. Oscilloscope
3. Ceramic capacitor $0.02\mu\text{F}$
4. Alignment tools

Preparation

1. Remove the top cover and masking plate at the bottom.
2. Solder a $0.02\mu\text{F}$ capacitor across C215, and then connect the input cable of the oscilloscope with alligator clips to it as shown in Fig. 3-3.
3. Connect the output cable of the sweep generator across CV103. Use alligator clips and make the connection through a $0.02\mu\text{F}$ coupling capacitor as shown in Fig. 3-4.

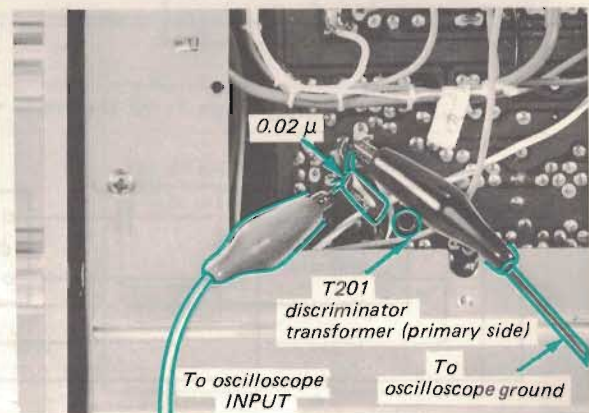


Fig. 3-3 Fm discriminator output connection

SECTION 3
ALIGNMENT AND ADJUSTMENT PROCEDURES

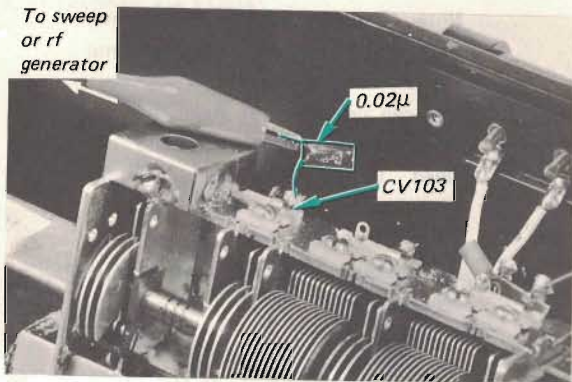


Fig. 3-4 Fm i-f signal injection

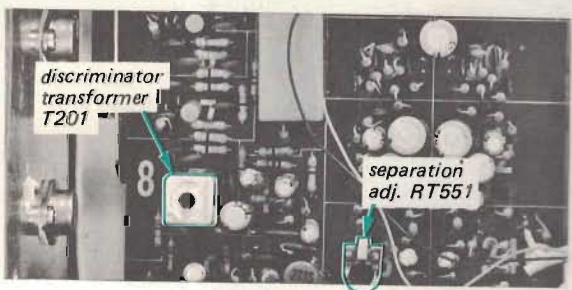


Fig. 3-5 Parts location

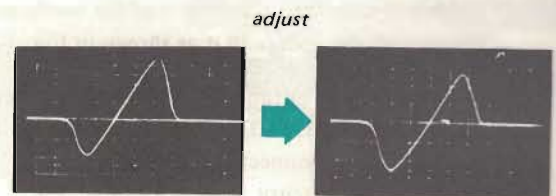


Fig. 3-7 "S" curve response

Procedure

1. With the equipment connected as shown in Fig. 3-6, set the sweep generator's controls as follows:
 - Center frequency . . . Specified frequency of ceramic filter, see table 3-1.
 - Sweep width 1 MHz
2. Set the tuner's controls as follows:
 - FUNCTION switch (1) . . . FUNCTION (2)
 - FUNCTION switch (2) . . . FM AUTO STEREO
3. Adjust the oscilloscope controls to provide a visible indication.

Note: Two or three traces will be observed on the oscilloscope as the center frequency of the sweep generator varies. The trace you are looking for has the largest amplitude. Once you get it, decrease the sweep generator output low enough to obtain rather noisy output.
4. Turn the top core (secondary side) of discriminator transformer T201 (See Fig. 3-5) with an alignment tool to obtain the "S" curve response, and equalize the positive and negative peaks of the "S" curve response, as shown in Fig. 3-7.
5. Adjust i-f transformer IFT101 (See Fig. 3-14) and the primary side of discriminator transformer (T201 bottom core, See Fig. 3-3) to obtain a maximum-amplitude "S" curve response.

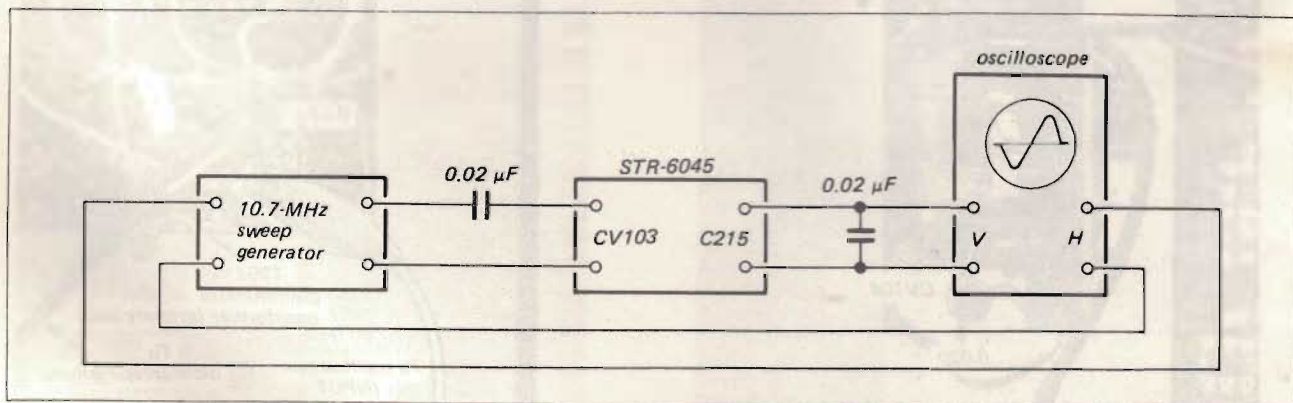


Fig. 3-6 Test setup for discriminator alignment by sweep generator

6. Change the signal generator's modulation to fm, 400 Hz 100%.
7. Turn the core of fm IFT 101 and bottom core of T201 (See Fig. 3-3 and Fig. 3-14), to obtain the maximum output.
8. Repeat the above mentioned procedures two or three times.

3-2. FM FREQUENCY COVERAGE ALIGNMENT

CAUTION

Never attempt alignment of the front-end section except for the frequency-coverage and dial-calibration adjustments. The front end section of the tuner has been carefully adjusted at the factory, so very little adjustment is necessary in the field. Alignment need not be performed when the front-end FET is replaced since changes in FET parameters have little effect upon tuning. If an rf-stage adjustment is required, ask your nearest SONY Service Station to send your unit to the Factory Service Center for a complete front-end alignment. Exercise caution when returning the faulty unit so that it is not damaged in transit. The warranty will not cover damage incurrent in transit to the Factory Service Center.

Note: Before starting this alignment, the discriminator transformer alignment should be performed.

Test Equipment Required

1. Standard fm signal generator
2. Ac VTVM
3. Alignment tools

Preparation

1. Remove the top cover as described in Procedure 2-3.
2. Connect the equipment as shown in Fig. 3-10.
3. Set the receiver's controls as follows:
 FUNCTION (1) switch . . . FUNCTION (2)
 FUNCTION (2) switch . . . FM AUTO
 STEREO

Generator Alignment

Follow the procedures given in Table 3-2 when performing this alignment with an fm signal generator. Be sure that the dial is mechanically calibrated.

Off-the-Air Alignment

Accurate dial calibration and a frequency-coverage test can also be performed by utilizing off-the-air local fm signals. However, before performing the following procedures, be sure that the dial is mechanically calibrated. See Procedure 2-5.

TABLE 3-2. FM FREQUENCY COVERAGE ALIGNMENT

Step	Coupling Between Front End and SSG	SSG Frequency and Output Level	Dial Indication	Scope Connection	Adjust	Indication
1.	Direct coupling	87.5 MHz 400 Hz 100 % Mod. 10 μ V (20 dB)	87.5 MHz	REC OUT jack (J904)	OSC coil L104 See Fig. 3-14.	Maximum VTVM reading
2.	Same as above	108 MHz 400 Hz 100 % Mod. 10 μ V (20 dB)	108 MHz	Same as above	OSC trimmer CT104 See Fig. 3-14	Same as above

Procedure

1. Tune the set to the lowest-frequency station.
2. Check the dial scale for a calibration accuracy of ± 300 kHz from the carrier frequency of the station. If the dial-accuracy deviation exceeds this limit, turn the local-oscillator coil L104 (as shown in Fig. 3-14) slightly until optimum calibration is obtained.
3. Tune the set to the highest-frequency station in your locality. If the dial-calibration error is excessive, adjust local-oscillator trimmer CT104 to obtain maximum calibration accuracy. See Fig. 3-14.

- (1) With the equipment connected as shown in Fig. 3-11, set the MPX and audio oscillator's controls as follows:
 MAIN CHANNEL OFF
 SUB CHANNEL ON
 PILOT (19 kHz) OFF
 AUDIO OSCILLATOR
 OUTPUT 400 Hz, 250 mV
- (2) Adjust the oscilloscope controls to obtain a visible indication. Be sure the scope's horizontal display switch is set for external input.
- (3) Turn the pilot-signal (19 kHz) phase control to obtain an in-phase and stable lissajous pattern as shown in Fig. 3-12.

3-3. FM STEREO SEPARATION ADJUSTMENT

Test Equipment Required

1. MPX generator
2. Fm signal generator
3. Audio oscillator
4. Ac VTVM
5. Oscilloscope
6. Alignment tools

Preparation

Before starting the stereo-separation adjustment, check and adjust the phase between the 19-kHz pilot signal and the sub-channel signal in the MPX stereo generator as follows:

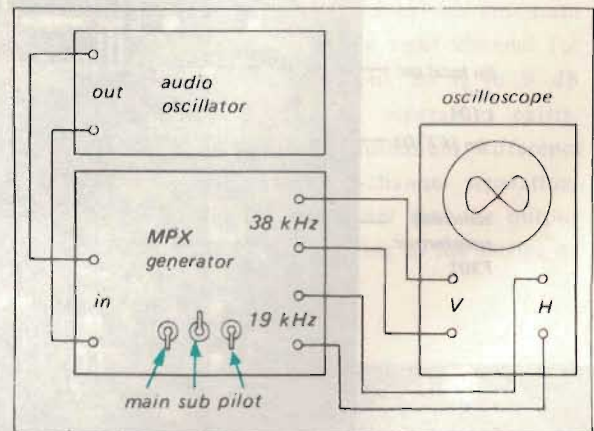


Fig. 3-11 Test setup for the MPX generator preadjustment

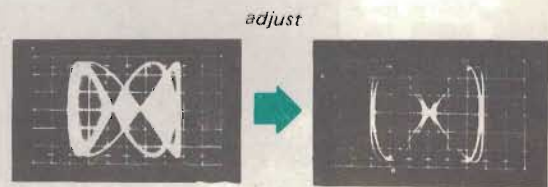


Fig. 3-12 Lissajous pattern

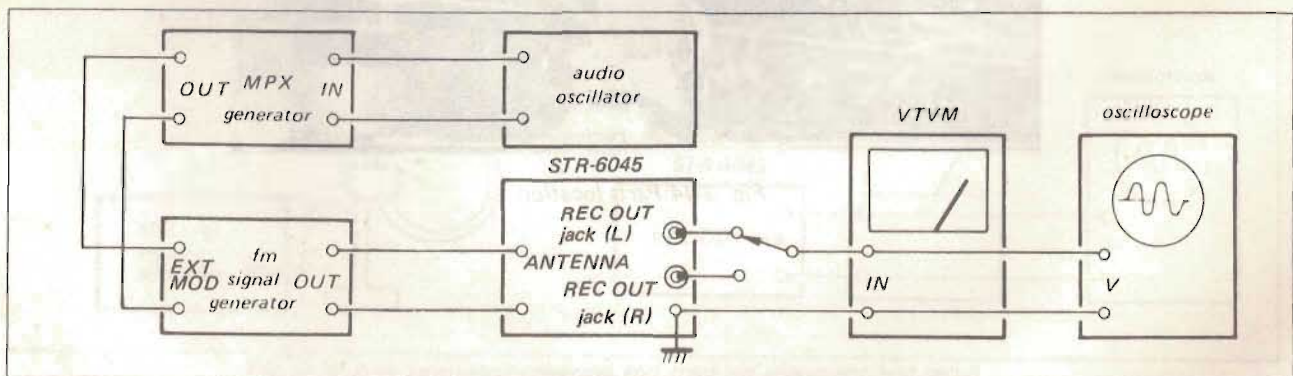


Fig. 3-13 Stereo separation adjustment test setup

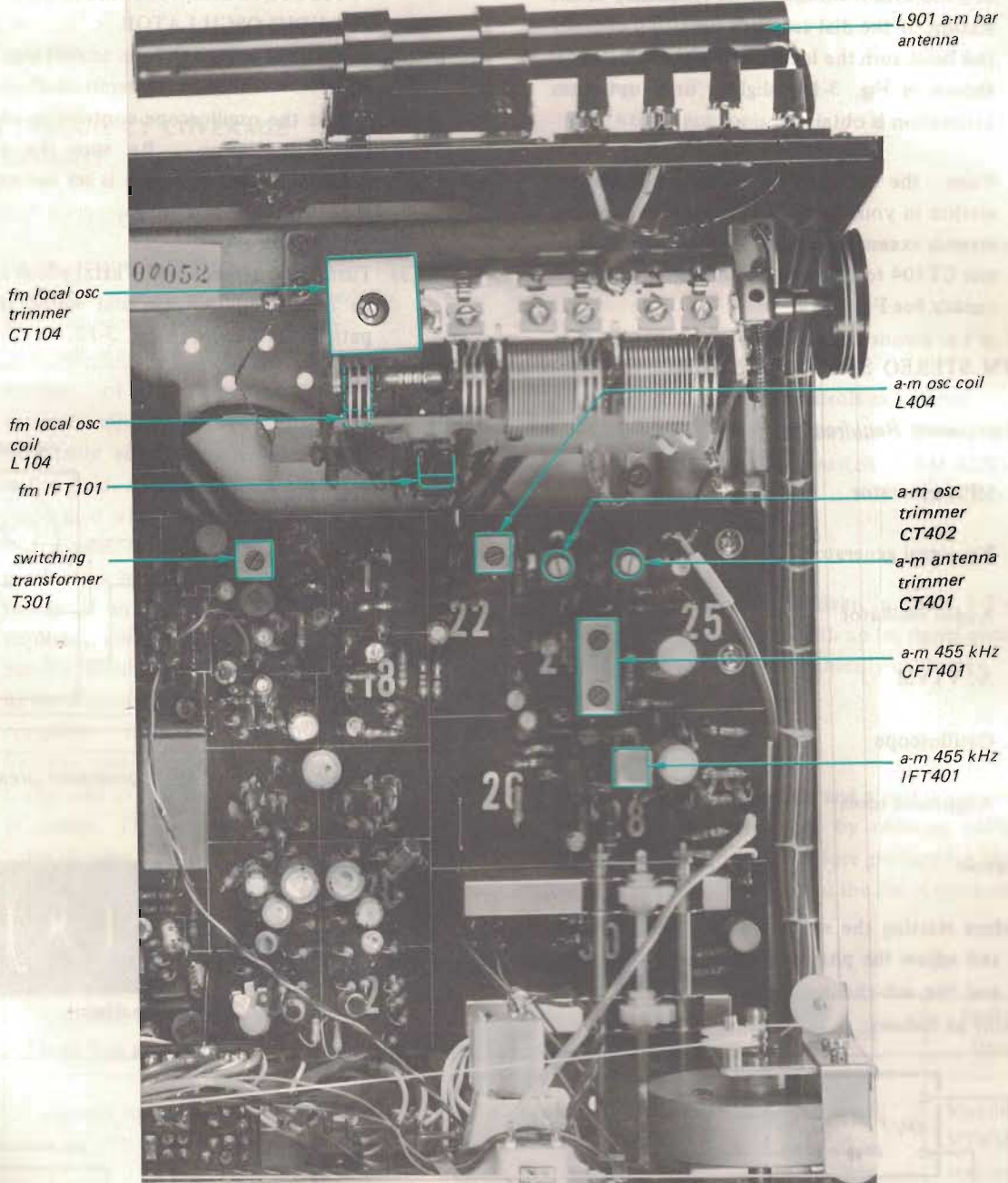


Fig. 3-14 Parts location

Procedure

1. Connect the equipment as shown in Fig. 3-13. Set the fm signal-generator's control as follows:
 - Carrier frequency 98 MHz
 - Output level 1,000 μ V (60 dB)

Modulation:

 - Main channel (400 Hz) . . . 33.75 kHz (45%)
 - Sub channel (38 kHz) . . . 33.75 kHz (45%)
 - Pilot (19 kHz) 7.5 kHz (10%)

The above mentioned modulation levels can be set as follows:

- (a) With the equipment connected as shown in Fig 3-13 set the MPX stereo generator controls as follows:

MAIN CHANNEL OFF
 SUB CHANNEL OFF
 PILOT (19 kHz) ON

- (b) Adjust the 19-kHz signal level to obtain a 7.5-kHz deviation on the FM SSG modulation indicator.

- (c) Reset the MPX stereo-generator's controls as follows:

MAIN CHANNEL ON
 SUB CHANNEL OFF
 PILOT (19 kHz) OFF
 INPUT SELECTOR L-CH

- (d) Adjust the audio-oscillator output (400 Hz) to obtain a 33.75-kHz deviation on the FM SSG modulation indicator.

- (e) Set all controls to their ON position.

2. Precisely tune the set to the SSG's carrier frequency, then turn the top core of switching transformer T301 to obtain maximum output at the left channel. See Fig. 3-14. Note that this adjustment has a close relationship with stereo distortion.
3. Record the output level of the left channel when the MPX generator's input selector is set to the left channel.
4. Switch the input selector to the right channel and read the residual signal level in the left channel.
5. The output-level to residual-level ratio represents the separation. Adjust separation adj. control RT551 (See Fig. 3-15) for minimum residual level. Check the right channel for separation. Usually, about an 8 to 9 dB difference in channel separation exists. Readjust RT551 for minimum difference between left-and right-channel separation. While doing this, remember that the output level also changes according to the setting of RT551.

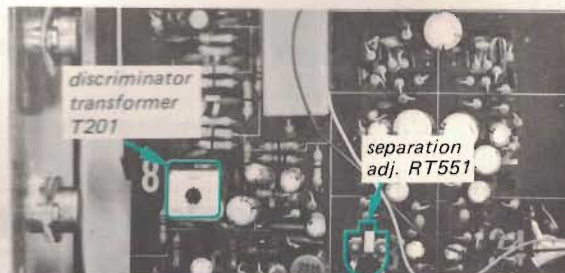


Fig. 3-15 Parts location

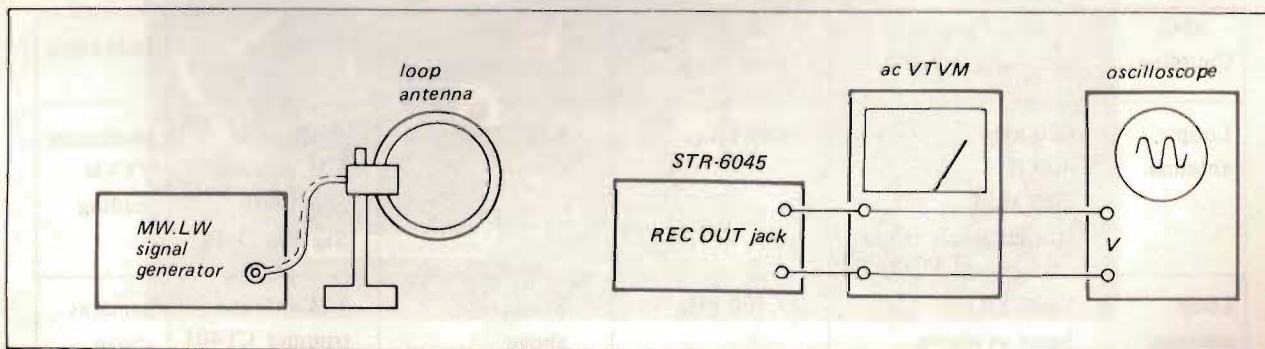


Fig. 3-16 A-m frequency coverage and tracking alignment test setup

3-4. A-M I-F STRIP ALIGNMENT

Note: The i-f transformers (CFT-401 and IFT-401) in the a-m i-f circuit are adjusted at the factory, so very little adjustment is necessary in the field. There is no need for alignment when replacing any of these i-f transformers.

3-5. FREQUENCY COVERAGE AND TRACKING ALIGNMENT

Preparation

Remove the top cover as described in Procedure 2-3. Then, set the receiver's FUNCTION switch to AM.

Signal generator Method

Test Equipment Required

1. Signal generator

2. Loop antenna

3. Ac VTVM

Procedure

With the equipment connected as shown in Fig. 3-16, follow the procedures given in Table 3-3 and 3-4 when performing this alignment with an a-m signal generator.

Off-the-Air Signal Method

Accurate dial calibration, and a frequency-coverage and tracking test can also be performed by utilizing off-the-air local a-m signals. However, before performing the following procedure, be sure that the dial is mechanically calibrated. See Procedure 2-5.

TABLE 3-3. A-M FREQUENCY COVERAGE ALIGNMENT

SSG Coupling	SSG Frequency and Output Level	Dial Indication	Scope Connection	Adjust	Indication
Loop antenna	530 kHz 400 Hz 30% Mod. 10,000 μ V (80 dB)	530 kHz	REC OUT jack (J904)	A-M OSC coil L404 See Fig. 3-14	Maximum VTVM reading
Loop Antenna	1,600 kHz Same as above	1,600 kHz	Same as above	A-M OSC trimmer CT402 See Fig. 3-14	Same as above

TABLE 3-4. A-M TRACKING ALIGNMENT

SSG Coupling	SSG Frequency and Output Level	Dial Indication	Scope Connection	Adjust	Indication
Loop antenna	620 kHz 400 Hz 30% Mod Output level; as low as possible	620 kHz	REC OUT jack (J904)	Position of A-M antenna coil L901 See Fig. 3-14	Maximum VTVM reading
Loop antenna	1,400 kHz Same as above	1,400 kHz	Same as above	A-M antenna trimmer CT401 See Fig. 3-14	Same as above

Frequency Coverage Alignment

1. Tune the receiver to the lowest-frequency station in your locality. If the dial-calibration error is excessive, turn the local oscillator-coil L404 (see Fig. 3-14) slightly until optimum dial calibration is obtained.
2. Tune the receiver to the highest-frequency station in your locality. If the dial-calibration error is excessive, adjust local-oscillator trimmer-capacitor CT404 (see Fig. 3-14) to obtain maximum calibration accuracy.

Tracking Alignment

1. Tune the set to the station whose carrier frequency is closest to 620 kHz and adjust the position of antenna coil L402 as shown in Fig. 3-14 to obtain maximum output.
2. Tune the set to the station whose carrier frequency is closest to 1,400 kHz and adjust antenna trimmer CT402 to obtain maximum output. See Fig. 3-14.
3. Repeat the above steps two or three times.

3-6. POWER AMPLIFIER ADJUSTMENT

Note: This adjustment should be performed after replacing any of the power transistors.

Dc-Bias Adjustment

Serious deficiencies in performance, such as thermal runaway of power transistors, will result if this adjustment is improperly set.

CAUTION

To avoid accidental power transistor damage, increase the ac line voltage gradually, using a variable transformer, while measuring the voltage across emitter resistors R722 (R772) of power transistors alternately as shown in Fig. 3-17); Check to see that the reading does not exceed 25 mV. If it does, turn off the power as soon as possible, then check and repair the trouble in the power-amplifier board.

Test Equipment Required

1. Dc millivoltmeter : Capable of measuring dc voltage of 100 mV or less.
2. Variable transformer

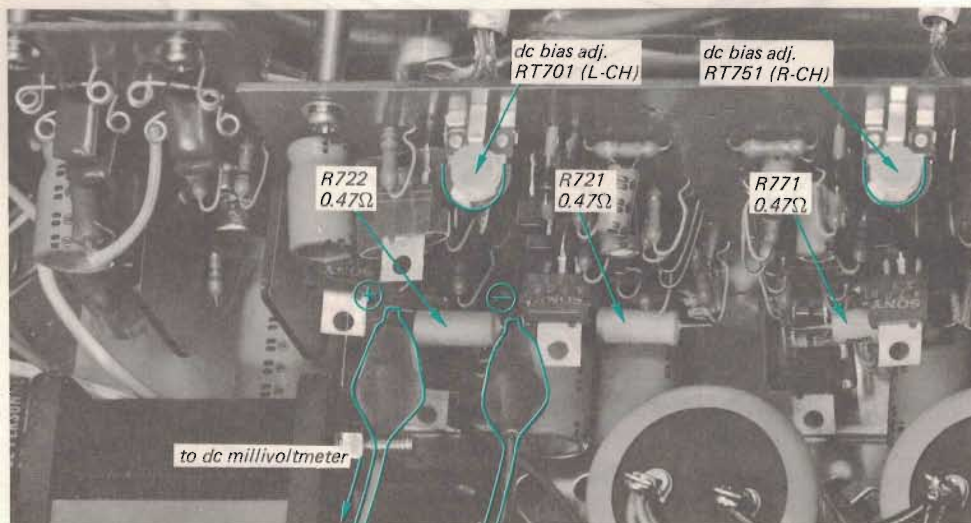


Fig. 3-17 Dc millivoltmeter connection

3. Screwdriver with 3 mm (1/8") blade

Preparation

1. Remove the top cover as described in Procedure 2-3.
2. Connect the dc millivoltmeter across emitter resistor R722 of power transistor Q901 as shown in Fig. 3-17.

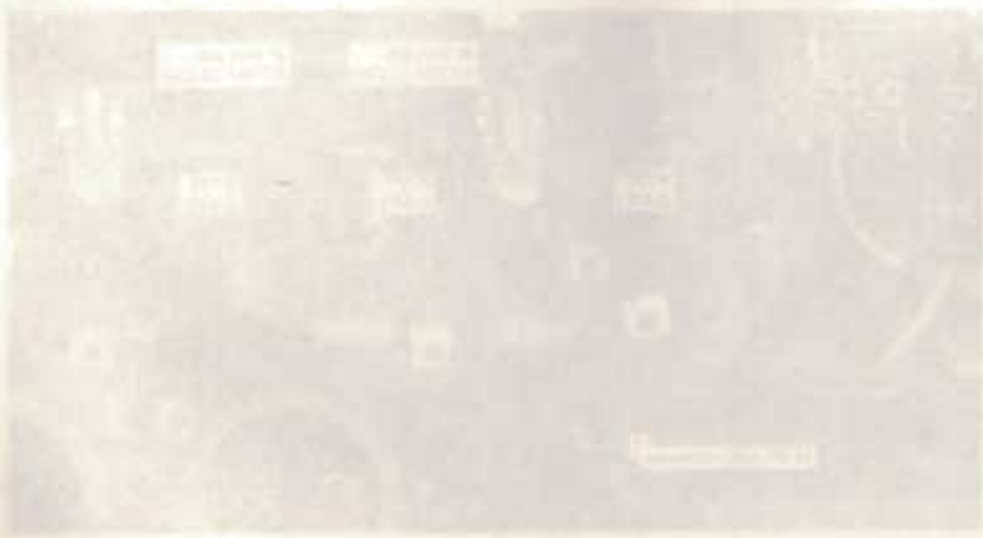
Procedure

1. Apply a drop of cement solvent to the semifixed resistors on the power amplifier board, and then set the semifixed resistors (see Fig. 3-17) on the power amplifier board as follows:

RT701 (L-CH, dc-bias) fully clockwise

RT751 (R-CH, dc-bias) fully counterclockwise

2. Set the variable transformer for minimum output.
3. Turn the POWER switch to ON, and then increase the line voltage up to the rated value.
4. Adjust RT701 and RT751 to obtain a 25 mV reading on the meter.



SECTION 4 REPACKING

The STR-6045 original shipping carton and packing materials are the ideal containers for shipping the unit. However to secure the maximum protection, the

STR-6045 must be repacked in these materials precisely as before. The proper repacking procedures are shown in Fig. 4-1.

X-37930-04 -
card ass'y, warranty (USA Model only)
X-44900-02
cloth, polishing
1-501-083
ribbon antenna, fm
1-506-138-11
phono plug, red
1-506-138-12
phono plug, white
1-532-298
fuse
2-043-415
bag, polyethylene (small)
3-701-020
bag, polyethylene (large)
3-790-949-31
manual, instruction (USA Model)
3-790-949-31
manual, instruction (CANADA Model)
3-793-105
list, warranty station (CANADA Model only)
3-793-183
card, inspection
3-796-836-41
SONY HiFi warranty (CANADA Model only)
4-802-201
bag, polyethylene (CANADA Model only)

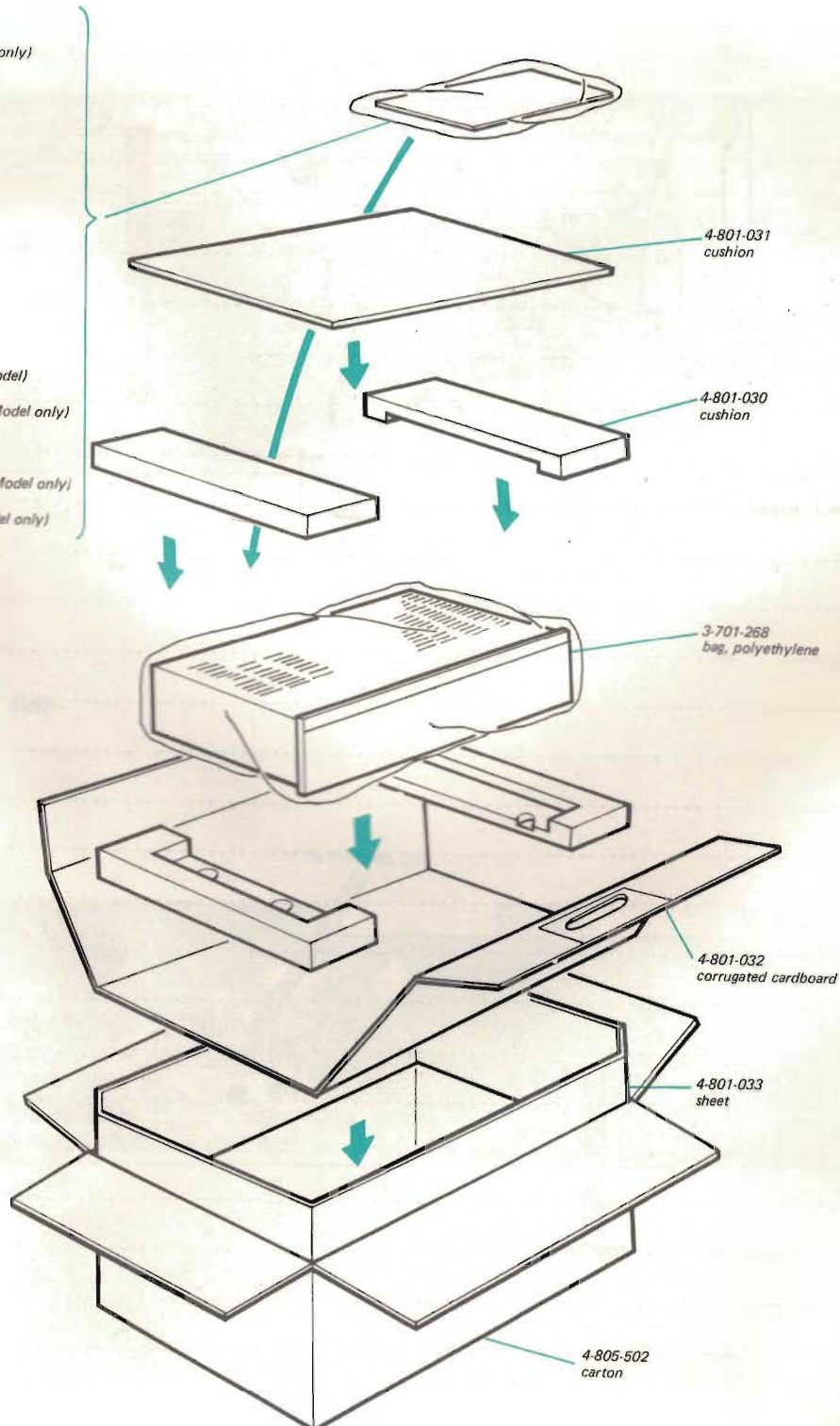


Fig. 4-1 Repacking

SECTION 4
REPACKING

MEMO

TO: [Faint text]
FROM: [Faint text]
SUBJECT: [Faint text]

[Faint text]

[Faint text]

[Faint text]

[Faint text]

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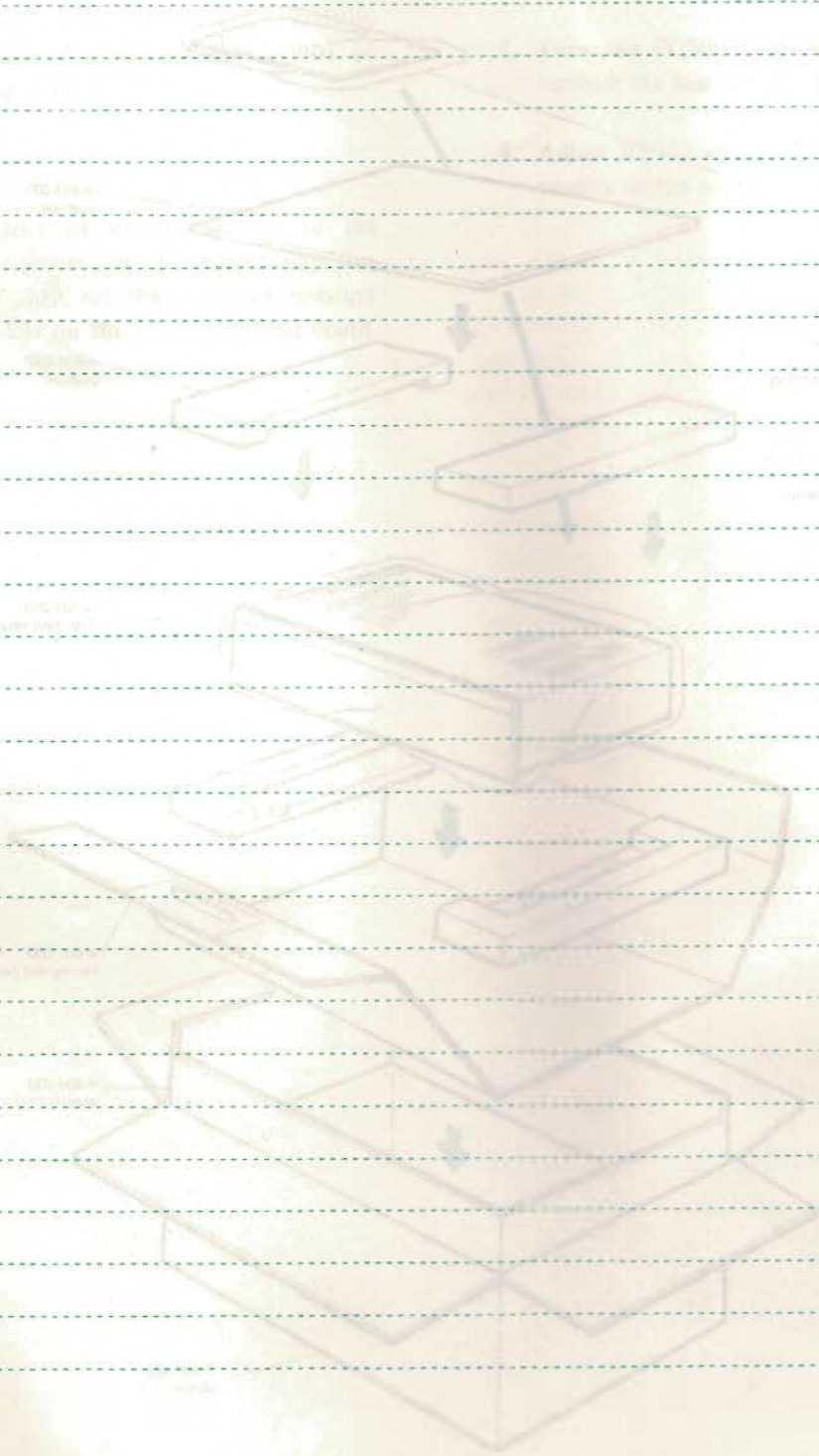
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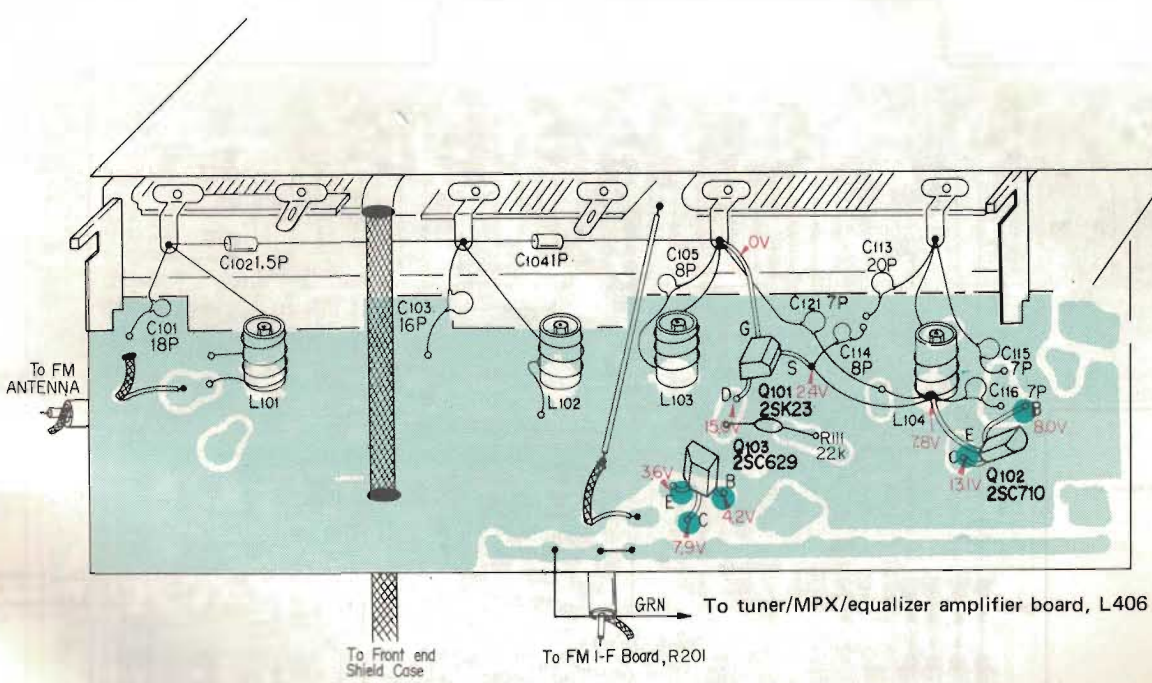
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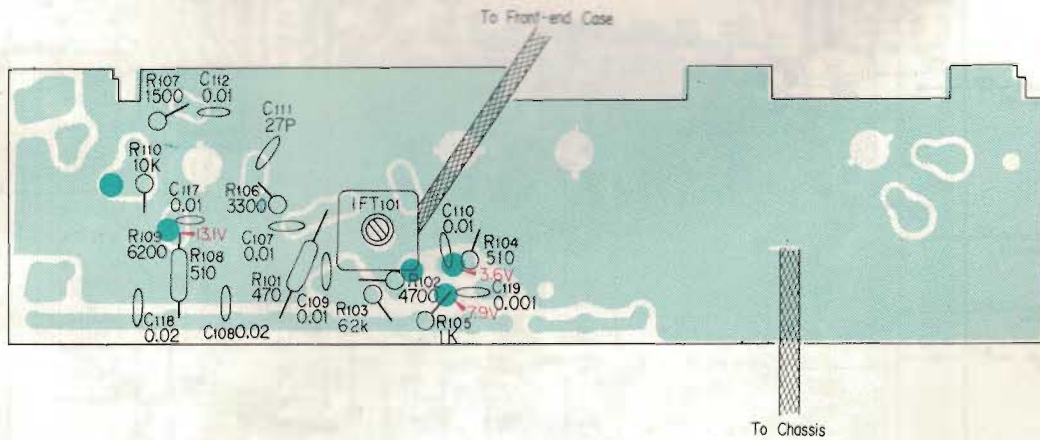
SECTION 5 DIAGRAMS

5-1. MOUNTING DIAGRAM—Fm Front End

—Conductor Side—

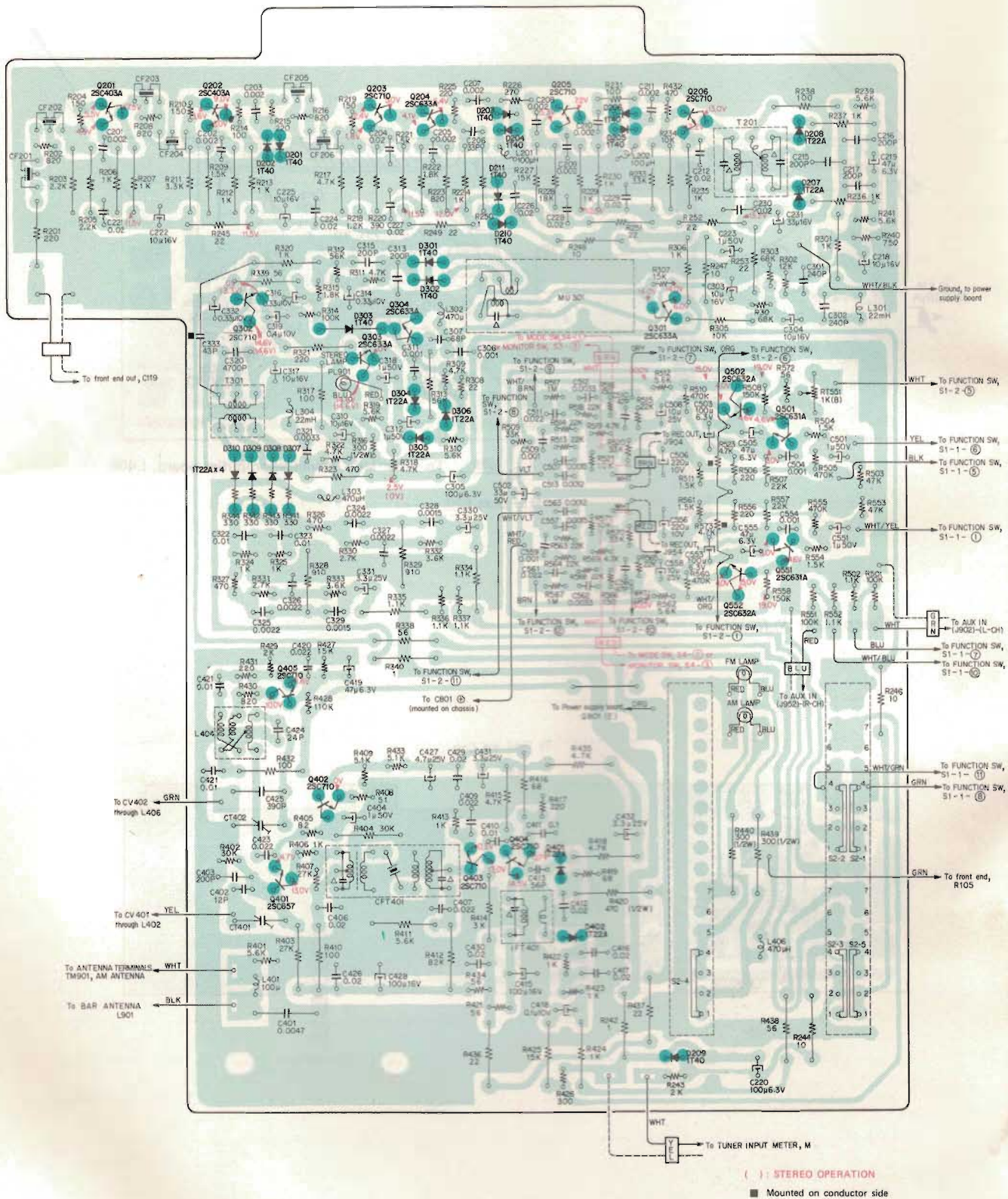


—Component Side—

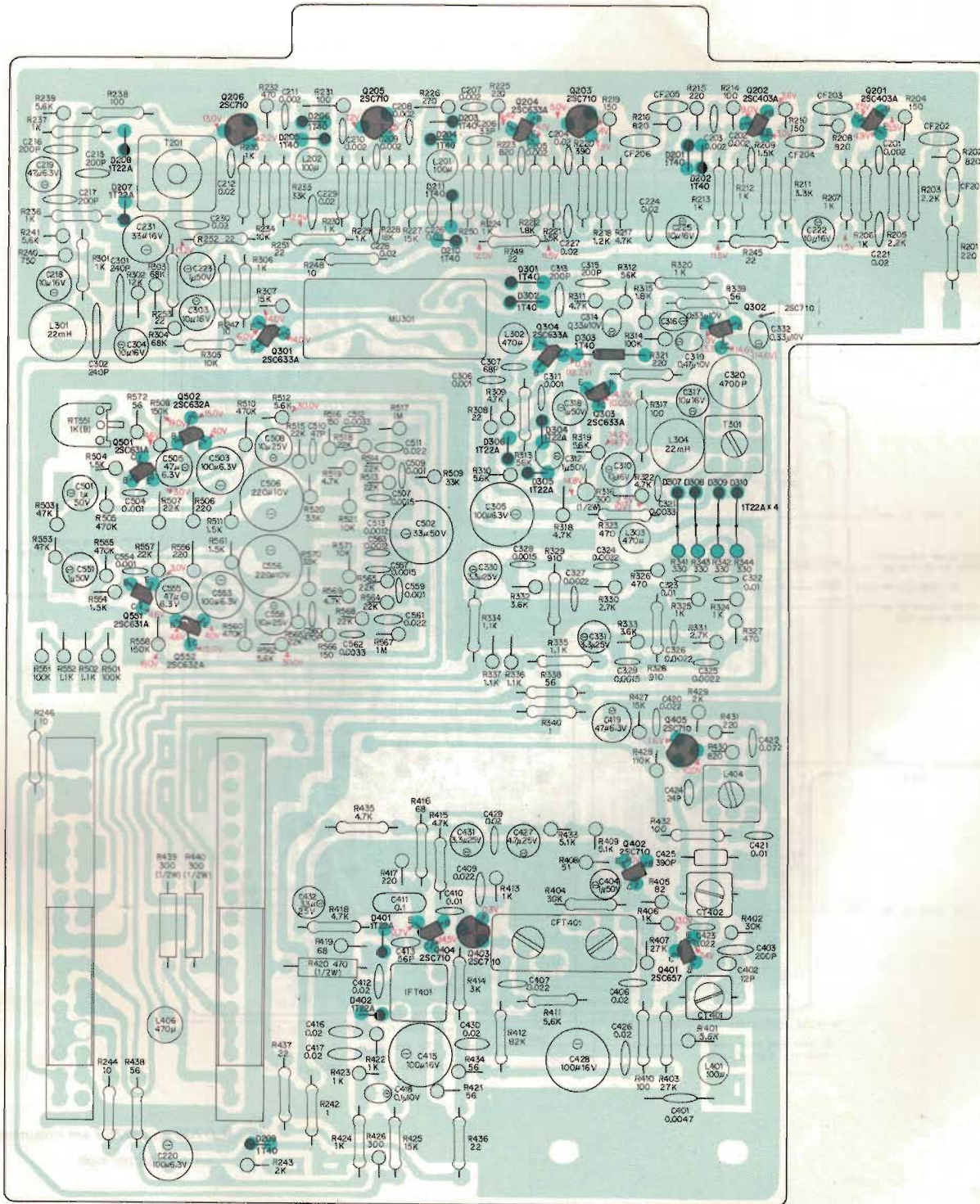


5-2. MOUNTING DIAGRAM—Tuner/MPX/Equalizer Amplifier Board

—Conductor Side—

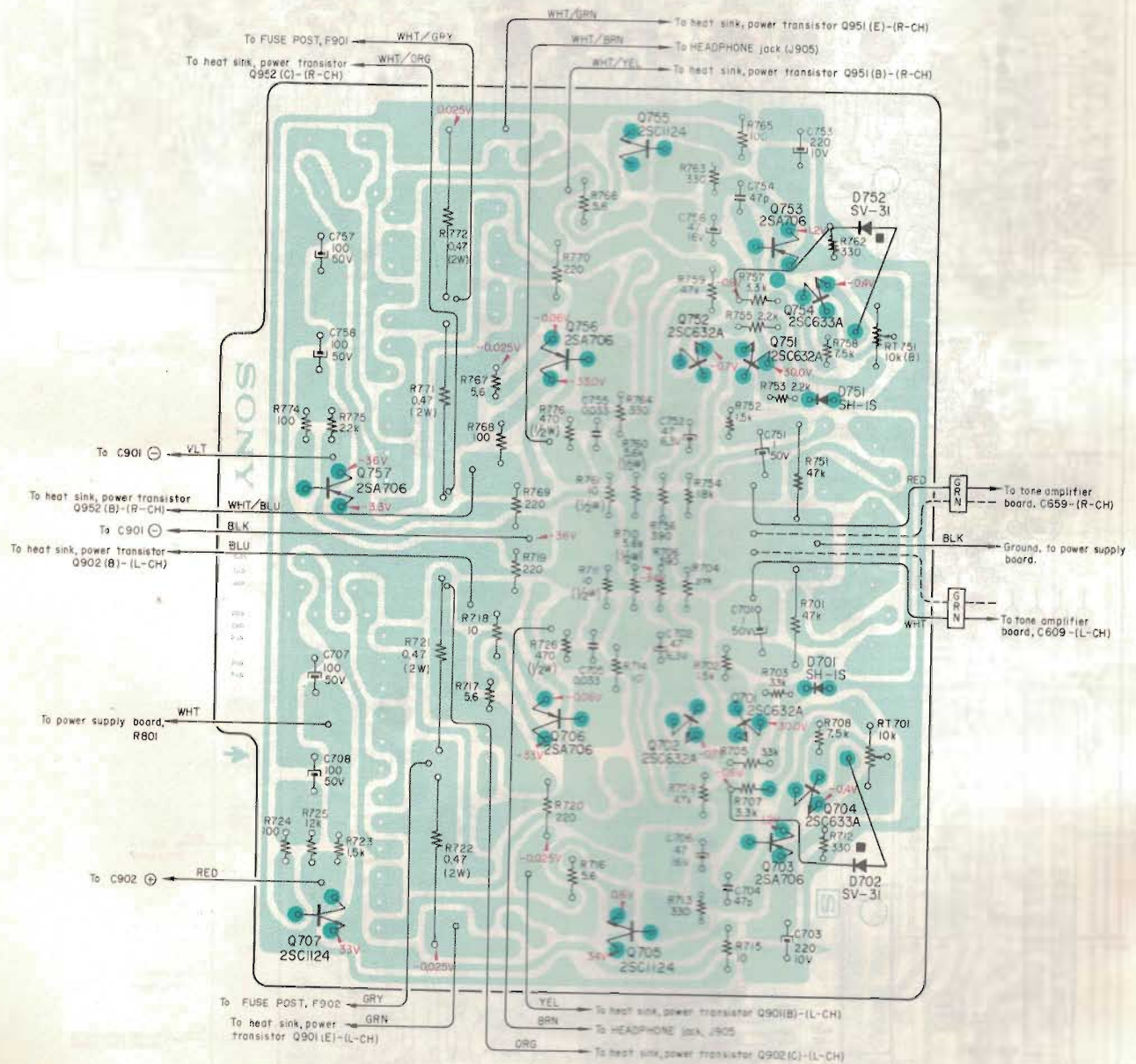


5-2. MOUNTING DIAGRAM—Tuner/MPX/Equalizer Amplifier Board
 —Component Side—



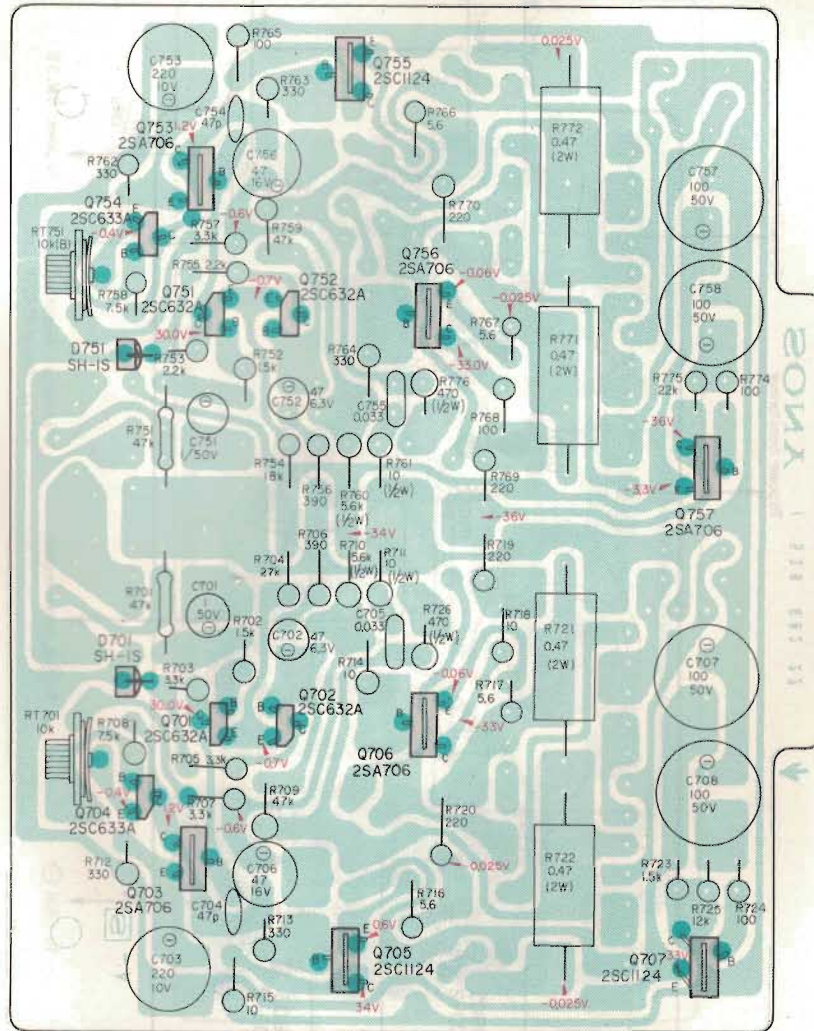
I : STEREO OPERATION

5.3. MOUNTING DIAGRAM—Power Amplifier Section
 —Conductor Side—

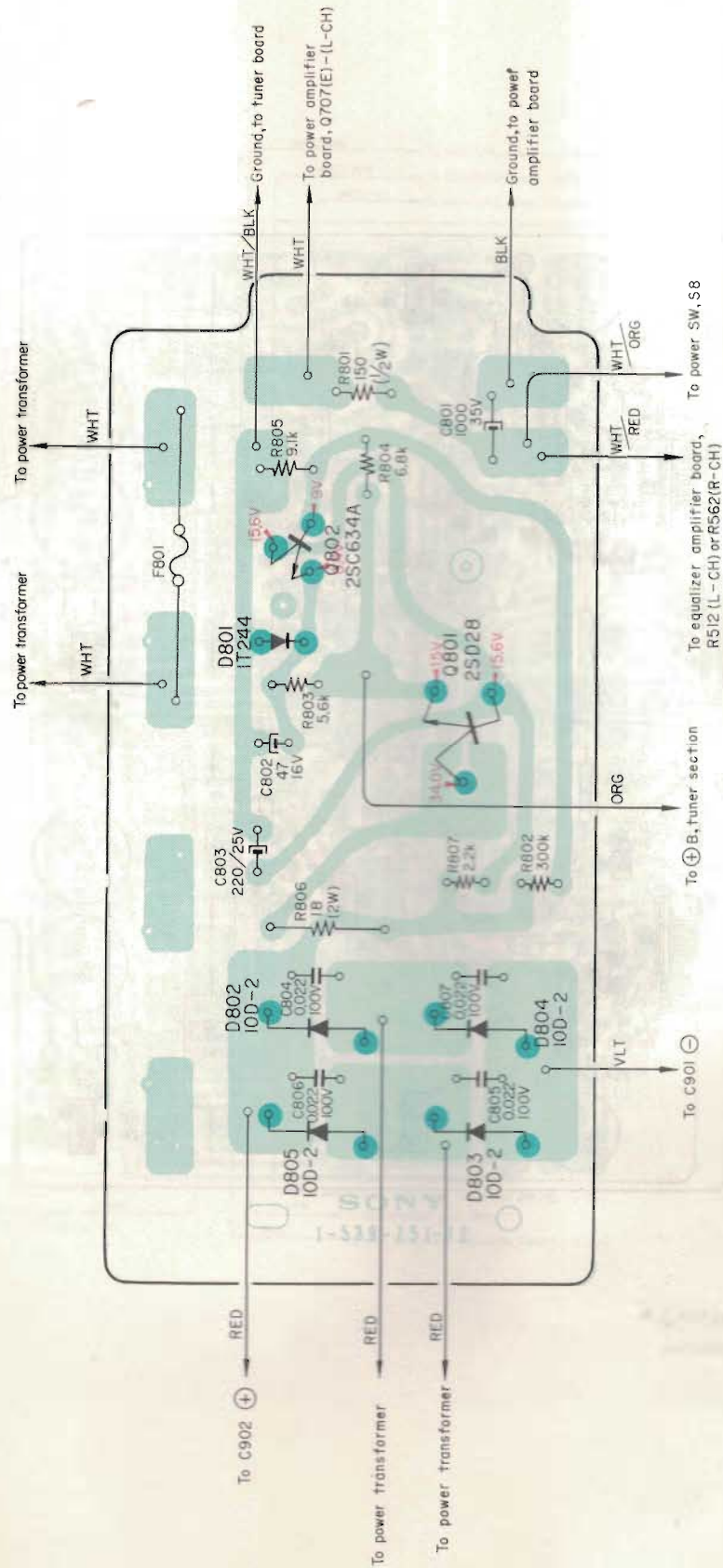


■ D702 and D752 are mounted on conductor side

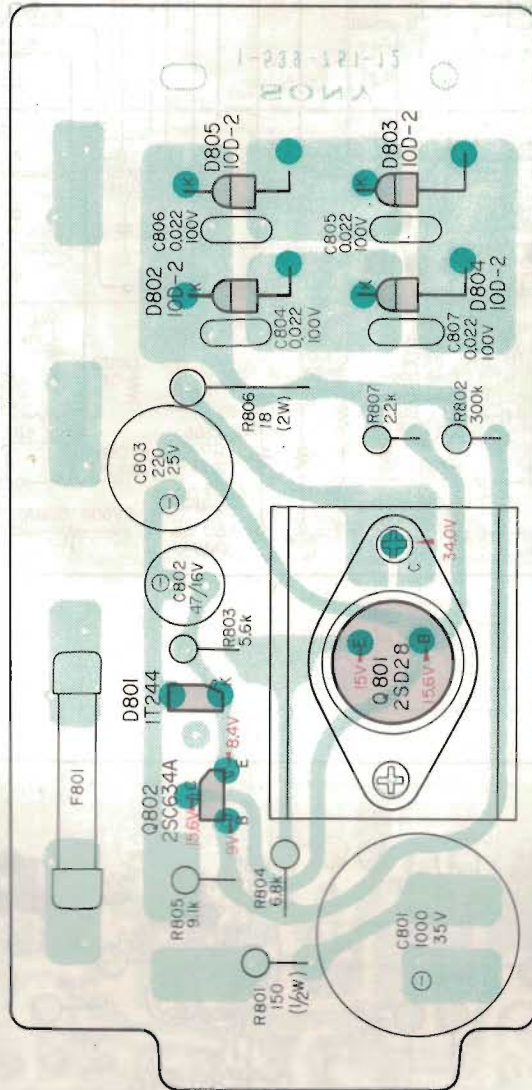
5-3. MOUNTING DIAGRAM—Power Amplifier Section
—Component Side—



5-4. MOUNTING DIAGRAM—Power Supply Board
—Conductor Side—

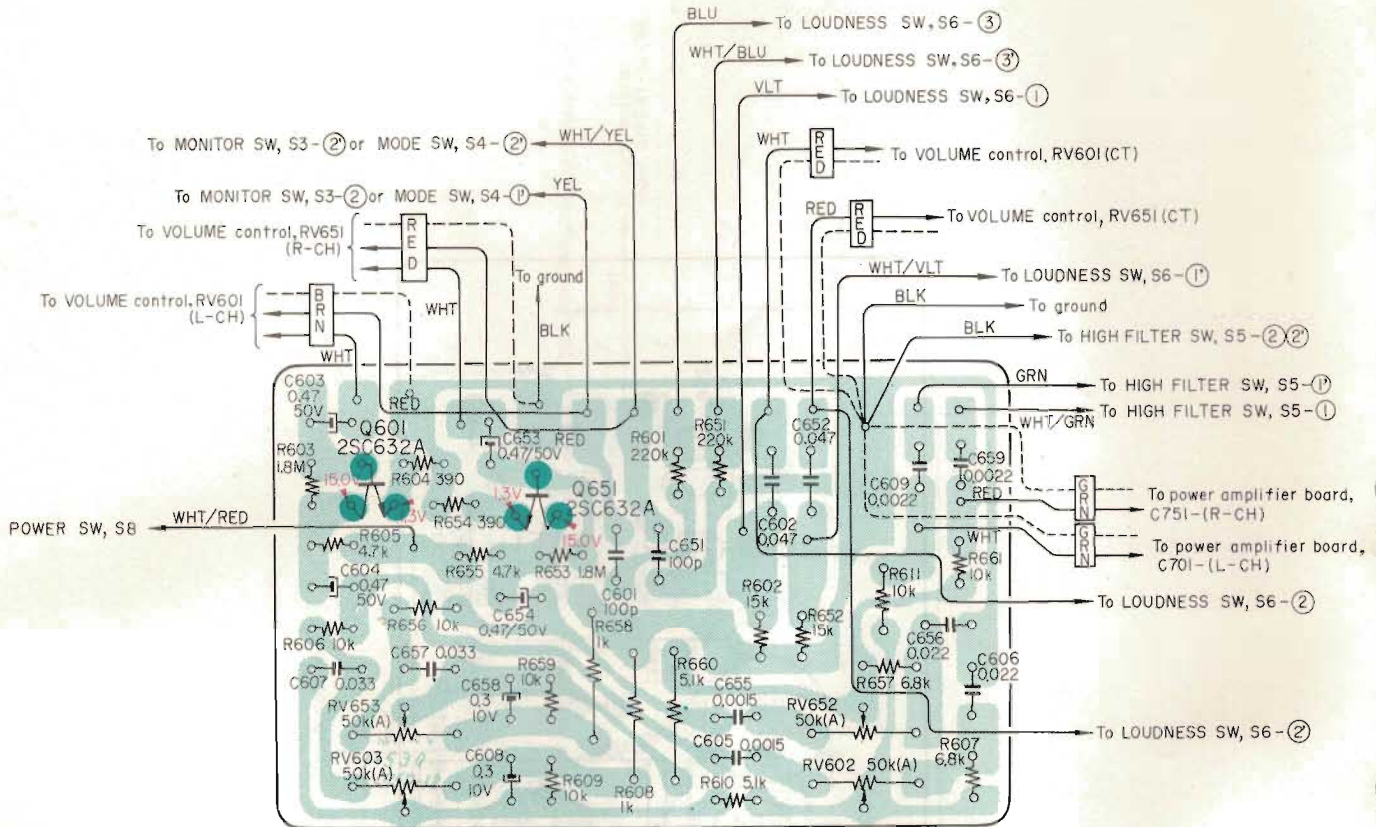


5-4. MOUNTING DIAGRAM--Power Supply Board
--Component Side--

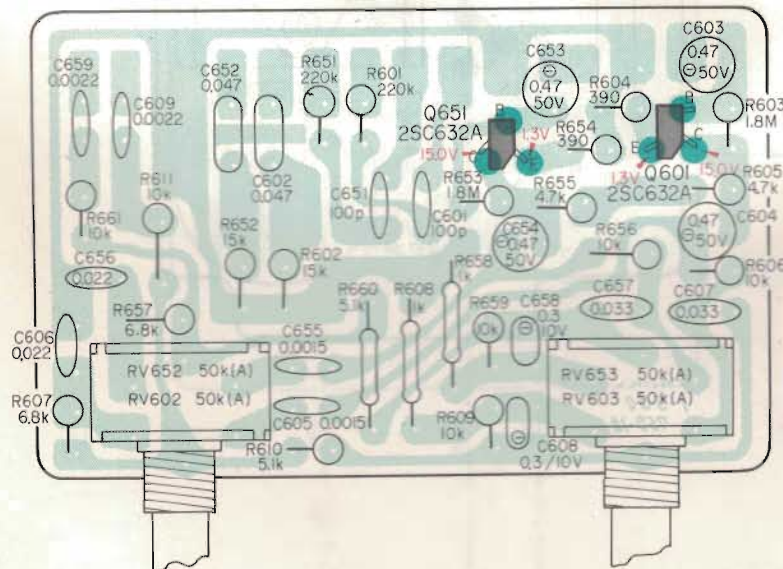


5-5. MOUNTING DIAGRAM—Tone Control Board

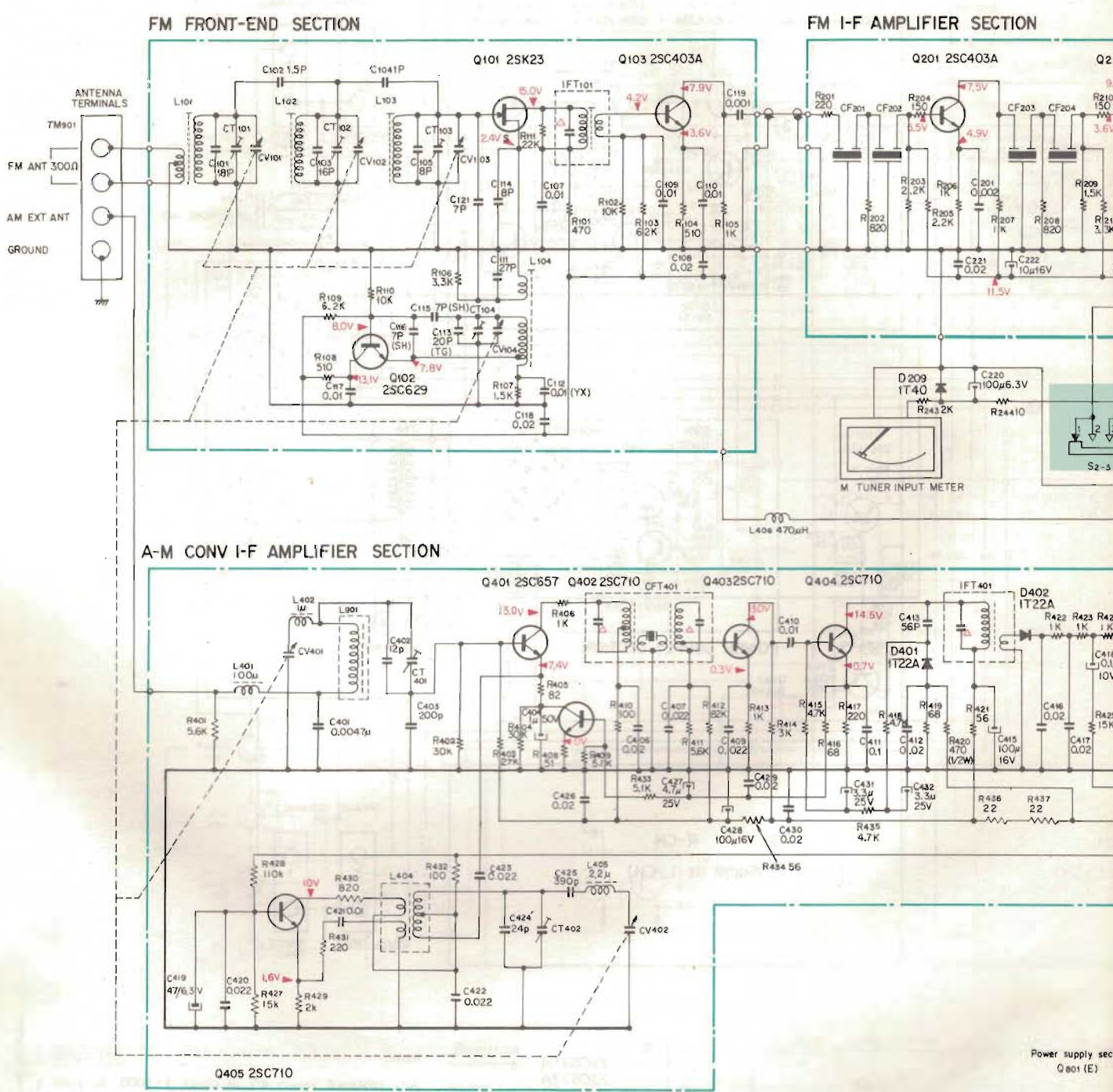
—Conductor Side—



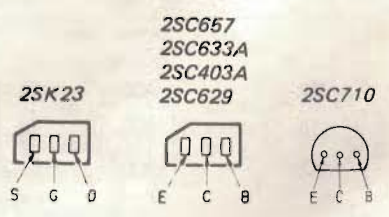
—Component Side—

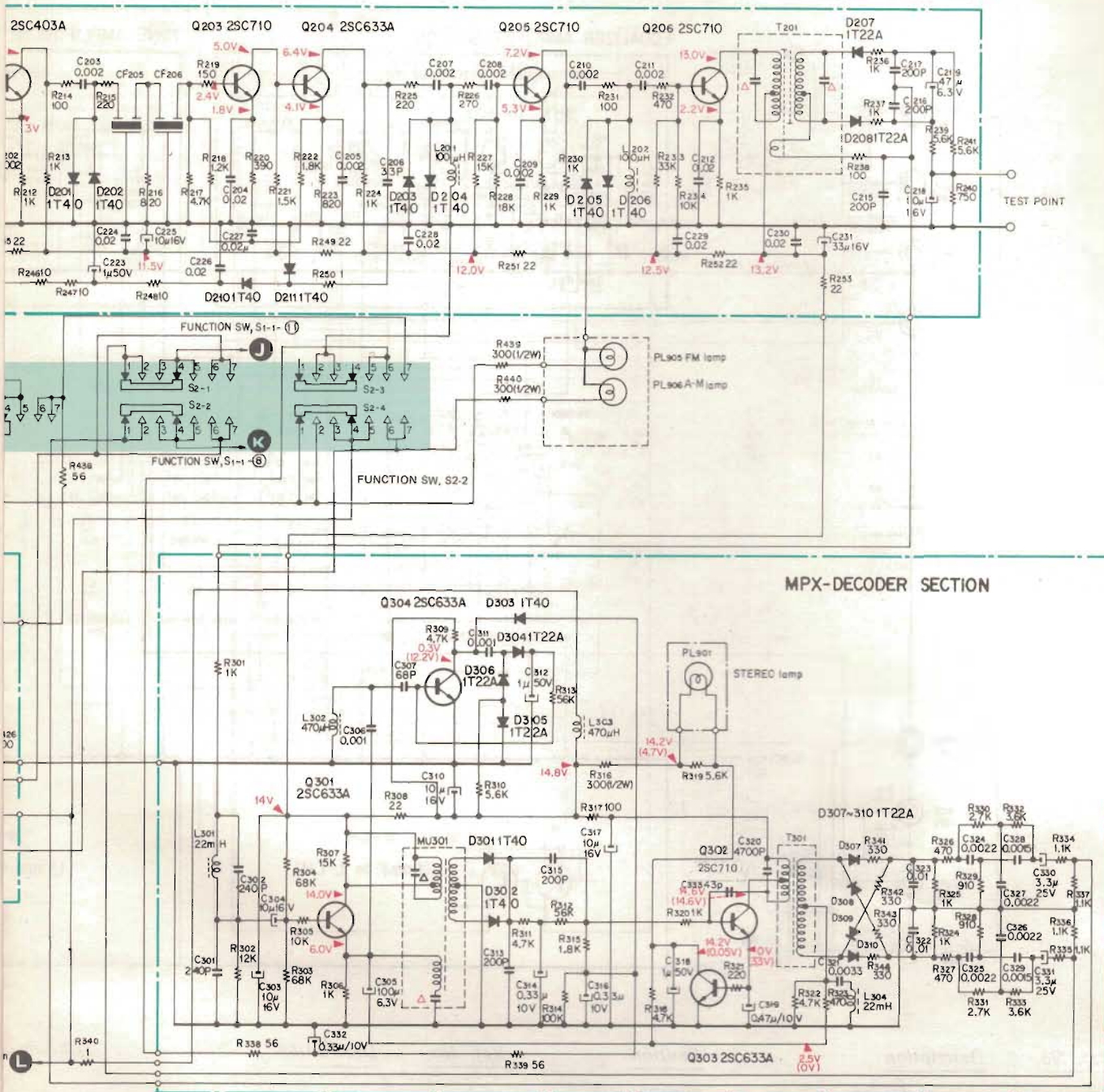


5-6. SCHEMATIC DIAGRAM—Tuner Section



Ref. No.	Description	Position
S1	FUNCTION (1) SW (AUX-FUNCTION (2)-PHONO)	FUNCTION (2)
S2	FUNCTION (2) SW (FM AUTO STEREO-FM MONO-AM)	FM AUTO STEREO





Note:

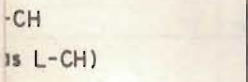
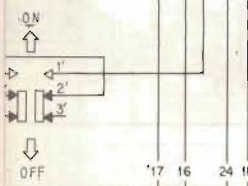
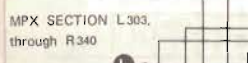
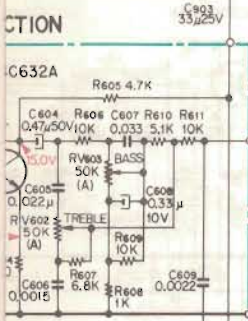
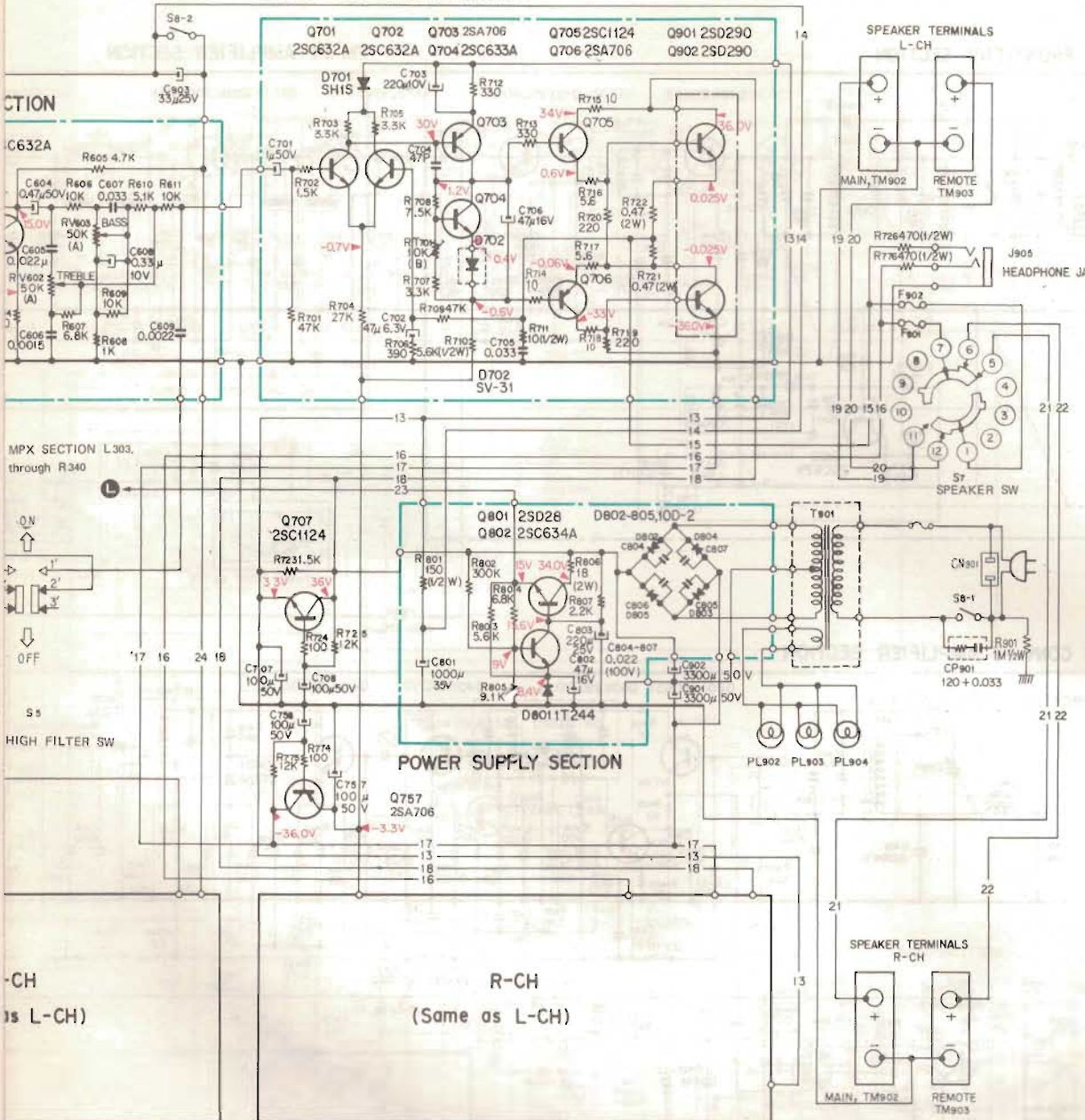
All resistance values are in ohms. k=1000, M=1000 k
 All capacitance values are in μF except as indicated with p, which means μF .
 All voltages represent an average value and should hold within $\pm 20\%$.
 All voltages are dc measured with a VOM which has an input impedance of 20 k ohms/volt. No signal in.

I : STEREO OPERATION

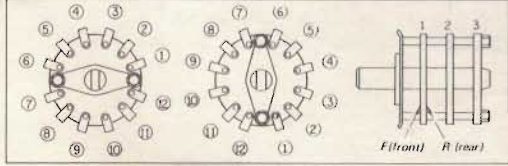
SONY
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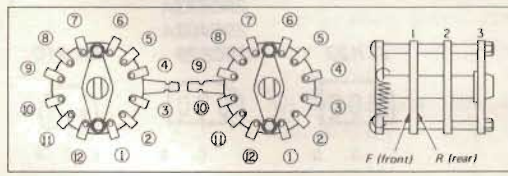
POWER AMPLIFIER SECTION



ROTARY SWITCH INDEX



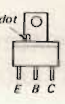
LEVER SWITCH INDEX



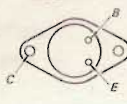
- 2SC631A
- 2SC632A
- 2SC633A
- 2SC634A



- 2SA706
- 2SC1124



- 2SD290
- 2SD28

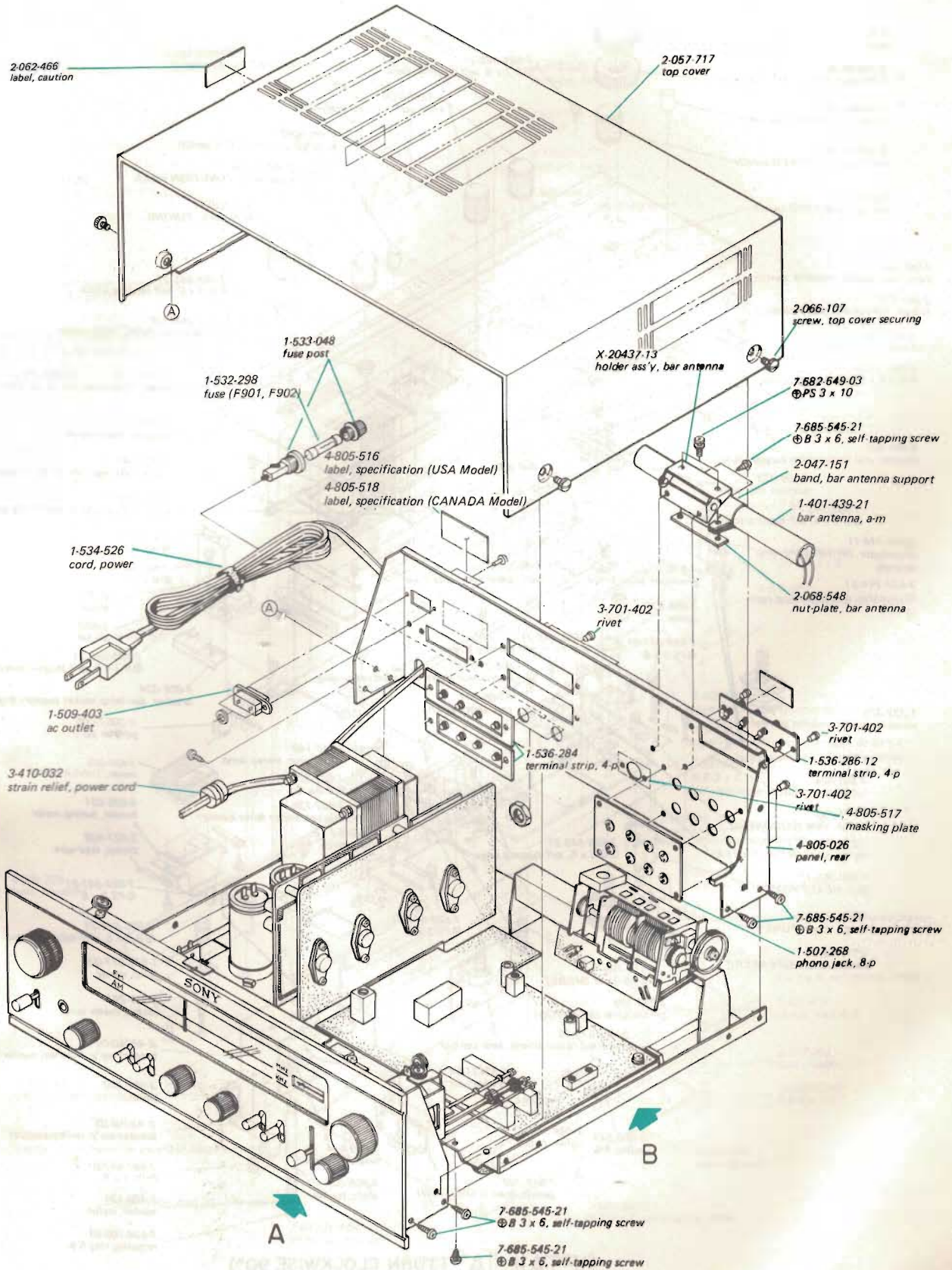


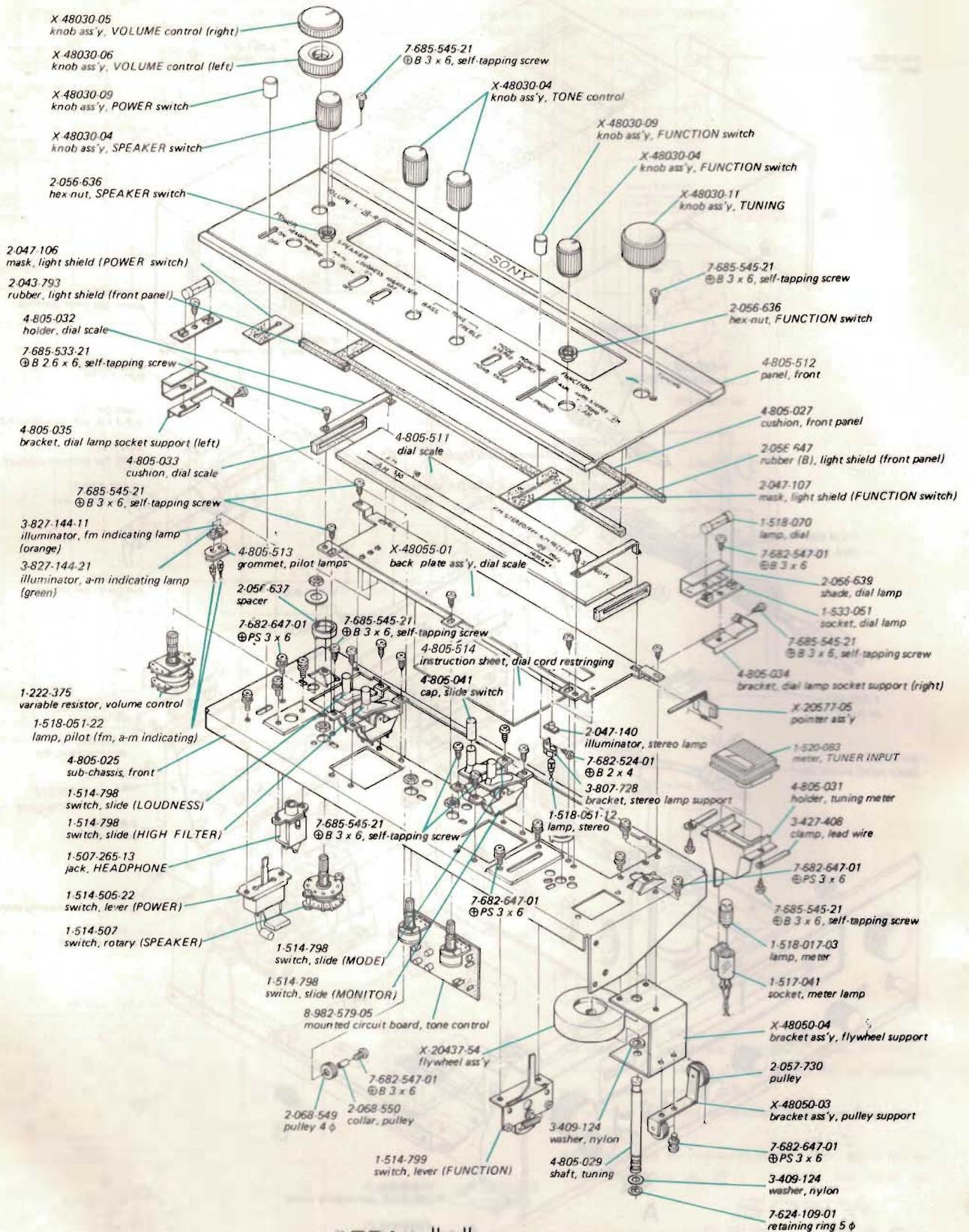
Note:

All resistance values are in ohms. k=1000, M=1000 k
 All capacitance values are in μF except as indicated with p, which means μpF .
 All voltages represent an average value and should hold within $\pm 20\%$.
 All voltages are dc measured with a VOM which has an input impedance of 20 k ohms/volt. No signal in.

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STR-6045
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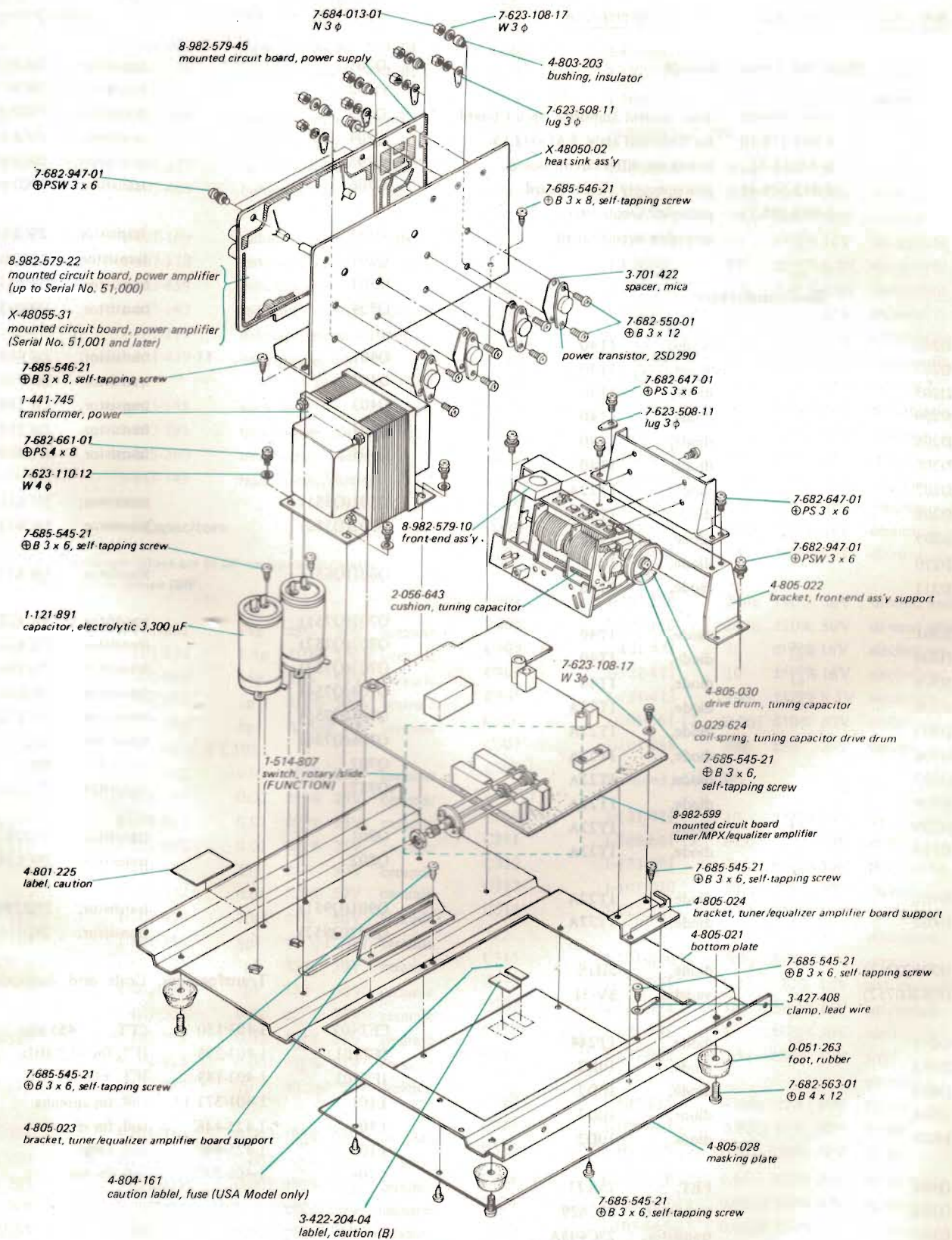
SECTION 6 EXPLODED VIEW





DETAIL "A" (TURN CLOCKWISE 90°)

SECTION 7
ELECTRICAL PARTS LIST



DETAIL "B"

SECTION 7 ELECTRICAL PARTS LIST

<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>
Mounted Circuit Boards			Q201		transistor, 2SC403A
	8-982-579-05	tone control amplifier circuit board	Q202		transistor, 2SC403A
	8-982-579-10	fm front-end ass'y, FAF-011AW	Q203		transistor, 2SC710
	X-48055-31	power amplifier circuit board	Q204		transistor, 2SC633A
	8-982-579-45	power supply circuit board	Q205		transistor, 2SC710
	8-982-598-11	tuner/MPX/equalizer amplifier circuit board	Q206		transistor, 2SC710
Semiconductors			Q301		transistor, 2SC633A
D201		diode, 1T40	Q302		transistor, 2SC710
D202		diode, 1T40	Q303		transistor, 2SC633A
D203		diode, 1T40	Q304		transistor, 2SC633A
D204		diode, 1T40	Q401		transistor, 2SC657
D205		diode, 1T40	Q402		transistor, 2SC710
D206		diode, 1T40	Q403		transistor, 2SC710
D207		diode, 1T22A	Q404		transistor, 2SC710
D208		diode, 1T22A	Q405		transistor, 2SC710
D209		diode, 1T40	Q501(Q551)		transistor, 2SC631A
D210		diode, 1T40	Q502(Q552)		transistor, 2SC632A
D211		diode, 1T40	Q601(Q651)		transistor, 2SC632A
D301		diode, 1T40	Q701(Q751)		transistor, 2SC632A
D302		diode, 1T40	Q702(Q752)		transistor, 2SC632A
D303		diode, 1T40	Q703(Q753)		transistor, 2SA706
D304		diode, 1T22A	Q704(Q754)		transistor, 2SC633A
D305		diode, 1T22A	Q705(Q755)		transistor, 2SC1124
D306		diode, 1T22A	Q706(Q756)		transistor, 2SA706
D307		diode, 1T22A	Q707		transistor, 2SC1124
D308		diode, 1T22A	Q757		transistor, 2SA706
D309		diode, 1T22A	Q801		transistor, 2SD28
D310		diode, 1T22A	Q802		transistor, 2SC634A
D401		diode, 1T22A	Q901(Q951)		transistor, 2SD290
D402		diode, 1T22A	Q902(Q952)		transistor, 2SD290
D701(D751)		diode, SH1S	Transformers, Coils and Inductors		
D702(D752)		varistor, SV-31	CFT401	1-403-150	CFT, 455 kHz
D801		diode, 1T244	IFT101	1-403-295	IFT, fm 10.7 MHz
D802		diode, 10D2	IFT401	1-403-149	IFT, a-m 455 kHz
D803		diode, 10D2	L101	1-401-371-12	coil, fm antenna
D804		diode, 10D2	L102	1-425-446	coil, fm rf
D805		diode, 10D2	L103	1-425-446	coil, fm rf
Q101		FET, 2SK23	L104	1-405-377	coil, fm osc
Q102		transistor, 2SC629			
Q103		transistor, 2SC403A			

Ref. No.	Part No.	Description	Ref. No.	Part No.	Description
L201	1-407-169	inductor, micro 100 μ H	C210	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic
L202	1-407-169	inductor, micro 100 μ H	C211	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic
L301	1-407-408	inductor, micro 22 mH	C212	1-101-073	0.02 $\pm\frac{80}{20}\%$ 50V ceramic
L302	1-407-177	inductor, micro 470 μ H	C213	Included in T 201	
L303	1-407-177	inductor, micro 470 μ H	C214		
L304	1-407-408	inductor, micro 22 mH	C215		1-101-030
L401	1-407-169	inductor, micro 100 μ H	C216	1-101-030	200p $\pm 5\%$ 50V ceramic
L402	1-407-178	inductor, micro 1 μ H	C217	1-101-030	200p $\pm 5\%$ 50V ceramic
L404	1-405-459	coil, a-m osc	C218	i-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
L405	1-407-182	inductor, micro 2.2 μ H	C219	1-121-487	47 $\pm\frac{100}{10}\%$ 6.3V electrolytic
L406	1-407-177	inductor, micro 470 μ H	C220	1-121-413	100 $\pm\frac{100}{10}\%$ 6.3V electrolytic
L901	1-401-439-11	bar antenna, a-m	C221	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
MU301	1-425-548	MPX unit	C222	1-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
T201	1-403-291	transformer, discriminator	C223	1-121-391	1 $\pm\frac{150}{10}\%$ 50V electrolytic
T301	1-425-260	transformer, switching	C224	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
T901	1-441-745	transformer, power	C225	1-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
			C226	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
			C227	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
			C228	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
			C229	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
			C230	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic
			C231	1-121-403	33 $\pm\frac{100}{10}\%$ 16V electrolytic
			C301	1-107-140	240p $\pm 10\%$ 50V silvered mica
			C302	1-107-140	240p $\pm 10\%$ 50V silvered mica
			C303	1-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
			C304	1-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
			C305	1-121-413	100 $\pm\frac{100}{10}\%$ 6.3V electrolytic
			C306	1-105-661-12	0.001 $\pm 10\%$ 50V mylar
			C307	1-101-888	68p $\pm 5\%$ 50V ceramic
			C308	Included in MU 301	
			C309		
			C310	1-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
			C311	1-105-661-12	0.001 $\pm 10\%$ 50V mylar
			C312	1-121-391	1 $\pm\frac{150}{10}\%$ 50V electrolytic
			C313	1-101-030	200p $\pm 5\%$ 50V ceramic
			C314	1-127-021	0.33 $\pm 20\%$ 10V solid, aluminum
			C315	1-101-030	200p $\pm 5\%$ 50V ceramic
			C316	1-127-021	0.33 $\pm 20\%$ 10V solid, aluminum
			C317	1-121-471	10 $\pm\frac{100}{10}\%$ 16V electrolytic
			C318	1-121-391	1 $\pm\frac{150}{10}\%$ 50V electrolytic
			C319	1-127-022	0.47 $\pm 20\%$ 10V solid, aluminum
			C320	1-103-575	4700p $\pm 5\%$ 50V styrol
			C321	1-106-013-12	0.0033 $\pm 5\%$ 50V mylar
			C322	1-105-673-12	0.01 $\pm 10\%$ 50V mylar
			C323	1-105-673-12	0.01 $\pm 10\%$ 50V mylar
			C324	1-105-665-12	0.0022 $\pm 10\%$ 50V mylar
			C325	1-105-665-12	0.0022 $\pm 10\%$ 50V mylar
			C326	1-105-665-12	0.0022 $\pm 10\%$ 50V mylar
			C327	1-105-665-12	0.0022 $\pm 10\%$ 50V mylar
			C328	1-105-663-12	0.0015 $\pm 10\%$ 50V mylar
			C329	1-105-663-12	0.0015 $\pm 10\%$ 50V mylar
C201	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			
C202	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			
C203	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			
C204	1-101-073	0.02 $\pm\frac{80}{20}\%$ 25V ceramic			
C205	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			
C206	1-101-872	33p $\pm 5\%$ 50V ceramic			
C207	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			
C208	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			
C209	1-101-919	0.002 $\pm\frac{80}{20}\%$ 25V ceramic			

Capacitors

All capacitance values are in μ F except as indicated with P, which means μ MF.

SECTION 7
ELECTRICAL PARTS LIST

<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>
C330	1-121-392	3.3 ±15% 25V electrolytic	C601(C651)	1-102-975	100p ±10% 50V ceramic
C331	1-121-392	3.3 ±15% 25V electrolytic	C602(C652)	1-105-681-12	0.047 ±10% 50V mylar
C332	1-127-021	0.33 ±20% 10V solid, aluminum	C603(C653)	1-121-726	0.47 ±15% 50V electrolytic
C333	1-102-966	43p ±5% 50V ceramic	C604(C654)	1-121-726	0.47 ±15% 50V electrolytic
C401	1-103-575	4700p ±5% 50V styrol	C605(C655)	1-105-663-12	0.0015 ±10% 50V mylar
C402	1-101-949	12p ±5% 50V ceramic	C606(C656)	1-105-677-12	0.022 ±10% 50V mylar
C403	1-101-030	200p ±5% 50V ceramic	C607(C657)	1-105-679-12	0.033 ±10% 50V mylar
C404	1-121-391	1 ±15% 50V electrolytic	C608(C658)	1-127-021	0.33 ±20% 10V solid, aluminum
C405	Included in CFT 401		C609(C659)	1-105-665-12	0.0022 ±10% 50V mylar
C406	1-101-073	0.02 ±8% 25V ceramic	C701(C751)	1-121-391	1 ±15% 50V electrolytic
C407	1-105-677-12	0.022 ±10% 50V mylar	C702(C752)	1-121-487	47 ±10% 6.3V electrolytic
C408	Included in CFT 401		C703(C753)	1-121-420	220 ±10% 10V electrolytic
C409	1-105-677-12	0.022 ±10% 50V mylar	C704(C754)	1-101-881	47p ±10% 50V ceramic
C410	1-105-673-12	0.01 ±10% 50V mylar	C705(C755)	1-105-679-12	0.033 ±10% 50V mylar
C411	1-105-685-12	0.1 ±10% 50V mylar	C706(C756)	1-121-409	47 ±10% 16V electrolytic
C412	1-101-073	0.02 ±8% 25V ceramic	C707(C757)	1-121-417	100 ±10% 50V electrolytic
C413	1-101-884	56p ±5% 50V ceramic	C708(C758)	1-121-417	100 ±10% 50V electrolytic
C414	Included in IFT 401		C801	1-121-388	1000 ±10% 35V electrolytic
C415	1-121-415	100 ±10% 16V electrolytic	C802	1-121-409	47 ±10% 16V electrolytic
C416	1-101-073	0.02 ±8% 25V ceramic	C803	1-121-422	220 ±10% 25V electrolytic
C417	1-101-073	0.02 ±8% 25V ceramic	C804	1-105-717-12	0.022 ±10% 100V mylar
C418	1-127-019	0.1 ±20% 10V solid, aluminum	C805	1-105-717-12	0.022 ±10% 100V mylar
C419	1-121-487	47 ±10% 6.3V electrolytic	C806	1-105-717-12	0.022 ±10% 100V mylar
C420	1-105-677-12	0.022 ±10% 50V mylar	C807	1-105-717-12	0.022 ±10% 100V mylar
C421	1-105-673-12	0.01 ±10% 50V mylar	C901	1-121-891	3300 ±10% 50V electrolytic
C422	1-105-677-12	0.022 ±10% 50V mylar	C902	1-121-891	3300 ±10% 50V electrolytic
C423	1-105-677-12	0.022 ±10% 50V mylar	C903	1-121-404	33 ±10% 25V electrolytic
C424	1-101-867	24p ±5% 50V ceramic	CT401	1-141-097	trimmer capacitor
C425	1-103-615	390p ±5% 50V styrol	CT402	1-141-097	trimmer capacitor
C426	1-101-073	0.02 ±8% 25V ceramic	CV101	1-151-191	capacitor, tuning
C427	1-121-395	4.7 ±15% 25V electrolytic	CV102		
C428	1-121-415	100 ±10% 16V electrolytic	CV103		
C429	1-101-073	0.02 ±8% 25V ceramic	CV104		
C430	1-101-073	0.02 ±8% 25V ceramic	CV301		
C431	1-121-392	3.3 ±15% 25V electrolytic	CV302		
C432	1-121-392	3.3 ±15% 25V electrolytic	CT101	1-151-191	capacitor, tuning
C501(C551)	1-121-391	1 ±15% 50V electrolytic	CT102		
C502	1-121-405	33 ±10% 50V electrolytic	CT103		
C503(C553)	1-121-413	100 ±10% 6.3V electrolytic	CT104		
C504(C554)	1-105-661-12	0.001 ±10% 50V mylar			
C505(C555)	1-121-487	47 ±10% 6.3V electrolytic			
C506(C556)	1-121-420	220 ±10% 10V electrolytic			
C507(C557)	1-105-666-12	0.0027 ±10% 50V mylar			
C508(C558)	1-121-398	10 ±10% 25V electrolytic			
C509(C559)	1-105-661-12	0.001 ±10% 50V mylar			
C510(C560)	1-101-880	47p ±5% 50V ceramic			
C511(C561)	1-106-027-12	0.022 ±5% 50V mylar			
C512(C562)	1-106-013-12	0.0033 ±5% 50V mylar			
			Resistors		
All resistance values are in ohms, ±5%, 1/4 watts and carbon type unless otherwise indicated.					
			R101	1-244-665	470
			R102	1-244-697	10K

<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>
R103	1-244-716	62K	R246	1-244-625	10
R104	1-244-666	510	R247	1-244-625	10
R105	1-244-673	1K	R248	1-244-625	10
R106	1-244-685	3.3K	R249	1-244-633	22
R107	1-244-675	1.5K	R250	1-244-601	1
R108	1-244-666	510	R251	1-244-633	22
R109	1-244-692	6.2K	R252	1-244-633	22
R110	1-244-697	10K	R253	1-244-633	22
R111	1-244-705	22K			
			R301	1-244-673	1K
R201	1-244-657	220	R302	1-242-699	12K
R202	1-242-671	820	R303	1-242-717	68K
R203	1-244-681	2.2K	R304	1-242-717	68K
R204	1-242-653	150	R305	1-244-697	10K
R205	1-244-681	2.2K	R306	1-244-673	1K
R206	1-244-673	1K	R307	1-242-701	15K
R207	1-244-673	1K	R308	1-242-633	22
R208	1-242-671	820	R309	1-242-689	4.7K
R209	1-244-677	1.5K	R310	1-242-691	5.6K
R210	1-242-653	150	R311	1-242-689	4.7K
R211	1-244-685	3.3K	R312	1-242-715	56K
R212	1-244-673	1K	R313	1-244-715	56K
R213	1-244-673	1K	R314	1-242-721	100K
R214	1-242-649	100	R315	1-242-679	1.8K
R215	1-242-657	220	R316	1-202-560	300 ±10% 1/2W composition
R216	1-242-671	820	R317	1-244-649	100
R217	1-244-689	4.7K	R318	1-242-689	4.7K
R218	1-244-675	1.2K	R319	1-242-691	5.6K
R219	1-242-653	150	R320	1-244-673	1K
R220	1-244-663	390	R321	1-244-657	220
R221	1-244-677	1.5K	R322	1-242-689	4.7K
R222	1-244-679	1.8K	R323	1-244-665	470
R223	1-244-671	820	R324	1-242-673	1K
R224	1-244-673	1K	R325	1-242-673	1K
R225	1-242-657	220	R326	1-242-665	470
R226	1-242-659	270	R327	1-242-665	470
R227	1-244-701	15K	R328	1-244-672	910
R228	1-244-703	18K	R329	1-244-672	910
R229	1-244-673	1K	R330	1-242-683	2.7K
R230	1-244-673	1K	R331	1-242-683	2.7K
R231	1-242-649	100	R332	1-242-686	3.6K
R232	1-242-665	470	R333	1-242-686	3.6K
R233	1-244-709	33K	R334	1-244-674	1.1K
R234	1-244-697	10K	R335	1-244-674	1.1K
R235	1-244-673	1K	R336	1-242-674	1.1K
R236	1-244-673	1K	R337	1-242-674	1.1K
R237	1-244-673	1K	R338	1-244-643	56
R238	1-244-649	100	R339	1-244-643	56
R239	1-242-691	5.6K	R340	1-244-601	1
R240	1-242-670	750	R341	1-244-661	330
R241	1-242-691	5.6K	R342	1-244-661	330
R242	1-244-601	1	R343	1-244-661	330
R243	1-242-680	2K	R344	1-244-661	330
R244	1-244-625	10			
R245	1-244-633	22			

<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>
R401	1-242-691	5.6K	R515(R565)	1-242-705	22K
R402	1-244-708	30K	R516(R566)	1-242-653	150
R403	1-242-707	27K	R517(R567)	1-242-945	1M
R404	1-242-708	30K	R518(R568)	1-242-705	22K
R405	1-242-647	82	R519(R569)	1-242-689	4.7K
R406	1-242-673	1K	R520(R570)	1-242-709	33K
R407	1-242-707	27K	R521(R571)	1-242-697	10K
R408	1-242-642	51	R572	1-242-643	56
R409	1-242-690	5.1K	R523(R573)	1-244-689	4.7K
R410	1-244-649	100			
R411	1-242-691	5.6K	R601(R651)	1-242-729	220K
R412	1-244-719	82K	R602(R652)	1-242-701	15K
R413	1-242-673	1K	R603(R653)	1-242-751	1.8M
R414	1-244-684	3K	R604(R654)	1-242-663	390
R415	1-242-689	4.7K	R605(R655)	1-242-689	4.7K
R416	1-242-645	68	R606(R656)	1-242-697	10K
R417	1-242-657-09	220	R607(R657)	1-242-693	6.8K
R418	1-242-689	4.7K	R608(R658)	1-244-673	1K
R419	1-242-645	68	R609(R659)	1-242-697	10K
R420	1-202-565	470 $\pm 10\%$ 1/2W composition	R610	1-242-690	5.1K
R421	1-244-643	56	R611(R661)	1-242-697	10K
R422	1-242-673	1K	R660	1-244-690	5.1K
R423	1-242-673	1K	R701(R751)	1-244-713	47K
R424	1-242-673	1K	R702(R752)	1-242-677	1.5K
R425	1-242-701	15K	R703(R753)	1-242-685	3.3K
R426	1-242-660	300	R704(R754)	1-242-707	27K
R427	1-242-701	15K	R705(R755)	1-242-685	3.3K
R428	1-242-722	110K	R706(R756)	1-242-663	390
R429	1-242-680	2K	R707(R757)	1-242-685	3.3K
R430	1-242-671	820	R708(R758)	1-242-694	7.5K
R431	1-242-657	220	R709(R759)	1-242-713	47K
R432	1-244-649	100	R710(R760)	1-202-591	5.6K $\pm 10\%$ 1/2W composition
R433	1-242-690	5.1K	R711(R761)	1-202-525	10 $\pm 10\%$ 1/2W composition
R434	1-242-643	56	R712(R762)	1-242-661	330
R435	1-244-689	4.7K	R713(R763)	1-242-661	330
R436	1-244-633	22	R714(R764)	1-242-625	10
R437	1-244-633	22	R715(R765)	1-242-625	10
R438	1-244-643	56	R716(R766)	1-242-619	5.6
R439	1-202-560	300 $\pm 10\%$ 1/2W composition	R717(R767)	1-242-619	5.6
R440	1-202-560	300 $\pm 10\%$ 1/2W composition	R718(R768)	1-242-625	10
			R719(R769)	1-242-657	220
R501(R551)	1-242-721	100K	R720(R770)	1-242-657	220
R502(R552)	1-242-674	1.1K	R721(R771)	1-205-802	0.47 $\pm 10\%$ 2W wire-wound
R503(R553)	1-242-713	47K	R722(R772)	1-205-802	0.47 $\pm 10\%$ 2W wire-wound
R504(R554)	1-242-677	1.5K	R723	1-242-677	1.5K
R505(R555)	1-242-737	470K	R724(R774)	1-242-649	100
R506(R556)	1-242-657-09	220	R725(R775)	1-242-699	12K
R507(R557)	1-242-705	22K	R726(R776)	1-202-565	470 $\pm 10\%$ 1/2W composition
R508(R558)	1-242-725	150K			
R509	1-242-709	33K	R801	1-202-553	150 $\pm 10\%$ 1/2W composition
R510(R560)	1-242-737	470K	R802	1-242-732	300K
R511(R561)	1-242-677	1.5K	R803	1-242-691	5.6K
R512(R562)	1-242-691	5.6K	R804	1-242-693	6.8K
R513(R563)	1-242-705	22K	R805	1-242-696	9.1K
R514(R564)	1-242-705	22K			

<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>
R806	1-206-117	18 $\pm 10\%$ 2W metal-oxide			
R807	1-242-681	2.2K			
R901	1-202-645	1M $\pm 10\%$ 1/2W composition			
RT551	1-222-945	1K(B), semi-fixed			
RT701(751)	1-222-981	10K(B), semi-fixed			
RV601(RV651)	1-222-375	250K (S), variable (volume control)			
RV602(RV652)	1-222-382	50K (A), variable (tone control)			
RV603(RV653)	1-222-382	50K (A), variable (tone control)			
Switches			Miscellaneous		
S1	1-514-799	switch, lever (FUNCTION 1)	F801	1-532-268	fuse 2A
S2	1-514-807	switch, rotary/slide (FUNCTION 2)	F901,902	1-532-298	fuse 2A
S3	1-514-798	switch, slide (MONITOR)	PL901	1-518-051-12	lamp, stereo 4.5V 40mA
S4	1-514-798	switch, slide (MODE)	PL902,903	1-518-070	lamp, dial 8V 0.3mA
S5	1-514-798	switch, slide (HIGH FILTER)	PL904	1-518-017-03	lamp, meter 8V 0.15 A
S6	1-514-798	switch, slide (LOUDNESS)	PL905,906	1-518-051-22	lamp, fm, a-m indicating 4.5V 40mA
S7	1-514-507	switch, rotary (SPEAKER)			
S8	1-514-505	switch, lever (POWER)			
			1-231-057-12		encapsulated component, 120 Ω + 0.033 μ F
			1-507-265-13		jack, HEADPHONE
			1-507-268		PHONO jack, 8-p
			1-509-403		AC outlet
			1-517-021		socket, meter lamp
			1-520-083		meter, tuning
			1-533-048		fuse post
			1-533-051		socket, dial lamp
			1-534-526		cord, power
			1-536-177		terminal strip, L1 (C)
			1-536-189		terminal strip, 1L1 (B)
			1-536-248		pin, connecting
			1-536-284		terminal strip, 4-p
			1-536-286		terminal strip, 4-p

Filters**FM I-F CERAMIC FILTERS**

<u>Part No.</u>	<u>Color</u>	<u>Specified Center Freq.</u>
CF201	red	10.70 MHz
CF202	black	10.66 MHz
CF203	white	10.74 MHz
CF204	green	10.62 MHz
CF205	yellow	10.78 MHz
CF206		

